



Calhoun: The NPS Institutional Archive
DSpace Repository

Theses and Dissertations

1. Thesis and Dissertation Collection, all items

1995-06

A design and performance analysis for the Hot Primary Heat Exchanger (HPX) using numerical analysis

Muhs, Kevin Scott.

Monterey, California. Naval Postgraduate School

<http://hdl.handle.net/10945/7512>

This publication is a work of the U.S. Government as defined in Title 17, United States Code, Section 101. Copyright protection is not available for this work in the United States.

Downloaded from NPS Archive: Calhoun



Calhoun is the Naval Postgraduate School's public access digital repository for research materials and institutional publications created by the NPS community. Calhoun is named for Professor of Mathematics Guy K. Calhoun, NPS's first appointed -- and published -- scholarly author.

Dudley Knox Library / Naval Postgraduate School
411 Dyer Road / 1 University Circle
Monterey, California USA 93943

<http://www.nps.edu/library>

NAVAL POSTGRADUATE SCHOOL MONTEREY, CALIFORNIA



THESIS

**A DESIGN AND PERFORMANCE ANALYSIS FOR
THE HOT PRIMARY HEAT EXCHANGER (HPX)
USING NUMERICAL ANALYSIS**

by
Kevin Scott Muhs
June, 1995

Thesis Advisor:

Ronald J. Pieper

Thesis Co-Advisor:

Ashok. Gopinath

Approved for public release; distribution is unlimited.

Thesis
M88477

DUDLEY KNOX LIBRARY
NAVAL POSTGRADUATE SCHOOL
MONTEREY CA 93943-5101

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instruction, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188) Washington DC 20503.			
1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE June 1995	3. REPORT TYPE AND DATES COVERED Master's Thesis	
4. TITLE AND SUBTITLE A Design and Performance Analysis for the Hot Primary Heat Exchanger (HPX) Using Numerical Analysis		5. FUNDING NUMBERS	
6. AUTHOR(S) Kevin Scott Muhs			
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Naval Postgraduate School Monterey CA 93943-5000		8. PERFORMING ORGANIZATION REPORT NUMBER	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)		10. SPONSORING/MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES The views expressed in this thesis are those of the author and do not reflect the official policy or position of the Department of Defense or the U.S. Government.			
12a. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution is unlimited.		12b. DISTRIBUTION CODE	
13. ABSTRACT (maximum 200 words) The Hot Primary Heat Exchanger (HPX), a key component of the ThermoAcoustic Life Sciences Refrigerator, consists of a tube and fin design. The tubing is bent into a serpentine pattern and overlaid on a screen of copper fins. The serpentine pattern results in several flow reversals and complex internal flow geometries within the heat exchanger. The fins are not consistently of uniform length and generally have heat rejection at both ends. This design results in a forced-cooled, single stack cold plate configuration with unequal temperatures at each end of the fin. The analysis of this configuration requires a methodology based upon the existence of an adiabatic point somewhere along the fin between the prime surfaces. Once the location of this adiabatic point is known, the cold plate may be treated on the basis of two isolated surfaces having fins with adiabatic tips. The goal of this thesis is to provide design analysis and performance predictions for the Hot Primary Heat Exchanger (HPX) using numerical analysis of the tube and fin arrangement of the HPX.			
14. SUBJECT TERMS Heat Exchange, Fin Analysis, Fin Efficiency		15. NUMBER OF PAGES 173	
		16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified	20. LIMITATION OF ABSTRACT UL

Approved for public release; distribution is unlimited.

**A DESIGN AND PERFORMANCE ANALYSIS FOR THE HOT PRIMARY HEAT
EXCHANGER (HPX) USING NUMERICAL ANALYSIS**

Kevin S. Muhs
Lieutenant, United States Navy
B.S., University of Washington, 1987

Submitted in partial fulfillment
of the requirements for the degree of

**MASTER OF SCIENCE IN MECHANICAL ENGINEERING
MASTER OF SCIENCE IN ASTRONAUTICAL ENGINEERING**

from the

**NAVAL POSTGRADUATE SCHOOL
June 1995**

Author:

Kevin Scott Muhs

Approved by:

Ronald J. Pieper, Thesis Advisor

Ashok Gopinath, Co-Advisor

Matthew D. Kelleher, Chairman
Department of Mechanical Engineering

Daniel J. Collins, Chairman
Department of Aeronautics and Astronautics

Thesis
M884/74
c.2

ABSTRACT

The Hot Primary Heat Exchanger (HPX), a key component of the ThermoAcoustic Life Sciences Refrigerator, consists of a tube and fin design. The tubing is bent into a serpentine pattern and overlaid on a screen of copper fins. The serpentine pattern results in several flow reversals and complex internal flow geometries within the heat exchanger. The fins are not consistently of uniform length and generally have heat rejection at both ends. This design results in a forced-cooled, single stack cold plate configuration with unequal temperatures at each end of the fin. The analysis of this configuration requires a methodology based upon the existence of an adiabatic point somewhere along the fin between the prime surfaces. Once the location of this adiabatic point is known, the cold plate may be treated on the basis of two isolated surfaces having fins with adiabatic tips. The goal of this thesis is to provide design analysis and performance predictions for the Hot Primary Heat Exchanger (HPX) using numerical analysis of the tube and fin arrangement of the HPX.

TABLE OF CONTENTS

I. INTRODUCTION	1
II. HEAT TRANSFER FROM EXTENDED SURFACES	5
A. BASIC HEAT TRANSFER CONCEPTS	5
B. FIN CONCEPTS	7
C. FIN ANALYSIS WITH AXISYMMETRIC HEAT LOADING	13
III. THE THERMOACOUSTIC LIFE SCIENCES REFRIGERATOR	21
A. THERMAL SYSTEMS OVERVIEW	21
B. THE HOT PRIMARY HEAT EXCHANGER (HPX)	22
C. COMPUTER MODELING OF THE HEAT TRANSFER PROCESS	28
IV. PERFORMANCE ANALYSIS	31
A. HOT PRIMARY GAS SIDE HEAT TRANSFER COEFFICIENT DETERMINATION	31
B. TEMPERATURE EXCESS DETERMINATION	34
V. EFFECTS OF TEMPERATURE EXCESS RATIO VARIATIONS	41
VI. RESULTS	49
A. PROGRAM OUTPUT	49
VII. SUMMARY AND CONCLUSIONS	55

A.	DESIGN EFFECTIVENESS	55
B.	EFFECTIVENESS OF SINGLE STACK COLD PLATE ANALYSIS	56
C.	EFFECTIVENESS OF COMPUTER MODELING	56
D.	VALIDITY OF PERFORMANCE ANALYSIS	57
APPENDIX A. MURRAY-GARDNER ASSUMPTIONS		59
APPENDIX B. TRANSFORMATION MATRIX DEVELOPMENT		61
APPENDIX C. NODAL MODELING DATA		65
APPENDIX D. SPREADSHEET K-VALUE DETERMINATION AND NODE CONNECTION DATA		69
APPENDIX E. TASS NODAL TEMPERATURE OUTPUT		151
LIST OF REFERENCES		157
INITIAL DISTRIBUTION LIST		159

LIST OF SYMBOLS, ACRONYMS, AND/OR ABBREVIATIONS

ROMAN LETTER SYMBOLS

A	area of heat flow path
b	fin height [m]
c	specific heat capacity [kJ/kg-K]
d	diameter [m]
h	heat transfer coefficient [W/m ² -K]
K	node conductance matrix
K	elements of the matrix K
k	thermal conductivity [W/m-K]
L	length of channel (fin length) [m]
ΔL	length between conductance nodes [m]
m	fin performance factor [m ⁻¹]
n	number of fins
Nu	Nusselt number [dimensionless]
P	wetted perimeter [m]
Pr	Prandtl number [dimensionless]
q	heat flow [W]
R	radius [m]
Re	Reynolds number [dimensionless]
Re	temperature excess ratio [dimensionless]
T	temperature [°C]
ΔT	temperature difference [°C]
t	elements of the temperature matrix T
w	weight flow [kg/hr]
Y	thermal admittance [W/K]

GREEK LETTER SYMBOLS

β	a linear transformation matrix
γ	element of the matrix Γ
Γ	a linear transformation matrix
δ	fin width or thickness [m]
θ	temperature excess [K]
Δ	$\Delta = e^{\theta}$
μ	dynamic viscosity
τ	element of the matrix β

SUBSCRIPTS

a	designates fin tip
avg	designates average
b	designates fin base
c	designates cross-sectional area
cond	designates heat flow due to conductivity
conv	designates heat flow due to convection
e	designates effective diameter
f	designates fin surface
F	designates fluid quantities

ideal	designates ideal values
in	designates input condition
inner	designates inner radius
max	designates maximum quantity
o	designates characteristic value
outer	designates outer radius
p	designates prime surface
s	designates surface area

ACRONYMS

CPX	Cold Primary Heat Exchanger
EHX	Experimental Heat Exchanger
HPX	Hot Primary Heat Exchanger
IRE	Insulated Refrigeration Enclosure
TALSR	ThermoAcoustic Life Sciences Refrigerator

ACKNOWLEDGMENT

The author would like to gratefully acknowledge the high quality guidance and technical assistance provided in the completion of this thesis by Professors Pieper and Kraus of the Electrical Engineering department. In addition, Professor Gopinath of the Mechanical Engineering department and Professor Biblarz of the Aeronautical Engineering curriculum provided many valuable suggestions.

The moral support and technical assistance of fellow students also assisted the author in this endeavor. Specifically, David Nash is responsible for the high quality graphics drawings, and Dan Rosser offered mathematical guidance and acted as a sounding board for a variety of my ideas.

The greatest portion of appreciation goes to the authors' family, Tammy, Anna Marie, and Bradley, for enduring long hours, schedule conflicts, missed events and high stress levels.

Thanks to one and all, and thanks to the Lord who has given me the privilege of knowing and working with each of the aforementioned individuals.

I. INTRODUCTION

The Hot Primary Heat Exchanger (HPX), a key component of the ThermoAcoustic Life Sciences Refrigerator (TALSR), consists of a tube and fin design. The tubing is bent into a serpentine pattern and overlaid on a screen of copper fins. This configuration results in several flow reversals and complex internal gas side flow geometries within the heat exchanger. The fins are not consistently of uniform length and generally have heat rejection at unequal temperatures on each end of the fin. This design results in a forced-cooled, single stack cold plate configuration. The TALSR uses forced convection with an acoustic oscillator providing internal flow through channels created within the configuration of the HPX.

The first formal analyses of the cold plate configuration was provided by Mark and Stephenson (1954) and Kraus (1961). These analyses provided expressions for the efficiency of the cold plate for the case of heat loading on one side. Subsequently, Kern and Kraus (1972) looked at the single stack cold plate with heat input on only one, and on both sides. Incropera and Dewitt (1981) presented a classical textbook culmination of extended surface research and general conduction analysis for fins of uniform cross-sectional area. An application of extended surface principles and research was used by Garrett (1992) to evaluate the forced convective thermal performance of the HPX. Most recently, Pieper and

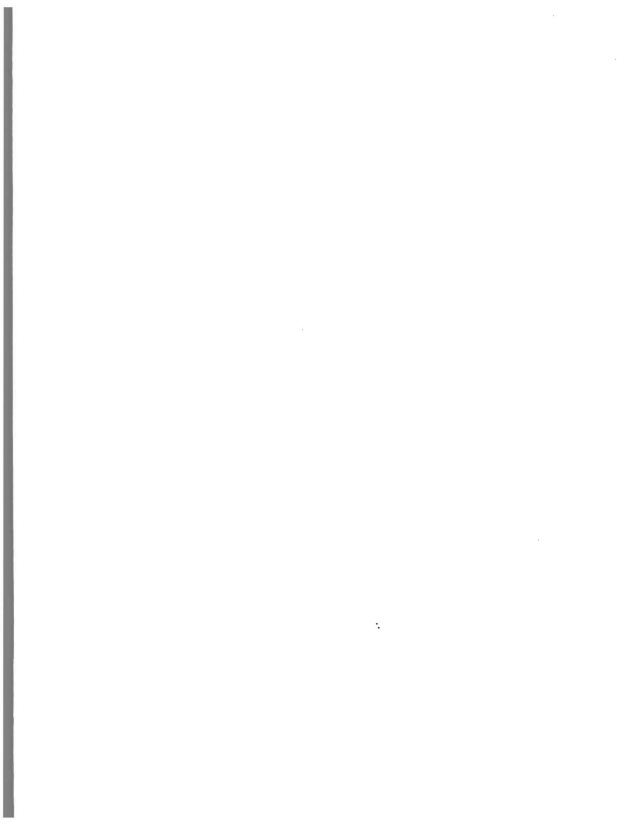
Kraus (1995) looked at the cold plate configuration with asymmetric heat loading and proposed dividing the plate into two fins, each possessing an adiabatic tip for analysis purposes. This permits a more accurate representation of the performance of the cold plate configuration.

The goal of this thesis is to utilize the results of Pieper and Kraus (1995) to provide design analysis and performance predictions for the Hot Primary Heat Exchanger (HPX) using a numerical optimization of the serpentine tube and fin arrangement in the HPX.

The serpentine pattern of the copper tubing in the HPX is unique when compared to a majority of the tube and fin heat exchangers currently in use. A vast majority of current applications involve parallel fluid flow in tubes through a matrix of fins to provide the required heat transfer. This results in fairly uniform base temperatures at each end of the fin. In contrast, the serpentine tubing in the HPX results in non-uniform base temperatures due to increasing temperatures along the length of the tube. Research into the thermal performance of a non-uniform base temperature design is limited and on-going, however, a successful application of this configuration has been achieved on a large scale at the WyoDak energy facility in Gillette Wyoming, shown in Figure 1.

Chapter II of this thesis is used to present fundamental heat transfer concepts, and extended surface evaluation techniques. Chapter III provides a physical description of

the ThermoAcoustic Life Sciences Refrigerator (TALSR) and discusses the role of the Hot Primary Heat Exchanger in the heat transfer cycle of the TALSR. Chapter IV details the numerical simulation techniques used in the performance analysis of the HPX. Chapter V presents a discussion on efficiency modeling and the factors affecting extended surface efficiencies. Analysis results and conclusions are presented in Chapters VI, and VII respectively.



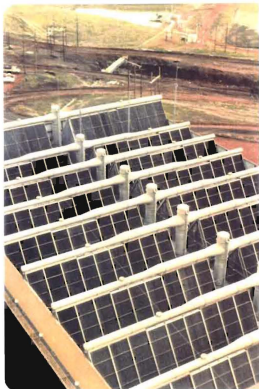


Figure 1: WyoDak Energy Facility in Gillete Wyoming



II. HEAT TRANSFER FROM EXTENDED SURFACES

The convective heat transfer rate of a bare surface may be increased by increasing the surface area through which the convection occurs. This may be accomplished by using surfaces that extend from the bare surface into the surrounding fluid. Naturally, a considerably larger amount of heat can be transferred from or to an extended surface in a given time period than from or to a bare surface. The type of extended surface most commonly used, is termed a fin. The thermal conductivity of the fin material has a strong effect on the temperature distribution along the fin and therefore influences the degree to which the heat transfer rate is enhanced.

A. BASIC HEAT TRANSFER CONCEPTS

Conduction is the heat flow mechanism whereby heat is transferred by molecular diffusion from one part of a medium under the influence of a temperature gradient without a net displacement of the particles that compose the medium. It was Fourier who proposed that the heat flow is directly proportional to the area of the heat flow path and the temperature gradient along the path,

$$q \propto A(dT/dx) \quad (2.1)$$

Insertion of a proportionality constant yields:

$$q_{\text{cond}} = -kA(dT/dx) \quad (2.2)$$

where,

A = area of the heat flow path

k = thermal conductivity of the material

(dT/dx) = change in temperature per unit length

The minus sign assures a positive heat flow in the presence of the required negative temperature gradient.

Convection is a fluid flow process that results in the transfer of heat from or to a confining surface by a flowing fluid. The fluid flow may be induced by buoyancy, density gradients or through the use of mechanical methods. Those methods utilizing mechanical flow generation are termed forced convection.

A second classification of convective heat transfer is as either internal or external. In internal flow the fluid is constrained on all sides by solid boundaries, as in flow through a pipe. In external flow the fluid has at least one side extending to infinity without encountering a solid surface. Heat flow during convection is directly proportional to the temperature difference between the confining surface and the surface area over which the process takes place:

$$q \propto A \Delta T \quad (2.3)$$

Insertion of a proportionality factor yields,

$$q_{\text{conv}} = hA \Delta T \quad (2.4)$$

Equation (2.4) is Newton's law of cooling and h is called the convection heat transfer coefficient and encompasses all the effects that influence the convection mode.

B. FIN CONCEPTS

To determine the heat transfer rate associated with a fin, the temperature distribution along the fin must first be obtained. In the temperature distribution analysis, some standard assumptions are made. First, radiation effects are neglected. In addition, the fin is assumed to comply with the well known Murray (1938) and Gardner (1945) assumptions listed in Appendix A. The one dimensional assumption of Murray-Gardner is valid because in most extended surface applications the fins are relatively very thin compared to their height. Thus, the temperature changes in the longitudinal direction are much larger than those in the transverse direction and the one dimensional assumption is satisfactory. The material used in the construction of the fin is characterized by a thermal conductivity, k . It is also assumed that the heat transfer coefficient due to convection, h , is known. Thus, following the standard, steady state fin characterization of Incropera and Dewitt (1981), it is found that;

$$(k) d(A_c(x) dT/dx) / dx - (h) (dA_s(x) / dx) (T - T_\infty) = 0 \quad (2.5)$$

where A_c is the cross-sectional area, and A_s is the surface

area, both of which may vary with x . Equation (2.5) may be simplified by defining a temperature excess, θ , as,

$$\theta(x) = T(x) - T_{\infty} \quad (2.6)$$

where because T_{∞} is a constant, $d\theta/dx = dT/dx$. Substituting Equation (2.6) into Equation (2.5), results in;

$$(k) d(A_c(x) d\theta(x)/dx)/dx - (h) (dA_s(x)/dx) \theta(x) = 0 \quad (2.7)$$

To determine the temperature distribution along the length of an individual fin, it is necessary to solve Equation (2.7) for the specific fin geometry.

For the case of an individual rectangular fin of length b , as shown in Figure 2, consider that the origin of the coordinate is at the fin tip with positive orientation toward the fin base. The fin width is a constant, δ , therefore A_c is a constant and $A_s = Px$, where A_s is the surface area measured from the tip to x and P is the fin perimeter. Thus, $(dA_c/dx) = 0$ and $(dA_s/dx) = P = (2L + 2\delta) = 2L$ and Equation (2.7) reduces to;

$$d^2\theta/dx^2 - m^2\theta = 0 \quad (2.8)$$

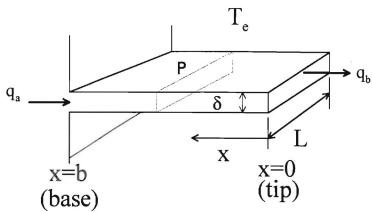


Figure 2: Rectangular longitudinal fin of length b .

where

$$m^2 = 2h/k\delta \quad (2.9)$$

Equation (2.8) is a linear, homogenous, second-order differential equation with constant coefficients. Its general solution is of the form;

$$\theta(x) = C_1 e^{mx} + C_2 e^{-mx} \quad (2.10)$$

By substitution, it is easily verified that Equation (2.10) is a solution to Equation (2.8).

To evaluate the constants C_1 and C_2 of Equation (2.10), it is necessary to specify initial value data;

$$\theta(x = b) = \theta_b$$

and (2.11)

$$q(x = b) = q_b$$

This makes

$$\theta_b = C_1 e^{nb} + C_2 e^{-nb} \quad (2.12)$$

and applying $q_b = k\lambda(d\theta_b/dx)$ gives

$$q_b = k\delta mL[C_1 e^{nb} - C_2 e^{-nb}] \quad (2.13)$$

or

$$q_b = Y_o [C_1 e^{mb} - C_2 e^{-mb}] \quad (2.14)$$

where $Y_o = k\delta mL$, is called the characteristic thermal admittance of the fin and has the units $W/^\circ C$.

It is then a matter of algebra to evaluate the constants C_1 and C_2 such that;

$$\theta(x) = \theta_b \cosh(m[b-x]) - (q_b/Y_o) \sinh(m[b-x]) \quad (2.15)$$

and

$$q(x) = \theta_b Y_o \sinh(m[b-x]) + q_b \cosh(m[b-x]) \quad (2.16)$$

Now that the temperature excess and heat flow at any point in the fin have been evaluated, a convenient method of mapping conditions at the fin tip to conditions at the fin base is desired.

For individual fins, Kraus et al. (1978) showed that conditions of heat flow and temperature excess (relative to the presumed constant and uniform temperature environment) at any point on a fin are induced by similar conditions at the fin base. This resulted in the development of a linear transformation that mapped conditions at the fin tip to conditions at the fin base:

$$\begin{bmatrix} \theta_b \\ q_b \end{bmatrix} = \beta \begin{bmatrix} \theta_a \\ q_a \end{bmatrix} = \begin{bmatrix} \tau_{11} & \tau_{12} \\ \tau_{21} & \tau_{22} \end{bmatrix} \begin{bmatrix} \theta_a \\ q_a \end{bmatrix} \quad (2.17)$$

where the matrix β is called the inverse thermal transmission matrix. Its elements are designated as the inverse thermal transmission parameters. A summary of this work is provided in Appendix B.

Applying the development of Kraus et al. (1978) to the rectangular fin of Figure 2, it is seen that the inverse thermal transmission matrix is given by

$$\beta = \begin{bmatrix} \cosh mb & (Z_o)(\sinh mb) \\ Y_o(\sinh mb) & \cosh mb \end{bmatrix} \quad (2.18)$$

where $Y_o = (2hk\delta)^{1/2}L$, $Z_o = 1/Y_o$, and k , L , h , and δ are the thermal conductivity, fin length, heat transfer coefficient, and fin thickness respectively. Thus, this matrix can be used to map conditions at the fin tip to conditions at the fin base

$$\begin{bmatrix} \theta_b \\ q_b \end{bmatrix} = \begin{bmatrix} \cosh mb & (Z_o)(\sinh mb) \\ Y_o(\sinh mb) & \cosh mb \end{bmatrix} \begin{bmatrix} \theta_a \\ q_a \end{bmatrix} \quad (2.19)$$

In addition to developing the linear transformation matrices, Kraus et al. (1978) also proposed that the conventional fin efficiency be abandoned and that single fins be characterized by a single parameter called the thermal transmission ratio, the ratio of the heat entering the fin to the temperature excess at the base of the fin. This was later called the fin input admittance [Kraus (1982)] and was given in the form of a bilinear transformation;

$$Y_{in} = q_b/\theta_a = (\tau_{21} + (q_a/\theta_a)\tau_{22})/(\tau_{11} + (q_a/\theta_a)\tau_{12}) \quad (2.20)$$

The fin input admittance is particularly useful in the analysis and evaluation of finned arrays and will play an important role in the analysis of the HPX.

C. FIN ANALYSIS WITH AXISYMMETRIC HEAT LOADING

Consider the forced cooled cold plate shown in Figure 3 and observe that the single fin of total height b has been subdivided into two fins with fin heights b_1 and b_2 , to allow for the fact that the temperature differences at its opposite ends may not be equal. Note that the temperature excess, θ , is defined as the difference between the temperature at any point on the fin, T , and the temperature of the coolant fluid, T_c , as given in Equation (2.6).

As shown in Figure 3, the origins of the fin height coordinates, x_1 and x_2 , are taken at the tips of fin 1 and fin

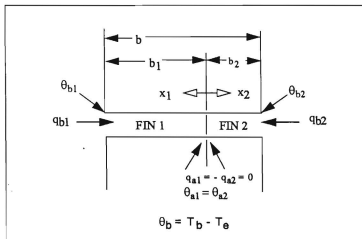


Figure 3: Forced cooled cold plate configuration used in axisymmetric heat loading analysis

2 with a positive orientation from fin tip to fin base. The fin heights, b_1 and b_2 , are chosen such that no heat crosses the interface between fin 1 and fin 2, thus creating an adiabatic fin tip condition. This is characterized by a linear transformation of Equation (2.19) for the longitudinal fin of rectangular profile shown, given by;

$$\begin{bmatrix} \theta_{b1} \\ q_{b1} \end{bmatrix} = \begin{bmatrix} \cosh mb_1 & Z_o(\sinh mb_1) \\ Y_o(\sinh mb_1) & \cosh mb_1 \end{bmatrix} \begin{bmatrix} \theta_{a1} \\ q_{a1} \end{bmatrix} \quad (2.21)$$

and

$$\begin{bmatrix} \theta_{b2} \\ q_{b2} \end{bmatrix} = \begin{bmatrix} \cosh mb_2 & Z_o(\sinh mb_2) \\ Y_o(\sinh mb_2) & \cosh mb_2 \end{bmatrix} \begin{bmatrix} \theta_{a2} \\ q_{a2} \end{bmatrix} \quad (2.22)$$

The cold plate configuration of Figure 3 is subject to the continuity and compatibility conditions at the interface between fins 1 and 2. These conditions require an adiabatic interface between b_1 and b_2 and are given in matrix form as;

$$\begin{bmatrix} \theta_{a1} \\ q_{a1} \end{bmatrix} = \begin{bmatrix} \theta_{a2} \\ -q_{a2} \end{bmatrix} = \begin{bmatrix} \theta_a \\ 0 \end{bmatrix} \quad (2.23)$$

If $\theta_{b1} \neq \theta_{b2}$, symmetry will not apply and the fin height s b_1 and b_2 will not be equal ($b_1 \neq b_2$).

In order to determine fin lengths b_1 and b_2 , Equations (2.21) and (2.22) may be expanded using the conditions of Equation (2.23). In particular with $\theta_{a1} = \theta_{a2} = \theta_a$, the following equations are derived,

$$\theta_{b1} = [\cosh mb_1]\theta_a \quad (2.24)$$

$$\theta_{b2} = [\cosh mb_2]\theta_a \quad (2.25)$$

Equation (2.24) and Equation (2.25) show that the base temperature excesses for b_1 and b_2 are related through θ_a , thus, a temperature excess ratio (R_θ) for a given cold plate configuration may be defined as:

$$R_\theta = \theta_{b1}/\theta_{b2} = [\cosh mb_1]/[\cosh mb_2] \quad (2.26)$$

The hyperbolic cosines of Equation (2.26) can also be represented as exponentials;

$$R_\theta = (e^{mb1} + e^{-mb1})/(e^{mb2} + e^{-mb2}) \quad (2.27)$$

Using the observation from Figure 3, that $b_2 = b - b_1$, it is a matter of algebra to show that;

$$R_\theta = (\Lambda^2 + e^{2mb1})/(\Lambda[e^{2mb2} + 1]) \quad (2.28)$$

where

$$\Lambda = e^{\eta b} \quad (2.29)$$

The value of b_2 for a given value of R_0 can then be found by re-arranging Equation (2.28) to provide;

$$b_2 = (1/2m) (\ln[\Lambda(\Lambda - R_0)/(R_0\Lambda - 1)]) \quad (2.30)$$

An evaluation of R_0 using Equation (2.30) confirms that if $R_0=1$ because $\theta_{b1} = \theta_{b2}$, then because of symmetry, b_2 must equal half of the total fin height. In addition, the value of R_0 for $b_2=0$ can be found directly from Equation (2.28),

$$(R_0)_{\max} = (\Lambda^2 + 1)/(2\Lambda) \quad (2.31)$$

and similarly for $b_2=b$,

$$(R_0)_{\min} = (2\Lambda)/(\Lambda^2 + 1) \quad (2.32)$$

If R_0 is not within the domain of values specified by Equations (2.31) and (2.32) the fin is then treated as a single fin without an adiabatic point. However, for the HPX model, the R_0 values are always within this domain and the single fin analysis is not required.

Once b_2 is known, b_1 is easily found through a simple subtraction procedure ($b_1 = b - b_2$). With both b_1 and b_2

known, the cold plate may be treated on the basis of two isolated surfaces having fins with adiabatic tips, treating each fin individually as though the other were not present. One surface is governed by b_1 with θ_{b1} specified, and the other is governed by b_2 with θ_{b2} specified. Thus, there are two entities, each with a prime surface and each with a fin, and these surfaces may be treated individually as if the other were not present.

The performance of each prime surface, and fin (b_1 or b_2) combination depends on the total input admittance of the pair. The total input admittance, Y_{in} , is just the sum of the prime surface and fin input admittances,

$$Y_{in} = Y_{in,p} + Y_{in,f} \quad (2.33)$$

where the subscripts, p and f refer to the prime surface and the fin, respectively, and where both prime and fin base surfaces are operating at θ_b .

The prime surface input admittance is determined by its convective dissipation

$$Y_{in,p} = hS_p \quad (2.34)$$

where as seen from Figure 4,

$$S_p = (W - \delta)L \quad (2.35)$$

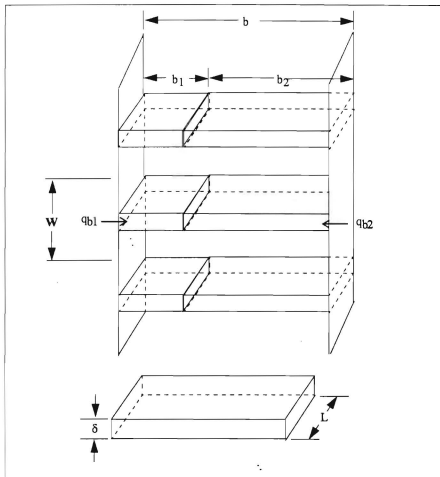


Figure 4: Schematic of single stack, cold plate heat transfer geometry.

which accounts for the footprint occupied by the fin.

The fin input admittance is derived from the fin β -matrix given by Equation (2.18). Because the height b_2 is based upon the determination of an adiabatic point, $Y_{in,f}$ is established by realizing that for $q_s = 0$ Equation (2.20) becomes;

$$Y_{in} = q_b/\theta_s = \tau_{21}/\tau_{11} = Y_o \sinh(mb) / \cosh(mb) \quad (2.36)$$

which for the fin governed by b_2 , becomes

$$Y_{in,f} = Y_o \tanh(mb_2) \quad (2.37)$$

Then, if the temperature excesses are specified so that R_0 leads to the establishment of b_2 , the heat dissipation is obtained from;

$$q_b = Y_{in} \theta_b \quad (2.38)$$

This section provides the basis for an accurate thermal performance model needed in the simulation of the heat transfer process in the TALSR discussed in the next chapter.

III. THE THERMOACOUSTIC LIFE SCIENCES REFRIGERATOR

The ThermoAcoustic Life Sciences Refrigerator (TALSR), developed at Naval Postgraduate School, was motivated by the desire to replace the Freon 512 vapor compression refrigeration system currently used on board the Space Shuttle. The TALSR provided a safer alternative due to the fact that it does not use chlorofluorocarbons (CFCs) and therefore could not potentially contaminate the small confined area of the Space Shuttle. In addition, the TALSR also provides the potential for higher reliability, over the current system, because it has no sliding seals and thus requires no lubrication. The ThermoAcoustic Life Sciences Refrigerator uses a complex thermal transport subsystem to remove heat from the Insulated Refrigeration Enclosure (IRE) of the Space Shuttle.

A. THERMAL SYSTEMS OVERVIEW

Heat is removed from the IRE by a Liquid-Air Heat Exchanger fabricated by the Modine Manufacturing Company. It is then transported through two thermoacoustic heat pumps, connected in series, by a mechanically pumped cold heat exchange fluid. The internal architecture of each heat pump consists of a Cold Primary Heat Exchanger (CPX), a Hot Primary Heat Exchanger (HPX), and an Electrodynamic Driver. The Electrodynamic Driver acoustically oscillates an internal

working fluid in each heat pump thereby creating internal gas side flow for both the HPX and the CPX. It is known that the heat transfer between surfaces can be enhanced using longitudinal acoustic waves [Vainshtein (1995)]. This internal gas side flow is used by the Cold Primary Heat Exchanger to remove heat from the cold-side exchange fluid, and transport it to the HPX. The HPX then transfers the heat removed from the cold-side exchange fluid into a secondary cooling loop. This secondary cooling loop transports the heat to the internal environment of the Space Shuttle via an Experimental Heat Exchanger (EHX). A schematic diagram of the series fluid flow through the TALSR thermal transport subsystem is shown in Figure 5 [Garrett (1992)].

B. THE HOT PRIMARY HEAT EXCHANGER (HPX)

The Hot Primary Heat Exchanger uses an acoustically oscillating medium to transport heat and must therefore be analyzed differently from most compact heat exchangers. The most significant difference between standard compact heat exchanger analysis and acoustical heat exchanger analysis is the fact that the acoustically oscillating gas parcels only move a limited distance before reversing their direction of flow. The consequence of this periodic flow reversal is that an increase in the effective surface area for heat transfer cannot arbitrarily be achieved by simply increasing the length of the heat exchange surfaces (fins) in the direction of flow.

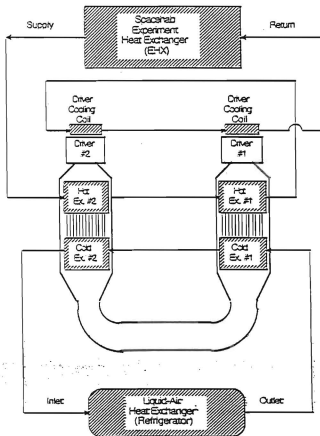


Figure 5: Schematic diagram of the series fluid flow through the Hot and Cold Primary Heat Exchangers. [Garrett (1992)]

Garrett (1992) has shown that the effective area over which heat transfer will take place is limited by the peak-to-peak excursions of the gas parcels over the heat exchange surface. Thus, heat exchange surfaces, which have a length in the flow direction equal to the peak-to-peak displacement of the gas, provide the maximum effective surface area for heat transfer.

The HPX utilizes copper tubing bent into a serpentine pattern and then soldered or furnace brazed on a screen of copper fins, as shown in Figure 6 [Garrett (1992)]. In this configuration, the fins are not of uniform length and for a majority of the fins, there is heat rejection at both ends. This design results in two parallel paths by which the fluid contained within the copper tubing can remove heat from the acoustically oscillating gas. The primary path is through the fins which are bonded to the tube. The fins represent the primary path because they have a greater surface area than the outside diameter of the tubing and because they are designed to have a length in the flow direction approximately equal to the peak-to-peak displacement of the gas. The secondary path is due to the direct convection of the gas around the tubing. This path also provides some useful heat transfer and requires consideration in the thermal analysis of the HPX. A schematic representation of the thermal resistances in the primary heat exchanger energy flow path is shown in Figure 7 [Garrett (1992)]. The tubing for the HPX is standard, circular cross-section, soft copper tubing, with an outer diameter (OD) of

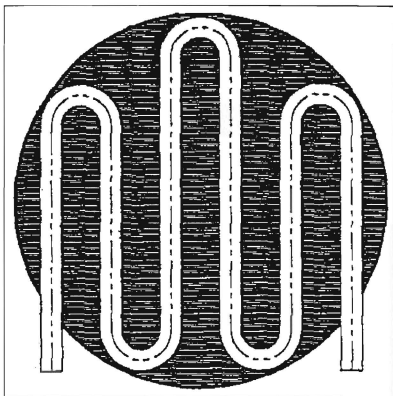


Figure 6: HPX design configuration [Garrett (1992)]

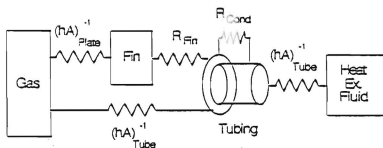


Figure 7: Schematic representation of thermal resistances in the HPX flow path. [Garrett (1992)]

0.635 cm and a wall thickness of 0.076 cm. The HPX has an inner diameter of 11 cm. Table 1 provides a list of the geometrical constraints and heat transfer characteristics used in the analysis of the HPX.

The physical design of the HPX can therefore be modeled as a forced-cooled, single stack cold plate configuration with unequal temperatures at each end of the fin. Thus, an analysis of the HPX can be completed using the derived relationships for cold plates with axisymmetric heat loading.

Symbol	Description	Value	Reference
c_p	specific heat capacity of water	4.182 kJ/kg-K	Incropera and Dewitt (1981)
δ	Fin thickness	0.0152 cm	Garrett (1992)
h_f	Fluid heat transfer coefficient	12600 W/m ² -K	Garrett (1992)
k	thermal conductivity of copper	401 W/m-K	Garrett (1992)
L	Fin width (channel length)	0.3175 cm	Garrett (1992)
Pr	Prandtl number	0.7068	Garrett (1992)
Re	Reynolds number	1900	Garrett (1992)
R_{inner}	Inner radius of copper tubing	0.2413 cm	Garrett (1992)
R_{outer}	Outer radius of copper tubing	0.3175 cm	Garrett (1992)
μ	mean dynamic viscosity	190×10^{-7} N-s/m ²	Incropera and Dewitt (1981)
μ_s	surface dynamic viscosity	184×10^{-7} N-s/m ²	Incropera and Dewitt (1981)

Table 1: A summary of the physical constraints and heat transfer properties used in the analysis of the HPX

C. COMPUTER MODELING OF THE HEAT TRANSFER PROCESS

Once an accurate thermal model has been obtained, an efficient and reliable method of analyzing the heat transfer processes occurring within the heat exchanger is required. This is accomplished through the use of Steady State Thermal Analyzer software version 2.2 provided by InterCept Software. The model builder provides the user with the means to model the physical configuration of interest in order to provide the thermal analyzer with an input file. The thermal analyzer then takes the input file and produces an output file containing a summary of the temperatures within the configuration.

The model building process begins with a drawing of the configuration and a subdivision of it into small but finite subvolumes. Each subvolume is presumed isothermal and the centers of each subvolume are then representative of the entire subvolume. These centers are referred to as nodes and are connected to adjacent nodes through branches consisting of various forms of thermal conductance. These conductance forms are dependent on the mode of heat transfer between adjoining pairs of nodes. The various heat transfer modes available to the user include conduction, laminar free convection, radiation, forced convection, and fluid flow.

Each node can also be connected to a constant temperature, a constant heat input, or a temperature dependent heat input with an appropriate tag. Once a sketch

representation of the nodalized model is complete, the comprehensive node connection data is ready to be input into the model builder program. The input for the model builder program begins with node 1, and the user is asked for information for each connecting node with a greater number. For each connection to an adjacent node, the user must specify the mode of heat transfer with a tag number. After specifying the connecting node and tag, the user is queried as to the whether the conductance will be calculated, input directly, or is the same as an earlier branch. Conductance values are required for each node connection to any higher number node.

Subsequent use of the thermal analysis software results in the writing of n node equations in n unknown temperatures where the nodes are connected by the appropriate thermal conductances. The general solution strategy for these n equations is to then use the nodal conductances of the model to form a set of heat balance equations. In matrix form, this set of heat balance equations has the general form;

$$[K] [T] = [B] \quad (3.1)$$

where K is the matrix of conductances, T is the node temperatures, and B is a matrix composed of constant temperature heat sinks, and/or heat inputs. Many of the conductances are linearized forms of nonlinear expressions for heat transfer by natural convection and other similar heat

transfer modes, therefore, the various terms in the \mathbf{K} matrix may themselves be functions of temperature. Solution of the \mathbf{T} matrix therefore, must be by iteration. Node temperatures obtained after each iteration are used to update the temperature dependent terms in the \mathbf{K} matrix. The thermal analyzer uses a Cholesky factorization [Hamming (1973)] of the \mathbf{K} matrix to perform this iteration. This iterative solution continues until the change in nodal temperatures between successive iterations is smaller than a user-specified error criteria. Once the iterative solution is obtained, the thermal analyzer writes the temperatures to an output file, where they can be read and analyzed by the user.

IV. PERFORMANCE ANALYSIS

The thermal analysis of the TALSR requires an adequate model capable of determining both the heat transfer characteristics for the complex flow geometries within the HPX, and the values of temperature along the serpentine pattern of the copper tubing. The thermal conductivity of copper, k , the fin thickness, δ , and the channel length, L , are all easily determined from the given material and geometrical considerations of the HPX. Therefore, to complete the thermal analysis, the convection coefficient, h , is required to determine the total input admittance, and the conductance matrix is needed to map base temperature excesses along the length of copper tubing. These remaining values are determined using numerical analysis techniques.

A. HOT PRIMARY GAS SIDE HEAT TRANSFER COEFFICIENT DETERMINATION

The convection heat transfer coefficient, h , encompasses all the effects that influence the convection mode. It depends on conditions in the boundary layer, which are influenced by surface geometry, the nature of fluid motion and many of the fluid thermodynamic and transport properties. By considering the magnitude of the factors affecting the heat transfer coefficient, h , an appreciation for the complexity in determining its value is obtained. In simple flow situations, solutions for h are readily effected mathematically, however,

for situations of complex flow geometries, such as those in the TALSR, the more practical approach involves calculating h from empirical equations. The particular form of these equations is obtained by correlating measured convection heat and mass transfer results in terms of appropriate dimensionless groups. The development of the dimensionless group used to determine h was performed by Incropera and Dewitt (1981), and resulted in the derivation of the Nusselt number (Nu). The dimensionless Nusselt number provides a measure of the convective heat transfer occurring at the surface. For a prescribed geometry, the Nusselt number is a universal function of x' , the Reynolds number, and the Prandtl number, where x' is the dimensionless length of the fluid along the channel. A detailed analysis of these factors will determine the exact correlation to be used in determining the Nusselt number. For the given flow geometry and considerations of the HPX, the Reynolds number is given by Garrett (1992) to be 1900, therefore, flow through the coolant channel remains in the laminar region. In the absence of strict correlations for oscillatory flow convection coefficients, a steady flow Nusselt correlation was assumed to provide a suitable representation of heat transfer in the channel. Sieder and Tate (1936) proposed a suitable correlation for laminar flow in tubes and ducts $[(Re_0 Pr D/L)^{1/3} (\mu/\mu_s)^{0.14}] \geq 2$ given by;

$$\text{Nu} = 1.86 (\text{RePr}/(L/D))^{1/3} (\mu/\mu_s)^{0.14} \quad (4.1)$$

where μ and μ_s are the average dynamic viscosity and the surface dynamic viscosity respectively. From knowledge of the Nusselt number, the convection coefficient may now be found using;

$$\text{Nu} = (hd_e/K_F) \quad (4.2)$$

where d_e is the effective diameter of a non-circular duct through which the fluid passes. Replacing D with d_e in Equation (4.1) and combining with Equation (4.2) results in

$$h = (\text{Nu}(K_F)/d_e) = (1.86K_F/d_e) (\text{RePr}/(L/d_e))^{1/3} (\mu/\mu_s)^{0.14} \quad (4.3)$$

Then using the values of L , Re and Pr specified in Table 1, and realizing that for air $(\mu/\mu_s)^{0.14} \sim 1$ over the temperature range of interest for the HPX it is easily shown that;

$$h = (7.9 \times 10^{-3})/d_e^{2/3} \quad (4.4)$$

where h is given in Watts/cm²-K. The effective diameter, d_e , is defined as;

$$d_e = (4A_c/P) \quad (4.5)$$

where A_c and P are the flow cross-sectional area and the wetted perimeter respectively. A rectangular duct flow geometry is assumed for the TALSR based on the large radius of curvature of the HPX and the small spacing between fins, thus as shown in Figure 4;

$$d_o = 2zb/(b + z) \quad (4.6)$$

where $z = (W - \delta)/2$, and $b = b_1 + b_2$. The value of b varies by location within the HPX, as shown in Figure 5, and results in corresponding changes in the convection coefficient for each location. Therefore the value of h in Equation (4.4) must be considered independently for each location along the copper tubing. This significantly increases the complexity of the analysis.

B. TEMPERATURE EXCESS DETERMINATION

Determination of temperature excess variation with location along the length of copper tubing is also required to adequately complete the analysis of the TALSR. An accurate model of the heat transfer processes shown in Figure 7 is required to determine this variation.

Application of the model builder program THANSS, located within the Steady State Thermal Analyzer software, to the TALSR is accomplished by dividing the length of the copper tubing surface into 144 subvolumes of varying size based on

location. Additionally, another 144 nodes are assigned to corresponding fluid nodes within the pipe to account for variations in fluid temperature as it flows through the tubing. A summary of nodal assignments based on location is given in Appendix C. An additional two nodes are required to complete the model. The first node, a constant heat source node, is assigned to the air flowing through the coolant channels created by the tube and fin design. The temperature of the air is considered uniform and constant at 40°C. The second node is used to represent the liquid input temperature at the inlet to the HPX. This temperature is also assumed uniform and constant at a temperature of 25°C.

The general form of the heat flow equations used for all modes of heat transfer considered within the HPX is;

$$q = K(T_1 - T_2) \quad (4.7)$$

where K, the conductance, varies in form depending on the mode of heat transfer considered. For the HPX model, four forms of thermal conductance are required to define the various modes of heat transfer occurring within the HPX.

The first conductance is represented as K_1 and is given by;

$$K_1 = kA_c/\Delta L \quad (4.8)$$

where k is the thermal conductivity, A_c is the cross sectional area, and ΔL is the length between adjacent nodes. This conductance is used to define heat flow between adjacent nodes on the surface of the copper tubing, therefore, the cross sectional area available for heat transfer, A_c , is given by:

$$A_c = \pi(R_{\text{outer}}^2 - R_{\text{inner}}^2) = 0.134 \text{ cm}^2 \quad (4.9)$$

The thermal conductivity of copper ($k = 401 \text{ W/m-K}$) was used for all calculations involving K_1 .

The second conductance is used in the calculation of the convective heat transfer between nodes on the surface of the copper tubing and corresponding liquid nodes located within the copper tubing. It is denoted as K_2 and is given as:

$$K_2 = h_c A_s \quad (4.10)$$

where h_c is the convective heat transfer coefficient due to water flow through the tube, and A_s is the surface area over which the heat transfer occurs. The given value of h_c for turbulent water flow through the tube is given by Garrett (1992) as $12600 \text{ W/m}^2\text{-K}$. The surface area over which the heat transfer occurs is based on the inner radius of the copper tubing and is given by:

$$A_s = 2\pi R_{\text{inner}} \Delta L \quad (4.11)$$

where ΔL is identical in value to that used in determining K_1 .

The third conductance form, K_3 , is used in the determination of the convective heat transfer between adjacent fluid nodes within the tube. It is given as:

$$K_3 = w_f C_f \quad (4.12)$$

where w_f is the fluid weight flow and c_f is its specific heat capacity. This value was calculated for a variety of flow rates ($w_f = 68 \text{ kg/hr}$, 149.7 kg/hr , 272.2 kg/hr , 362.9 kg/hr) through the tubes, and the thermal performance of each flow rate was analyzed. A constant value of 4.182 kJ/kg-K was used for the specific heat capacity of water in all calculations of K_3 .

The fourth conductance term necessary to analyze the thermal model is used in the calculation of the heat transfer from the surface of the tubing, to the surrounding environment via both the prime and fin surfaces. This term is the most difficult of the conductance forms to determine, and requires a return to the principles presented in the single stack cold plate analysis. Equation (2.33) is written in the form of the general heat equation used by the thermal analysis software in its calculations where;

$$K_4 = Y_{in} = Y_{in,p} + Y_{in,f} \quad (4.13)$$

and

$$\theta_s = (T_s - T_e) = (T_1 - T_2) \quad (4.14)$$

Therefore, the fourth conduction term is the sum of the prime surface and fin input admittances, and the temperature difference is given in terms of a temperature excess at the base of the fin. Applying this conductance form to the HPX requires consideration of the length, ΔL , between adjacent nodes. The length between adjacent nodes determines both the number of fins, and the amount of prime surface associated with each node. The ΔL in the analysis model is varied with location along the copper tubing as shown in Appendix C. Once ΔL is determined, the resulting number of fins, n , and prime surface area may be used with the determined value of h to give;

$$K_4 = hn(W - \delta)L + nY_o \tanh(mb_2) \quad (4.15)$$

where $n = \Delta L/W$.

Once the model provides the required data to satisfy the K-value equations, the solution of the thermal conductance matrix is straightforward and ideally suited to a spreadsheet

application. The calculated K-values are then used as input to the thermal analyzer to form a series of node connection data. The spreadsheet calculations and resulting node connection data for each case considered is provided in Appendix D. In the HPX model, the tube water inlet temperature and the oscillating air temperature are assigned constant values. Additionally, as mentioned earlier, 144 nodes were assigned to locations along the copper tubing (nodes 1-144) and 144 corresponding nodes (nodes 145-288) were assigned to the centerline liquid temperature within the tubing.

In the initial development, it was assumed that all fin pairs were shared equally ($\theta_{b1} = \theta_{b2}$). This condition is the easiest to model, because fin sharing node pairs have equivalent values of K_f assigned to them. This model results in the assigning of 46 distinct K-values and is used in the establishment of the initial temperature excess to be used in subsequent iterations. The computed temperature excess variation with location was then used in the calculation of the nodal fin sharing pair R_f values using Equation (2.26). Once the R_f values were known, the values of b_2 and b_1 were calculated using Equation (2.30). The assignment of specific, non uniform fin lengths (b_1 , b_2) along the tubing surface, required the value of K_f to be modified for each node. This was required based on the fact that now unique values of $Y_{in,f}$ existed for each node. Applying the K-value equations to each

node, for this model, resulted in the generation of 252 unique values of K_4 . These values were then entered into the thermal analysis program. The thermal performance for a variety of flow rates ($w_F = 68$ kg/hr, 149.7 kg/hr, 272.2 kg/hr, 362.9 kg/hr) was also analyzed for this new model. These analyses provided adequate data for a performance prediction of the TALSR.

V. EFFECTS OF TEMPERATURE EXCESS RATIO VARIATIONS

The base temperature excess (θ_b), as defined earlier, is the difference between the temperature at the base of the fin and the temperature of the coolant fluid, given by;

$$\theta_b = T_b - T_\infty \quad (5.1)$$

It represents the maximum driving potential for convective heat transfer across the fin. Hence, the maximum rate at which a fin could dissipate energy is the rate that would exist if the entire fin surface were at the base temperature. However, because any fin is characterized by a finite conduction resistance, a temperature gradient will exist along the fin and the rate of energy dissipation will be less than the maximum rate. Thus, a convenient measure for the thermal performance of a particular fin is provided by the fin efficiency, η , defined as [Incropera and DeWitt (1981)];

$$\eta = q_f/q_{ideal} \quad (5.2)$$

where

$$\begin{aligned} q_f &= q_b = Y_o \theta_b \tanh(mb_2) \\ q_{ideal} &= hPb\theta_b \end{aligned} \quad (5.3)$$

for a rectangular fin of uniform cross sectional area with an

adiabatic tip. The equation for q_{ideal} represents the heat convectively transferred from a fin of height b to the environment if $\theta = \theta_b$ at all points along the fin. Combining Equations (5.2) and Equation (5.3) results in a conventional fin efficiency given as;

$$\eta = \tanh(mb)/mb \quad (5.4)$$

where m is as given in Equation (2.9), and b is the total height of the fin. The application of this parameter to cold plates with asymmetric heat loading, such as those modeled in the HPX, will result in individual efficiencies being identified for each fin subdivision (b_1 and b_2). In addition, an overall efficiency for the total fin height b is also calculable.

A simplified cold plate configuration will be used as the model for this analysis in order to provide clarity to the development. The model will consist of a single fin with a total height b , and known heat transfer characteristics for the surrounding flow geometry. Therefore, the only required data to complete the thermal analysis of the model is the prime surface temperature on either end of the fin. Once this value is known, R_s , b_1 and b_2 are easily determined using Equations (2.26) through (2.28).

A conventional derivation of the efficiencies for each fin subdivision is easily determined by substituting the

values of b_1 and b_2 in for the total fin height, b , in Equation (5.3). A conventional overall efficiency of the entire fin height, b , can also be calculated using

$$\eta_{\text{overall}} = (q_{\text{actual}b1} + q_{\text{actual}b2}) / (q_{\text{ideal}b1} + q_{\text{ideal}b2}) \quad (5.5)$$

which algebraically reduces to

$$\eta_{\text{overall}} = \eta_{b1} / (1 + (b_2/b_1 R_0)) + \eta_{b2} / (1 + (b_1 R_0/b_2)) \quad (5.6)$$

The value of R_0 used in determining Equation (5.6) is based upon the average temperature change across the fin as given by

$$R_0 = (\Delta T/2 + T_{\text{avg}} - T_e) / (-\Delta T/2 + T_{\text{avg}} - T_e) \quad (5.7)$$

where

$$\Delta T = (T_{b1} - T_{b2})$$

$$\text{and} \quad T_{\text{avg}} = (T_{b1} + T_{b2}) / 2 \quad (5.8)$$

The use of this definition for R_0 , contrary to one based solely on T_{b1} or T_{b2} , provides an accurate representation of the response in fin efficiency due to variations in base temperature excess across the fin.

These variations in fin efficiency were then plotted versus the difference in base temperature excesses as shown in Figure 8.

A more practical definition for fin efficiency would result in the efficiency of each segment increasing with the

Conventional Efficiencies vs. Temperature Excess Difference

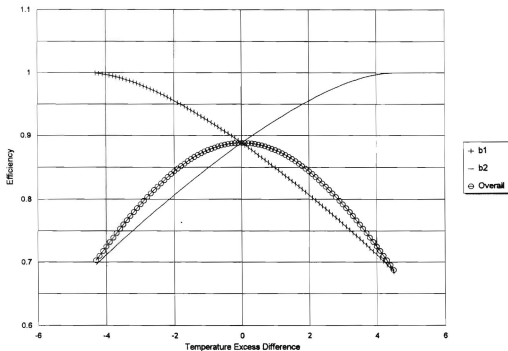


Figure 8: Graphical representation of conventional efficiency variation with changing base temperature excess difference

length of the respective fin heights. For this development the overall efficiency is defined as

$$\eta_{\text{overall}} = \eta_1 + \eta_2 \quad (5.9)$$

where η_1 and η_2 are given by

$$\eta_i = q_{fi}/q_{\text{ideal}} = Y_o \theta_{bi} \tanh(mb_i)/q_{\text{ideal}} \quad (5.10)$$

and $i = 1$ or 2 . The value of q_{ideal} for this development is given as

$$q_{\text{ideal}} = hPb\theta_{bi} \quad (5.11)$$

where θ_{bi} is chosen as the maximum value of the magnitude of either θ_{b1} or θ_{b2} . For example, for $R_0 \geq 1$ it follows from Equation (5.11) that $q_{\text{ideal}} = hPb\theta_{b1}$. After substitution of this result into Equation (5.10) and combining with Equation (5.11), it is found that for $R_0 \geq 1$ overall efficiency is given as

$$\eta_{\text{overall}} = (\tanh(mb_1)/(mb)) + (\tanh(mb_2)/(mbR_0)) \quad (5.12)$$

Similarly for $R_0 \leq 1$

$$\eta_{\text{overall}} = (R_0(\tanh(mb_1)) / (mb)) + (\tanh(mb_2) / (mb)) \quad (5.13)$$

These equations are seen to be equal for the case where $R_0 = 1$. A graphical representation of the relationship between the individual fin efficiencies and the practical overall efficiency is presented in Figure 9.

Practical Efficiencies vs. Temperature Excess Difference

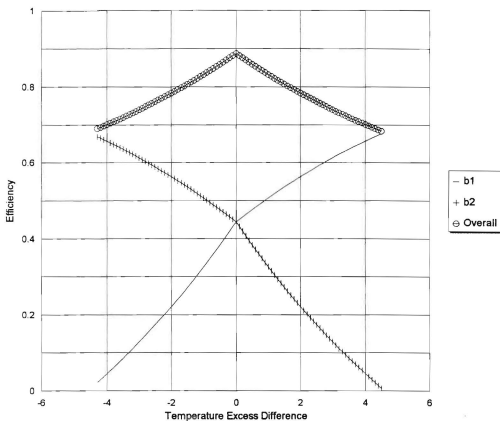


Figure 9 : Relationship of practical efficiencies with variations in base temperature excess difference

VI. RESULTS

An accurate design and performance analysis of the HPX requires critical assessment of the thermal analyzer output data, and representation of that data in a format that is easily understood and interpreted.

A. PROGRAM OUTPUT

The thermal analyzer output data for the simplified model provides baseline temperature excess variations along the surface of the copper tubing and liquid centerline temperatures. The temperature output, for the nodes assigned to the tubing surface (1-144), indicated variations in temperature along the length of the tubing. This is due to variations in available heat transfer area, based on the assignment of node locations and resultant fin allocation. Additionally, the liquid centerline temperature showed a gradually increasing trend from inlet to outlet which is consistent with the expected results.

Analysis of the complex model resulted in similar temperature variations for both the tubing and liquid centerline temperatures, with only slight differences in actual temperature values from those obtained using the simplified model. Complex model analysis for different flow rates indicated that temperature values along the surface of the tube, and throughout the liquid in the tube were largely

dependent on the mass flow rate. For an increasing mass flow rate, this dependence resulted in lower tube surface temperatures, fluid outlet temperature, and overall change in fluid temperature as it passed through the heat exchanger. A summary of the output nodal temperatures for each model considered is found in Appendix E. The results were consistent with expectations and are presented graphically in Figures (10) and (11). In addition, the thermal analysis provided the necessary data to calculate the overall heat transfer for each mass flow rate, using;

$$q = (dm/dt)c_f \Delta T \quad (6.1)$$

where c_f is the specific heat capacity of water (4.182 kJ/kg-K). The heat transfer rate is plotted for each mass flow rate and is presented in Figure (12).

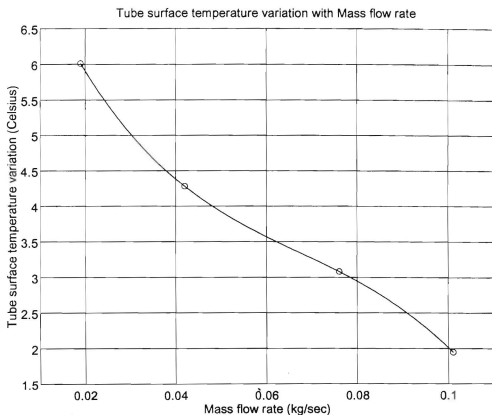


Figure 10: Graphical representation of Tube surface temperature variation with mass flow rate.

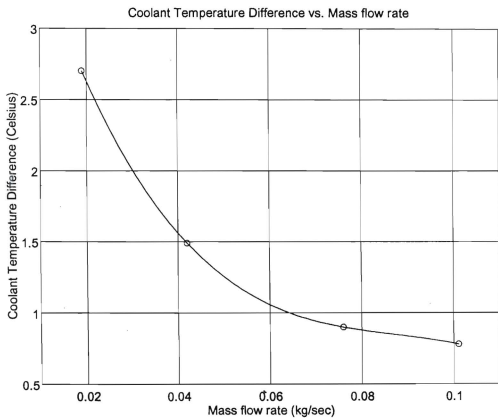


Figure 11: Graphical representation of Coolant Temperature difference ($T_{\text{outlet}} - T_{\text{inlet}}$) variation with mass flow rate.

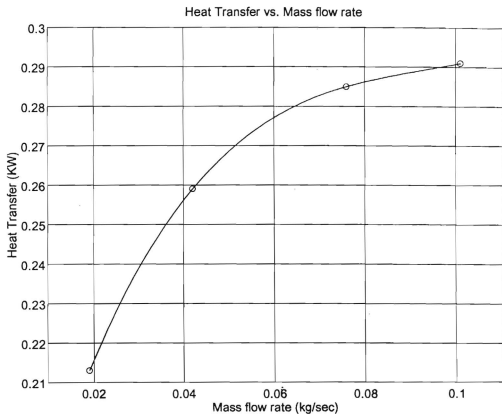


Figure 12: Graphical representation of Heat Transfer with mass flow rate.

VII. SUMMARY AND CONCLUSIONS

The results of this investigation into the thermal performance of the HPX leads to several conclusions. These conclusions are broken down into the following topics: design effectiveness, effectiveness of applying single stack cold plate analysis, effectiveness of computer modeling, and performance analysis validity.

A. DESIGN EFFECTIVENESS

Design effectiveness consideration was based solely on the physical configuration of the HPX. The use of copper tubing bent into a serpentine pattern and then soldered or furnace brazed on a screen of copper fins results in a small and inefficient contact surface between the tubing and the fins. A better design and the one actually used to model the HPX would inlay the copper tubing into the screen of copper fins. This would result in a much higher effective surface area for heat transfer than the current configuration. The success of applying a serpentine tubing pattern for this application as opposed to the more conventional parallel pattern was not analyzed and provides a basis for future thesis work.

B. EFFECTIVENESS OF SINGLE STACK COLD PLATE ANALYSIS

An analysis based on the work of Pieper and Kraus (1995) indicated distinct fin sharing characteristics along the length of copper tubing based on the temperature excess ratio across each shared fin. This resulted in small variations in computed temperatures along the length of the tubing compared to a model subjected to equal operating temperatures on the right and left base surfaces. The magnitude of this variation is dependent on the scale of the application and could result in large values for a large scale application similar to the WyoDak facility in Gillette, Wyoming. Thus, a single stack cold plate analysis would be very useful if the analysis required very accurate representations of temperature along the length of copper tubing in a large scale application. The variation in the magnitude of the temperature variation based on the scale of the application provides a basis for further research.

C. EFFECTIVENESS OF COMPUTER MODELING

Computer modeling provided a convenient and reliable method of calculating the multiple equations created as the result of a detailed analysis of the HPX heat exchanger. The use of computer modeling provides flexibility in the analysis of various heat transfer parameters. The model used for the analysis of the HPX consisted of air flowing over fins,

heating water flowing through the copper tubing. Once these initial inputs are set up and the requisite files built within the thermal analysis software, it becomes simply a matter of replacing the initial model values with new values to evaluate a new system. Therefore, various working fluids with widely varying properties and different internal heat exchanger geometries can be analyzed very easily. This permits the convenient application of specific conditions for a given application, thus saving money and laborious hours in the lab building and evaluating various configurations for a given application. However, once a given application is chosen through the use of computer modeling, extensive testing and empirical data collection is required to validate the computer generated results. For the HPX model analyzed in this thesis, the collection of empirical results through testing and subsequent comparison with the computer generated results is still required.

D. VALIDITY OF PERFORMANCE ANALYSIS

The performance analysis of the HPX required the determination of the convection coefficient, h , and the conductance matrix. These values were determined using numerical analysis techniques.

In the absence of strict correlations for oscillatory flow convection coefficients, a steady flow Nusselt correlation was assumed to provide a suitable representation

of heat transfer in the channel. This is a major assumption, but not without merit based on the argument provided in the thermal performance section. However, a more representative analysis could be made through the application of a Nusselt correlation based solely on acoustically oscillated flow analysis. The derivation of these correlations is currently being pursued through a variety of research, including work conducted at Naval Postgraduate School.

The conductance matrix was used to determine the temperature distribution along the length of the copper tubing. This distribution of temperatures was reasonable and behaved predictably with changes in the mass flow rate of water through the tubing. These temperatures were then used to calculate values for the temperature excess ratio, and subsequently determine the respective lengths of b_1 and b_2 . A new temperature distribution was then found based on this cold plate analysis. This provided an adequate representation of the temperature variation along the length of the tubing, however a more accurate distribution could be acquired by repetition of the analysis for each new set of temperature distribution data acquired. This could continue until a user-specified variation limit between successive attempts was met, thus satisfying a predetermined level of accuracy.

APPENDIX A. MURRAY-GARDNER ASSUMPTIONS

The Murray-Gardner assumptions are:

1. The heat flow in the fin and its temperatures remain constant with time.
2. The fin material is homogenous, its thermal conductivity is the same in all directions, and it remains constant.
3. The heat transfer coefficient to the fin is constant and uniform over the entire surface of the fin.
4. The temperature of the medium surrounding the fin is uniform.
5. The fin thickness is so small compared with its height that temperature gradients across the fin thickness may be neglected.
6. The temperature at the base of the fin is uniform.
7. There is no contact resistance where the base of the fin joins the prime surface.
8. There are no heat sources within the fin itself.
9. The heat transferred through the outermost edge of the fin is negligible compared with that leaving the fin through its lateral surface.
10. Heat transfer to or from the fin is proportional to the temperature excess between the fin and the surrounding medium.

APPENDIX B. TRANSFORMATION MATRIX DEVELOPMENT

A general application of linear, homogenous, second-order differential equation theory dictates that Equation (2.7) posses two independent solutions. These solutions, and the subsequent development of a linear transformation matrix to map conditions at the fin tip to conditions at the fin base were performed by Kraus et al. (1978). The solutions, designated $\lambda_1(x)$ and $\lambda_2(x)$, must satisfy the initial conditions at the base of the fin where $x = b$.

$$\begin{aligned}\lambda_1(b) &= 1; \lambda_1'(b) = 0, \\ \lambda_2(b) &= 0; \lambda_2'(b) = (1/kA_c(b))\end{aligned}\tag{B.1}$$

where the prime indicates a first derivative. The heat flow, $q(x)$, is always taken as positive from base to tip. Therefore, for longitudinal fins, $q(x)$ is given by;

$$q(x) = kA_c(x) (d\theta(x)/dx)\tag{B.2}$$

Thus, the solutions λ_1 and λ_2 can be used to assemble the expressions for the temperature excess $\theta(x)$ and heat flow $q(x)$, at any point in the fin in terms of θ_b and q_b at the fin base;

$$\theta(x) = \theta_b \lambda_1(x) + q_b \lambda_2(x) \quad (\text{B.3})$$

$$q(x) = kA_c(x) [\theta_b \lambda_1'(x) + q_b \lambda_2'(x)] \quad (\text{B.4})$$

In matrix form, Equations (B.3) and (B.4) become;

$$\begin{bmatrix} \theta(x) \\ q(x) \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & kA_c(x) \end{bmatrix} \begin{bmatrix} \lambda_1(x) & \lambda_2(x) \\ \lambda_1'(x) & \lambda_2'(x) \end{bmatrix} \begin{bmatrix} \theta_b \\ q_b \end{bmatrix} \quad (\text{B.5})$$

The thermal transmission matrix is the linear transformation generated when x is set equal to a , where a equals either the fin height or zero depending on the origin of the height coordinate;

$$\begin{bmatrix} \theta_a \\ q_a \end{bmatrix} = \Gamma \begin{bmatrix} \theta_b \\ q_b \end{bmatrix} = \begin{bmatrix} \gamma_{11} & \gamma_{12} \\ \gamma_{21} & \gamma_{22} \end{bmatrix} \begin{bmatrix} \theta_b \\ q_b \end{bmatrix} \quad (\text{B.6})$$

where

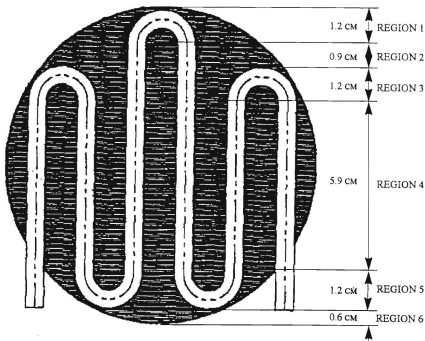
$$\begin{aligned} \gamma_{11} &= \lambda_1(a) \\ \gamma_{12} &= \lambda_2(a) \\ \gamma_{21} &= kA_c(a) \lambda_1'(a) \\ \gamma_{22} &= kA_c(a) \lambda_2'(a) \end{aligned} \quad (\text{B.7})$$

The elements of the thermal transmission matrix are called the thermal transmission parameters. To represent conditions at the fin base in terms of conditions at the fin tip, it is seen that;



$$\begin{bmatrix} \theta_b \\ q_b \end{bmatrix} = \Gamma^{-1} \begin{bmatrix} \theta_s \\ q_s \end{bmatrix} = \beta \begin{bmatrix} \theta_s \\ q_s \end{bmatrix} = \begin{bmatrix} \tau_{11} & \tau_{12} \\ \tau_{21} & \tau_{22} \end{bmatrix} \begin{bmatrix} \theta_s \\ q_s \end{bmatrix} \quad (\text{B.8})$$



where the matrix β is the inverse of the thermal transmission matrix and is called the inverse thermal transmission matrix. Its elements are designated as the inverse thermal transmission parameters.



APPENDIX C. NODAL MODELING DATA



REGION	LENGTH (CM)	# OF FINS	# OF NODES	FINS/NODE
1	1.2	22.6	3	7.53
2	0.9	16.2	2	8.1
3	1.2	22.6	3	7.53
4	5.9	110.7	16	6.92
5	1.2	22.6	3	7.53
6	0.6	11.3	0	N/A

	Tube Surface Nodes	Liquid Nodes
	21 - 23	165 - 167
	5 - 20	149 - 164
	1 - 4	145 - 148
	24 - 26	168 - 170
	27 - 42	171 - 186
	43 - 45	187 - 189

	Tube Surface Nodes	Liquid Nodes
	70 - 72	214 - 216
	68 - 69	212 - 213
	65 - 67	209 - 211
	49 - 64	193 - 208
	46 - 48	190 - 192
	73 - 75	217 - 219
	76 - 77	220 - 221
	78 - 80	222 - 220
	81 - 96	223 - 238
	97 - 99	239 - 242

	Tube Surface Nodes	Liquid Nodes
	119 - 121	263 - 265
	103 - 118	247 - 262
	100 - 102	244 - 246
	122 - 124	266 - 268
	125 - 140	269 - 284
	141 - 144	284 - 288

APPENDIX D. SPREADSHEET K-VALUE DETERMINATION AND NODE CONNECTION DATA

The general procedure for each case is as follows:

1. Use node location and applicable equations to determine fin length associated with that particular node.
2. Determine K-Values using spreadsheet application.
3. Input K-Values into user friendly spreadsheet that associates each K-Value with a particular node and branch.
4. Once K-Values are input into thermal analysis software, an easily read summary of the individual branches and their associated conductances is produced.

TASS GENERAL INPUT MENU - SI Units

(1) Case Title:

TALSR(METRIC)---- RUN 1. SIMPLE MODEL CASE

(2) Nodes	288
(3) Constant Temperatures	2
(4) Unique Exponents	0
(5) Temperature Dependent Conductances	0
(6) Temperature Dependent Heat Inputs	0
(7) Computational Accuracy	.0100
(8) Starting Temperature	25.0

Are these inputs correct (Y/N) ? Y

CONDUCTIVITY	EFFECTIVE FIN LENGTH (L) IN CENTIMETERS
K1	N/A
K2	N/A
K3	N/A
K4	N/A
K5	N/A
K6	0.5715
K7	0.094
K8	0.269
K9	0.414
K10	0.531
K11	0.62
K12	0.681
K13	0.716
K14	0.732
K15	N/A
K16	N/A
K17	N/A
K18	0.552
K19	0.404
K20	0.148
K21	1.0185
K22	0.748
K23	0.592
K24	0.888
K25	0.55
K26	1.4655
K27	0.925
K28	0.6125
K29	N/A
K30	N/A
K31	N/A
K32	0.5715
K33	N/A
K34	N/A
K35	N/A
K36	N/A
K37	N/A
K38	N/A
K39	0.5715
K40	2.907
K41	N/A
K42	2.482
K43	1.84
K44	1.119
K45	0.359
K46	N/A

17.554

MEET DATA									
Item	Channel Width (in)	Effective Diameter (cm)	Heat Transfer Coefficient (h)	Yin (f)	Prandtl Number	Outer pipe diameter (cm)	Inner pipe diameter (cm)	Pipe Area (sq cm)	K - Value (W/mK)
K1	0.318	0.015	0.053	431.00	1900.00	0.707	0.635	0.483	0.134
K2									
K3									
K4									
K5									
K6									
K7									
K8									
K9									
K10									
K11									
K12									
K13									
K14									
K15									
K16									
K17									
K18									
K19									
K20									
K21									
K22									
K23									
K24									
K25									
K26									
K27									
K28									
K29									
K30									
K31									
K32									
K33									
K34									

BRANCH	NODE	TON	TAG	I, C, S	BRANCH	NODE	TON	TAG	I, C, S
1	1	2	1	K1	51	16	17	1	S9
2		145	4	K2	52		160	4	S10
3	2	3	1	S1	53		301	1	S11
4		146	4	S2	54		301	1	S38
5	3	4	1	S1	55	17	18	1	S9
6		147	4	S2	56		161	4	S10
7	4	5	1	K3	57		301	1	S11
8		148	4	S2	58		301	1	S34
9	5	6	1	K4	59	18	19	1	S9
10		149	4	K5	60		162	4	S10
11		301	1	K6	61		301	1	S11
12	6	7	1	S9	62		301	1	S30
13		150	4	S10	63	19	20	1	S9
14		301	1	S11	64		163	4	S10
15	7	8	1	S9	65		301	1	S11
16		151	4	S10	66		301	1	S26
17		301	1	S11	67	20	21	1	K15
18		301	1	K7	68		164	4	S10
19	8	9	1	S9	69		301	1	S11
20		152	4	S10	70		301	1	S22
21		301	1	S11	71	21	22	1	K16
22		301	1	K8	72		165	4	K17
23	9	10	1	S9	73		301	1	K18
24		153	4	S10	74	22	23	1	S71
25		301	1	S11	75		166	4	S72
26		301	1	K9	76		301	1	K19
27	10	11	1	S9	77	23	24	1	S71
28		154	4	S10	78		167	4	S72
29		301	1	S11	79		301	1	K20
30		301	1	K10	80	24	25	1	S71
31	11	12	1	S9	81		168	4	S72
32		155	4	S10	82		301	1	K21
33		301	1	S11	83		301	1	S79
34		301	1	K11	84	25	26	1	S71
35	12	13	1	S9	85		169	4	S72
36		156	4	S10	86		301	1	K22
37		301	1	S11	87		301	1	S76
38		301	1	K12	88	26	27	1	S67
39	13	14	1	S9	89		170	4	S72
40		157	4	S10	90		301	1	K23
41		301	1	S11	91		301	1	S73
42		301	1	K13	92	27	28	1	S9
43	14	15	1	S9	93		171	4	S10
44		158	4	S10	94		301	1	S11
45		301	1	S11	95		301	1	S11
46		301	1	K14	96	28	29	1	S9
47	15	16	1	S9	97		172	4	S10
48		159	4	S10	98		301	1	S11
49		301	1	S11	99		301	1	S11
50		301	1	S42	100	29	30	1	S9

BRANCH	NODE	TON	TAG	I. C. S	BRANCH	NODE	TON	TAG	I. C. S
101		173	4	S10	151		301	1	S11
102		301	1	S11	152	42	43	1	S67
103		301	1	S11	153		186	4	S10
104	30	31	1	S9	154		301	1	S11
105		174	4	S10	155		301	1	S11
106		301	1	S11	156	43	44	1	S71
107		301	1	S11	157		187	4	S72
108	31	32	1	S9	158		301	1	S73
109		175	4	S10	159		301	1	K24
110		301	1	S11	160	44	45	1	S71
111		301	1	S11	161		188	4	S72
112	32	33	1	S9	162		301	1	S76
113		176	4	S10	163		301	1	K25
114		301	1	S11	164	45	46	1	S71
115		301	1	S11	165		189	4	S72
116	33	34	1	S9	166		301	1	S79
117		177	4	S10	167	46	47	1	S71
118		301	1	S11	168		190	4	S72
119		301	1	S11	169		301	1	K26
120	34	35	1	S9	170		301	1	S79
121		178	4	S10	171	47	48	1	S71
122		301	1	S11	172		191	4	S72
123		301	1	S11	173		301	1	K27
124	35	36	1	S9	174		301	1	S76
125		179	4	S10	175	48	49	1	S67
126		301	1	S11	176		192	4	S72
127		301	1	S11	177		301	1	K28
128	36	37	1	S9	178		301	1	S73
129		180	4	S10	179	49	50	1	S9
130		301	1	S11	180		193	4	S10
131		301	1	S11	181		301	1	S11
132	37	38	1	S9	182		301	1	S11
133		181	4	S10	183	50	51	1	S9
134		301	1	S11	184		194	4	S10
135		301	1	S11	185		301	1	S11
136	38	39	1	S9	186		301	1	S11
137		182	4	S10	187	51	52	1	S9
138		301	1	S11	188		195	4	S10
139		301	1	S11	189		301	1	S11
140	39	40	1	S9	190		301	1	S11
141		183	4	S10	191	52	53	1	S9
142		301	1	S11	192		196	4	S10
143		301	1	S11	193		301	1	S11
144	40	41	1	S9	194		301	1	S11
145		184	4	S10	195	53	54	1	S9
146		301	1	S11	196		197	4	S10
147		301	1	S11	197		301	1	S11
148	41	42	1	S9	198		301	1	S11
149		185	4	S10	199	54	55	1	S9
150		301	1	S11	200		198	4	S10

BRANCH	NODE	TON	TAG	I, C, S	BRANCH	NODE	TON	TAG	I, C, S
201		301	1	S11	251	67	68	1	K35
202		301	1	S11	252		211	4	K36
203	55	56	1	S9	253		301	1	S245
204		199	4	S10	254		301	1	S82
205		301	1	S11	255	68	69	1	K37
206		301	1	S11	256		212	4	K38
207	56	57	1	S9	257		301	1	K39
208		200	4	S10	258		301	1	K40
209		301	1	S11	259	69	70	1	K41
210		301	1	S11	260		213	4	S256
211	57	58	1	S9	261		301	1	S257
212		201	4	S10	262		301	1	K42
213		301	1	S11	263	70	71	1	S71
214		301	1	S11	264		214	4	S72
215	58	59	1	S9	265		301	1	S73
216		202	4	S10	266		301	1	K43
217		301	1	S11	267	71	72	1	S71
218		301	1	S11	268		215	4	S72
219	59	60	1	S9	269		301	1	S76
220		203	4	S10	270		301	1	K44
221		301	1	S11	271	72	73	1	S71
222		301	1	S11	272		216	4	S72
223	60	61	1	S9	273		301	1	S79
224		204	4	S10	274		301	1	K45
225		301	1	S11	275	73	74	1	S71
226		301	1	S11	276		217	4	S72
227	61	62	1	S9	277		301	1	S274
228		205	4	S10	278		301	1	S79
229		301	1	S11	279	74	75	1	S71
230		301	1	S11	280		218	4	S72
231	62	63	1	S9	281		301	1	S270
232		206	4	S10	282		301	1	S76
233		301	1	S11	283	75	76	1	S259
234		301	1	S11	284		219	4	S72
235	63	64	1	S9	285		301	1	S266
236		207	4	S10	286		301	1	S73
237		301	1	S11	287	76	77	1	S255
238		301	1	S11	288		220	4	S256
239	64	65	1	K29	289		301	1	S262
240		208	4	S10	290		301	1	S257
241		301	1	S11	291	77	78	1	S251
242		301	1	S11	292		221	4	S256
243	65	66	1	K30	293		301	1	S258
244		209	4	K31	294		301	1	S257
245		301	1	K32	295	78	79	1	S247
246		301	1	S90	296		222	4	S252
247	66	67	1	K33	297		301	1	S82
248		210	4	K34	298		301	1	S245
249		301	1	S245	299	79	80	1	S243
250		301	1	S86	300		223	4	S248

BRANCH	NODE	TON	TAG	I. C. S	BRANCH	NODE	TON	TAG	I. C. S
301		301	1	S86	352		236	4	S10
302		301	1	S245	353		301	1	S11
303	80	81	1	S239	354		301	1	S11
304		224	4	S244	355	93	94	1	S9
305		301	1	S90	356		237	4	S10
306		301	1	S245	357		301	1	S11
307	81	82	1	S9	358		301	1	S11
308		225	4	S10	359	94	95	1	S9
309		301	1	S11	360		238	4	S10
310		301	1	S11	361		301	1	S11
311	82	83	1	S9	362		301	1	S11
312		226	4	S10	363	95	96	1	S9
313		301	1	S11	364		239	4	S10
314		301	1	S11	365		301	1	S11
315	83	84	1	S9	366		301	1	S11
316		227	4	S10	367	96	97	1	S67
317		301	1	S11	368		240	4	S10
318		301	1	S11	369		301	1	S11
319	84	85	1	S9	370		301	1	S11
320		228	4	S10	371	97	98	1	S71
321		301	1	S11	372		241	4	S72
322		301	1	S11	373		301	1	S73
323	85	86	1	S9	374		301	1	S177
324		229	4	S10	375	98	99	1	S71
325		301	1	S11	376		242	4	S72
326		301	1	S11	377		301	1	S76
327	86	87	1	S9	378		301	1	S173
328		230	4	S10	379	99	100	1	S71
329		301	1	S11	380		243	4	S72
330		301	1	S11	381		301	1	S79
331	87	88	1	S9	382		301	1	S169
332		231	4	S10	383	100	101	1	S71
333		301	1	S11	384		244	4	S72
334		301	1	S11	385		301	1	S79
335	88	89	1	S9	386	101	102	1	S71
336		232	4	S10	387		245	4	S72
337		301	1	S11	388		301	1	S163
338		301	1	S11	389		301	1	S76
339	89	90	1	S9	390	102	103	1	S67
340		233	4	S10	391		246	4	S72
341		301	1	S11	392		301	1	S159
342		301	1	S11	393		301	1	S73
343	90	91	1	S9	394	103	104	1	S9
344		234	4	S10	395		247	4	S10
345		301	1	S11	396		301	1	S11
346		301	1	S11	397		301	1	S11
347	91	92	1	S9	398	104	105	1	S9
348		235	4	S10	399		248	4	S10
349		301	1	S11	400		301	1	S11
350		301	1	S11	401		301	1	S11
351	92	93	1	S9	402	105	106	1	S9

BRANCH	NODE	TON	TAG	I. C. S	BRANCH	NODE	TON	TAG	I. C. S
403		249	4	S10	453		301	1	S11
404		301	1	S11	454	118	119	1	S67
405		301	1	S11	455		262	4	S10
406	106	107	1	S9	456		301	1	S11
407		250	4	S10	457		301	1	S11
408		301	1	S11	458	119	120	1	S71
409		301	1	S11	459		263	4	S72
410	107	108	1	S9	460		301	1	S73
411		251	4	S10	461		301	1	S90
412		301	1	S11	462	120	121	1	S71
413		301	1	S11	463		264	4	S72
414	108	109	1	S9	464		301	1	S76
415		252	4	S10	465		301	1	S86
416		301	1	S11	466	121	122	1	S71
417		301	1	S11	467		265	4	S72
418	109	110	1	S9	468		301	1	S79
419		253	4	S10	469		301	1	S82
420		301	1	S11	470	122	123	1	S71
421		301	1	S11	471		266	4	S72
422	110	111	1	S9	472		301	1	S79
423		254	4	S10	473	123	124	1	S71
424		301	1	S11	474		267	4	S72
425		301	1	S11	475		301	1	S76
426	111	112	1	S9	476	124	125	1	S67
427		255	4	S10	477		268	4	S72
428		301	1	S11	478		301	1	S73
429		301	1	S11	479	125	126	1	S9
430	112	113	1	S9	480		269	4	S10
431		256	4	S10	481		301	1	S22
432		301	1	S11	482		301	1	S11
433		301	1	S11	483	126	127	1	S9
434	113	114	1	S9	484		270	4	S10
435		257	4	S10	485		301	1	S26
436		301	1	S11	486		301	1	S11
437		301	1	S11	487	127	128	1	S9
438	114	115	1	S9	488		271	4	S10
439		258	4	S10	489		301	1	S30
440		301	1	S11	490		301	1	S11
441		301	1	S11	491	128	129	1	S9
442	115	116	1	S9	492		272	4	S10
443		259	4	S10	493		301	1	S34
444		301	1	S11	494		301	1	S11
445		301	1	S11	495	129	130	1	S9
446	116	117	1	S9	496		273	4	S10
447		260	4	S10	497		301	1	S38
448		301	1	S11	498		301	1	S11
449		301	1	S11	499	130	131	1	S9
450	117	118	1	S9	500		274	4	S10
451		261	4	S10	501		301	1	S42
452		301	1	S11	502		301	1	S11

BRANCH	NODE	TON	TAG	I, C, S	BRANCH	NODE	TON	TAG	I, C, S
503	131	132	1	S9	553				
504		275	4	S10	554				
505		301	1	S46	555				
506		301	1	S11	556				
507	132	133	1	S9	557				
508		276	4	S10	558				
509		301	1	S42	559				
510		301	1	S11	560				
511	133	134	1	S9	561				
512		277	4	S10	562				
513		301	1	S38	563				
514		301	1	S11	564				
515	134	135	1	S9	565				
516		278	4	S10	566				
517		301	1	S34	567				
518		301	1	S11	568				
519	135	136	1	S9	569				
520		279	4	S10	570				
521		301	1	S30	571				
522		301	1	S11	572				
523	136	137	1	S9	573				
524		280	4	S10	574				
525		301	1	S26	575				
526		301	1	S11	576				
527	137	138	1	S9	577				
528		281	4	S10	578				
529		301	1	S22	579				
530		301	1	S11	580				
531	138	139	1	S9	581				
532		282	4	S10	582				
533		301	1	S18	583				
534		301	1	S11	584				
535	139	140	1	S9	585				
536		283	4	S10	586				
537		301	1	S11	587				
538	140	141	1	S7	588				
539		284	4	S10	589				
540		301	1	S11	590				
541	141	142	1	S1	591				
542		285	4	S2	592				
543	142	143	1	S1	593				
544		286	4	S2	594				
545	143	144	1	S1	595				
546		287	4	S2	596				
547	144	288	4	S2	597				
548					598				
549					599				
550					600				
551					601				
552					602				

BRANCH	NODE	TON	TAG	I, C, S	BRANCH	NODE	TON	TAG	I, C, S
701	145	302	5	K46	751	195	194	5	S701
702	146	145	5	S701	752	196	195	5	S701
703	147	146	5	S701	753	197	196	5	S701
704	148	147	5	S701	754	198	197	5	S701
705	149	148	5	S701	755	199	198	5	S701
706	150	149	5	S701	756	200	199	5	S701
707	151	150	5	S701	757	201	200	5	S701
708	152	151	5	S701	758	202	201	5	S701
709	153	152	5	S701	759	203	202	5	S701
710	154	153	5	S701	760	204	203	5	S701
711	155	154	5	S701	761	205	204	5	S701
712	156	155	5	S701	762	206	205	5	S701
713	157	156	5	S701	763	207	206	5	S701
714	158	157	5	S701	764	208	207	5	S701
715	159	158	5	S701	765	209	208	5	S701
716	160	159	5	S701	766	210	209	5	S701
717	161	160	5	S701	767	211	210	5	S701
718	162	161	5	S701	768	212	211	5	S701
719	163	162	5	S701	769	213	212	5	S701
720	164	163	5	S701	770	214	213	5	S701
721	165	164	5	S701	771	215	214	5	S701
722	166	165	5	S701	772	216	215	5	S701
723	167	166	5	S701	773	217	216	5	S701
724	168	167	5	S701	774	218	217	5	S701
725	169	168	5	S701	775	219	218	5	S701
726	170	169	5	S701	776	220	219	5	S701
727	171	170	5	S701	777	221	220	5	S701
728	172	171	5	S701	778	222	221	5	S701
729	173	172	5	S701	779	223	222	5	S701
730	174	173	5	S701	780	224	223	5	S701
731	175	174	5	S701	781	225	224	5	S701
732	176	175	5	S701	782	226	225	5	S701
733	177	176	5	S701	783	227	226	5	S701
734	178	177	5	S701	784	228	227	5	S701
735	179	178	5	S701	785	229	228	5	S701
736	180	179	5	S701	786	230	229	5	S701
737	181	180	5	S701	787	231	230	5	S701
738	182	181	5	S701	788	232	231	5	S701
739	183	182	5	S701	789	233	232	5	S701
740	184	183	5	S701	790	234	233	5	S701
741	185	184	5	S701	791	235	234	5	S701
742	186	185	5	S701	792	236	235	5	S701
743	187	186	5	S701	793	237	236	5	S701
744	188	187	5	S701	794	238	237	5	S701
745	189	188	5	S701	795	239	238	5	S701
746	190	189	5	S701	796	240	239	5	S701
747	191	190	5	S701	797	241	240	5	S701
748	192	191	5	S701	798	242	241	5	S701
749	193	192	5	S701	799	243	242	5	S701
750	194	193	5	S701	800	244	243	5	S701

BRANCH	NODE	TON	TAG	I, C, S	BRANCH	NODE	TON	TAG	I, C, S
801	245	244	5	S701	851				
802	246	245	5	S701	852				
803	247	246	5	S701	853				
804	248	247	5	S701	854				
805	249	248	5	S701	855				
806	250	249	5	S701	856				
807	251	250	5	S701	857				
808	252	251	5	S701	858				
809	253	252	5	S701	859				
810	254	253	5	S701	860				
811	255	254	5	S701	861				
812	256	255	5	S701	862				
813	257	256	5	S701	863				
814	258	257	5	S701	864				
815	259	258	5	S701	865				
816	260	259	5	S701	866				
817	261	260	5	S701	867				
818	262	261	5	S701	868				
819	263	262	5	S701	869				
820	264	263	5	S701	870				
821	265	264	5	S701	871				
822	266	265	5	S701	872				
823	267	266	5	S701	873				
824	268	267	5	S701	874				
825	269	268	5	S701	875				
826	270	269	5	S701	876				
827	271	270	5	S701	877				
828	272	271	5	S701	878				
829	273	272	5	S701	879				
830	274	273	5	S701	880				
831	275	274	5	S701	881				
832	276	275	5	S701	882				
833	277	276	5	S701	883				
834	278	277	5	S701	884				
835	279	278	5	S701	885				
836	280	279	5	S701	886				
837	281	280	5	S701	887				
838	282	281	5	S701	888				
839	283	282	5	S701	889				
840	284	283	5	S701	890				
841	285	284	5	S701	891				
842	286	285	5	S701	892				
843	287	286	5	S701	893				
844	288	287	5	S701	894				
845					895				
846					896				
847					897				
848					898				
849					899				
850					900				

TASS Branch Connection Summary in W/degC or Watts if Tag = 10

Brnh From To Tag Conduct	Brnh From To Tag Conduct	Brnh From To Tag Conduct
1 1 2 1.178E+01	57 17 301 1.840E-01	113 32 176 4.701E+00
2 1 145 4.576E+00	58 17 301 1.910E-01	114 32 301 1.840E-01
3 2 3 1.178E+01	59 18 19 1.146E+01	115 32 301 1.840E-01
4 2 146 4.576E+00	60 18 162 4.701E+00	116 33 34 1.146E+01
5 3 4 1.178E+01	61 18 301 1.840E-01	117 33 177 4.701E+00
6 3 147 4.576E+00	62 18 301 1.820E-01	118 33 301 1.840E-01
7 4 5 1.160E+01	63 19 20 1.146E+01	119 33 301 1.840E-01
8 4 148 4.576E+00	64 19 163 4.701E+00	120 34 35 1.146E+01
9 5 6 1.146E+01	65 19 301 1.840E-01	121 34 178 4.701E+00
10 5 149 4.701E+00	66 19 301 1.680E-01	122 34 301 1.840E-01
11 5 301 1.840E-01	67 20 21 1.129E+01	123 34 301 1.840E-01
12 6 7 1.146E+01	68 20 164 4.701E+00	124 35 36 1.146E+01
13 6 150 4.701E+00	69 20 301 1.840E-01	125 35 179 4.701E+00
14 6 301 1.840E-01	70 20 301 1.490E-01	126 35 301 1.840E-01
15 7 8 1.146E+01	71 21 22 1.115E+01	127 35 301 1.840E-01
16 7 151 4.701E+00	72 21 165 4.889E+00	128 36 37 1.146E+01
17 7 301 1.840E-01	73 21 301 1.900E-01	129 36 180 4.701E+00
18 7 301 1.240E-01	74 22 23 1.115E+01	130 36 301 1.840E-01
19 8 9 1.146E+01	75 22 166 4.889E+00	131 36 301 1.840E-01
20 8 152 4.701E+00	76 22 301 1.710E-01	132 37 38 1.146E+01
21 8 301 1.840E-01	77 23 24 1.115E+01	133 37 181 4.701E+00
22 8 301 1.490E-01	78 23 167 4.889E+00	134 37 301 1.840E-01
23 9 10 1.146E+01	79 23 301 1.320E-01	135 37 301 1.840E-01
24 9 153 4.701E+00	80 24 25 1.115E+01	136 38 39 1.146E+01
25 9 301 1.840E-01	81 24 168 4.889E+00	137 38 182 4.701E+00
26 9 301 1.680E-01	82 24 301 1.131E+00	138 38 301 1.840E-01
27 10 11 1.146E+01	83 24 301 1.320E-01	139 38 301 1.840E-01
28 10 154 4.701E+00	84 25 26 1.115E+01	140 39 40 1.146E+01
29 10 301 1.840E-01	85 25 169 4.889E+00	141 39 183 4.701E+00
30 10 301 1.820E-01	86 25 301 1.111E+00	142 39 301 1.840E-01
31 11 12 1.146E+01	87 25 301 1.710E-01	143 39 301 1.840E-01
32 11 155 4.701E+00	88 26 27 1.129E+01	144 40 41 1.146E+01
33 11 301 1.840E-01	89 26 170 4.889E+00	145 40 184 4.701E+00
34 11 301 1.910E-01	90 26 301 1.940E-01	146 40 301 1.840E-01
35 12 13 1.146E+01	91 26 301 1.900E-01	147 40 301 1.840E-01
36 12 156 4.701E+00	92 27 28 1.146E+01	148 41 42 1.146E+01
37 12 301 1.840E-01	93 27 171 4.701E+00	149 41 185 4.701E+00
38 12 301 1.970E-01	94 27 301 1.840E-01	150 41 301 1.840E-01
39 13 14 1.146E+01	95 27 301 1.840E-01	151 41 301 1.840E-01
40 13 157 4.701E+00	96 28 29 1.146E+01	152 42 43 1.129E+01
41 13 301 1.840E-01	97 28 172 4.701E+00	153 42 186 4.701E+00
42 13 301 1.100E+00	98 28 301 1.840E-01	154 42 301 1.840E-01
43 14 15 1.146E+01	99 28 301 1.840E-01	155 42 301 1.840E-01
44 14 158 4.701E+00	100 29 30 1.146E+01	156 43 44 1.115E+01
45 14 301 1.840E-01	101 29 173 4.701E+00	157 43 187 4.889E+00
46 14 301 1.101E+00	102 29 301 1.840E-01	158 43 301 1.900E-01
47 15 16 1.146E+01	103 29 301 1.840E-01	159 43 301 1.124E+00
48 15 159 4.701E+00	104 30 31 1.146E+01	160 44 45 1.115E+01
49 15 301 1.840E-01	105 30 174 4.701E+00	161 44 188 4.889E+00
50 15 301 1.100E+00	106 30 301 1.840E-01	162 44 301 1.710E-01
51 16 17 1.146E+01	107 30 301 1.840E-01	163 44 301 1.920E-01
52 16 160 4.701E+00	108 31 32 1.146E+01	164 45 46 1.115E+01
53 16 301 1.840E-01	109 31 175 4.701E+00	165 45 189 4.889E+00
54 16 301 1.970E-01	110 31 301 1.840E-01	166 45 301 1.320E-01
55 17 18 1.146E+01	111 31 301 1.840E-01	167 46 47 1.115E+01
56 17 161 4.701E+00	112 32 33 1.146E+01	168 46 190 4.889E+00

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
169	46	301	1	.149E+00	225	60	301	1	.840E-01	281	74	301	1	.138E+00
170	46	301	1	.320E-01	226	60	301	1	.840E-01	282	74	301	1	.710E-01
171	47	48	1	.115E+01	227	61	62	1	.146E+01	283	75	76	1	.120E+01
172	47	191	4	.889E+00	228	61	205	4	.701E+00	284	75	219	4	.889E+00
173	47	301	1	.125E+00	229	61	301	1	.840E-01	285	75	301	1	.157E+00
174	47	301	1	.710E-01	230	61	301	1	.840E-01	286	75	301	1	.900E-01
175	48	49	1	.129E+01	231	62	63	1	.146E+01	287	76	77	1	.125E+01
176	48	192	4	.889E+00	232	62	206	4	.701E+00	288	76	220	4	.655E+00
177	48	301	1	.970E-01	233	62	301	1	.840E-01	289	76	301	1	.171E+00
178	48	301	1	.900E-01	234	62	301	1	.840E-01	290	76	301	1	.980E-01
179	49	50	1	.146E+01	235	63	64	1	.146E+01	291	77	78	1	.210E+01
180	49	193	4	.701E+00	236	63	207	4	.701E+00	292	77	221	4	.655E+00
181	49	301	1	.840E-01	237	63	301	1	.840E-01	293	77	301	1	.172E+00
182	49	301	1	.840E-01	238	63	301	1	.840E-01	294	77	301	1	.980E-01
183	50	51	1	.146E+01	239	64	65	1	.108E+01	295	78	79	1	.172E+01
184	50	194	4	.701E+00	240	64	208	4	.701E+00	296	78	222	4	.542E+00
185	50	301	1	.840E-01	241	64	301	1	.840E-01	297	78	301	1	.131E+00
186	50	301	1	.840E-01	242	64	301	1	.840E-01	298	78	301	1	.920E-01
187	51	52	1	.146E+01	243	65	66	1	.992E+00	299	79	80	1	.992E+00
188	51	195	4	.701E+00	244	65	209	4	.990E+00	300	79	223	4	.815E+00
189	51	301	1	.840E-01	245	65	301	1	.920E-01	301	79	301	1	.111E+00
190	51	301	1	.840E-01	246	65	301	1	.940E-01	302	79	301	1	.920E-01
191	52	53	1	.146E+01	247	66	67	1	.172E+01	303	80	81	1	.108E+01
192	52	196	4	.701E+00	248	66	210	4	.815E+00	304	80	224	4	.990E+00
193	52	301	1	.840E-01	249	66	301	1	.920E-01	305	80	301	1	.940E-01
194	52	301	1	.840E-01	250	66	301	1	.111E+00	306	80	301	1	.920E-01
195	53	54	1	.146E+01	251	67	68	1	.210E+01	307	81	82	1	.146E+01
196	53	197	4	.701E+00	252	67	211	4	.542E+00	308	81	225	4	.701E+00
197	53	301	1	.840E-01	253	67	301	1	.920E-01	309	81	301	1	.840E-01
198	53	301	1	.840E-01	254	67	301	1	.131E+00	310	81	301	1	.840E-01
199	54	55	1	.146E+01	255	68	69	1	.125E+01	311	82	83	1	.146E+01
200	54	198	4	.701E+00	256	68	212	4	.655E+00	312	82	226	4	.701E+00
201	54	301	1	.840E-01	257	68	301	1	.980E-01	313	82	301	1	.840E-01
202	54	301	1	.840E-01	258	68	301	1	.172E+00	314	82	301	1	.840E-01
203	55	56	1	.146E+01	259	69	70	1	.120E+01	315	83	84	1	.146E+01
204	55	199	4	.701E+00	260	69	213	4	.655E+00	316	83	227	4	.701E+00
205	55	301	1	.840E-01	261	69	301	1	.980E-01	317	83	301	1	.840E-01
206	55	301	1	.840E-01	262	69	301	1	.171E+00	318	83	301	1	.840E-01
207	56	57	1	.146E+01	263	70	71	1	.115E+01	319	84	85	1	.146E+01
208	56	200	4	.701E+00	264	70	214	4	.889E+00	320	84	228	4	.701E+00
209	56	301	1	.840E-01	265	70	301	1	.900E-01	321	84	301	1	.840E-01
210	56	301	1	.840E-01	266	70	301	1	.157E+00	322	84	301	1	.840E-01
211	57	58	1	.146E+01	267	71	72	1	.115E+01	323	85	86	1	.146E+01
212	57	201	4	.701E+00	268	71	215	4	.889E+00	324	85	229	4	.701E+00
213	57	301	1	.840E-01	269	71	301	1	.710E-01	325	85	301	1	.840E-01
214	57	301	1	.840E-01	270	71	301	1	.138E+00	326	85	301	1	.840E-01
215	58	59	1	.146E+01	271	72	73	1	.115E+01	327	86	87	1	.146E+01
216	58	202	4	.701E+00	272	72	216	4	.889E+00	328	86	230	4	.701E+00
217	58	301	1	.840E-01	273	72	301	1	.320E-01	329	86	301	1	.840E-01
218	58	301	1	.840E-01	274	72	301	1	.670E-01	330	86	301	1	.840E-01
219	59	60	1	.146E+01	275	73	74	1	.115E+01	331	87	88	1	.146E+01
220	59	203	4	.701E+00	276	73	217	4	.889E+00	332	87	231	4	.701E+00
221	59	301	1	.840E-01	277	73	301	1	.670E-01	333	87	301	1	.840E-01
222	59	301	1	.840E-01	278	73	301	1	.320E-01	334	87	301	1	.840E-01
223	60	61	1	.146E+01	279	74	75	1	.115E+01	335	88	89	1	.146E+01
224	60	204	4	.701E+00	280	74	218	4	.889E+00	336	88	232	4	.701E+00

Brnh	From To	Tag	Conduct	Brnh	From To	Tag	Conduct	Brnh	From To	Tag	Conduct
337	88 301	1	.840E-01	393	102 301	1	.900E-01	449	116 301	1	.840E-01
338	88 301	1	.840E-01	394	103 104	1	.146E+01	450	117 118	1	.146E+01
339	89 90	1	.146E+01	395	103 247	4	.701E+00	451	117 261	4	.701E+00
340	89 233	4	.701E+00	396	103 301	1	.840E-01	452	117 301	1	.840E-01
341	89 301	1	.840E-01	397	103 301	1	.840E-01	453	117 301	1	.840E-01
342	89 301	1	.840E-01	398	104 105	1	.146E+01	454	118 119	1	.129E+01
343	90 91	1	.146E+01	399	104 248	4	.701E+00	455	118 262	4	.701E+00
344	90 301	4	.701E+00	400	104 301	1	.840E-01	456	118 301	1	.840E-01
346	90 301	1	.840E-01	401	104 301	1	.840E-01	457	118 301	1	.840E-01
347	90 301	1	.840E-01	402	105 106	1	.146E+01	458	119 120	1	.115E+01
347	91 92	1	.146E+01	403	105 249	4	.701E+00	459	119 263	4	.889E+00
348	91 235	4	.701E+00	404	105 301	1	.840E-01	460	119 301	1	.900E-01
349	91 301	1	.840E-01	405	105 301	1	.840E-01	461	119 301	1	.940E-01
350	91 301	1	.840E-01	406	106 107	1	.146E+01	462	120 121	1	.115E+01
351	92 93	1	.146E+01	407	106 250	4	.701E+00	463	120 264	4	.889E+00
352	92 236	4	.701E+00	408	106 301	1	.840E-01	464	120 301	1	.111E+00
353	92 301	1	.840E-01	409	106 301	1	.840E-01	465	120 301	1	.111E+00
354	92 301	1	.840E-01	410	107 108	1	.146E+01	466	121 122	1	.115E+01
355	93 94	1	.146E+01	411	107 251	4	.701E+00	467	121 265	4	.889E+00
356	93 237	4	.701E+00	412	107 301	1	.840E-01	468	121 301	1	.320E-01
357	93 301	1	.840E-01	413	107 301	1	.840E-01	469	121 301	1	.131E+00
358	93 301	1	.840E-01	414	108 109	1	.146E+01	470	122 123	1	.115E+01
359	94 95	1	.146E+01	415	108 252	4	.701E+00	471	122 266	4	.889E+00
360	94 238	4	.701E+00	416	108 301	1	.840E-01	472	122 301	1	.320E-01
361	94 301	1	.840E-01	417	108 301	1	.840E-01	473	123 124	1	.115E+01
362	94 301	1	.840E-01	418	109 110	1	.146E+01	474	123 267	4	.889E+00
363	95 96	1	.146E+01	419	109 253	4	.701E+00	475	123 301	1	.710E-01
364	95 239	4	.701E+00	420	109 301	1	.840E-01	476	124 125	1	.129E+01
365	95 301	1	.840E-01	421	109 301	1	.840E-01	477	124 268	4	.889E+00
366	95 301	1	.840E-01	422	110 111	1	.146E+01	478	124 301	1	.900E-01
367	96 97	1	.129E+01	423	110 254	4	.701E+00	479	125 126	1	.146E+01
368	96 240	4	.701E+00	424	110 301	1	.840E-01	480	125 269	4	.701E+00
369	96 301	1	.840E-01	425	110 301	1	.840E-01	481	125 301	1	.490E-01
370	96 301	1	.840E-01	426	111 112	1	.146E+01	482	125 301	1	.840E-01
371	97 98	1	.115E+01	427	111 255	4	.701E+00	483	126 127	1	.146E+01
372	97 241	4	.889E+00	428	111 301	1	.840E-01	484	126 270	4	.701E+00
373	97 301	1	.900E-01	429	111 301	1	.840E-01	485	126 301	1	.680E-01
374	97 301	1	.970E-01	430	112 113	1	.146E+01	486	126 301	1	.840E-01
375	98 99	1	.115E+01	431	112 256	4	.701E+00	487	127 128	1	.146E+01
376	98 242	4	.889E+00	432	112 301	1	.840E-01	488	127 271	4	.701E+00
377	98 301	1	.710E-01	433	112 301	1	.840E-01	489	127 301	1	.820E-01
378	98 301	1	.125E+00	434	113 114	1	.146E+01	490	127 301	1	.840E-01
379	99 100	1	.115E+01	435	113 257	4	.701E+00	491	128 129	1	.146E+01
380	99 243	4	.889E+00	436	113 301	1	.840E-01	492	128 272	4	.701E+00
381	99 301	1	.320E-01	437	113 301	1	.840E-01	493	128 301	1	.910E-01
382	99 301	1	.149E+00	438	114 115	1	.146E+01	494	128 301	1	.840E-01
383	100 101	1	.115E+01	439	114 258	4	.701E+00	495	129 130	1	.146E+01
384	100 244	4	.889E+00	440	114 301	1	.840E-01	496	129 273	4	.701E+00
385	100 301	1	.320E-01	441	114 301	1	.840E-01	497	129 301	1	.970E-01
386	101 102	1	.115E+01	442	115 116	1	.146E+01	498	129 301	1	.840E-01
387	101 245	4	.889E+00	443	115 259	4	.701E+00	499	130 131	1	.146E+01
388	101 301	1	.920E-01	444	115 301	1	.840E-01	500	130 274	4	.701E+00
389	101 301	1	.710E-01	445	115 301	1	.840E-01	501	130 301	1	.100E+00
390	102 103	1	.129E+01	446	116 117	1	.146E+01	502	130 301	1	.840E-01
391	102 246	4	.889E+00	447	116 260	4	.701E+00	503	131 132	1	.146E+01
392	102 301	1	.124E+00	448	116 301	1	.840E-01	504	131 275	4	.701E+00

Brnh	From	To	Taq	Conduct	Brnh	From	To	Taq	Conduct	Brnh	From	To	Taq	Conduct
505	131	301	1	.101E+00	561	158	157	5	.174E+03	617	214	213	5	.174E+03
506	131	301	1	.840E+01	562	159	158	5	.174E+03	618	215	214	5	.174E+03
507	132	133	1	.146E+01	563	160	159	5	.174E+03	619	216	215	5	.174E+03
508	132	276	4	.701E+00	564	161	160	5	.174E+03	620	217	216	5	.174E+03
509	132	301	1	.100E+00	565	162	161	5	.174E+03	621	218	217	5	.174E+03
510	132	301	1	.840E+01	566	163	162	5	.174E+03	622	219	218	5	.174E+03
511	133	134	1	.146E+01	567	164	163	5	.174E+03	623	220	219	5	.174E+03
512	133	277	4	.701E+00	568	165	164	5	.174E+03	624	221	220	5	.174E+03
513	133	301	1	.970E+01	569	166	165	5	.174E+03	625	222	221	5	.174E+03
514	133	301	1	.840E+01	570	167	166	5	.174E+03	626	223	222	5	.174E+03
515	134	135	1	.146E+01	571	168	167	5	.174E+03	627	224	223	5	.174E+03
516	134	278	4	.701E+00	572	169	168	5	.174E+03	628	225	224	5	.174E+03
517	134	301	1	.910E+01	573	170	169	5	.174E+03	629	226	225	5	.174E+03
518	134	301	1	.840E+01	574	171	170	5	.174E+03	630	227	226	5	.174E+03
519	135	136	1	.146E+01	575	172	171	5	.174E+03	631	228	227	5	.174E+03
520	135	279	4	.701E+00	576	173	172	5	.174E+03	632	229	228	5	.174E+03
521	135	301	1	.820E+01	577	174	173	5	.174E+03	633	230	229	5	.174E+03
522	135	301	1	.840E+01	578	175	174	5	.174E+03	634	231	230	5	.174E+03
523	136	137	1	.146E+01	579	176	175	5	.174E+03	635	232	231	5	.174E+03
524	136	280	4	.701E+00	580	177	176	5	.174E+03	636	233	232	5	.174E+03
525	136	301	1	.680E+01	581	178	177	5	.174E+03	637	234	233	5	.174E+03
526	136	301	1	.840E+01	582	179	178	5	.174E+03	638	235	234	5	.174E+03
527	137	138	1	.146E+01	583	180	179	5	.174E+03	639	236	235	5	.174E+03
528	137	281	4	.701E+00	584	181	180	5	.174E+03	640	237	236	5	.174E+03
529	137	301	1	.490E+01	585	182	181	5	.174E+03	641	238	237	5	.174E+03
530	137	301	1	.840E+01	586	183	182	5	.174E+03	642	239	238	5	.174E+03
531	138	139	1	.146E+01	587	184	183	5	.174E+03	643	240	239	5	.174E+03
532	138	282	4	.701E+00	588	185	184	5	.174E+03	644	241	240	5	.174E+03
533	138	301	1	.240E+01	589	186	185	5	.174E+03	645	242	241	5	.174E+03
534	138	301	1	.840E+01	590	187	186	5	.174E+03	646	243	242	5	.174E+03
535	139	140	1	.146E+01	591	188	187	5	.174E+03	647	244	243	5	.174E+03
536	139	283	4	.701E+00	592	189	188	5	.174E+03	648	245	244	5	.174E+03
537	139	301	1	.840E+01	593	190	189	5	.174E+03	649	246	245	5	.174E+03
538	140	141	1	.160E+01	594	191	190	5	.174E+03	650	247	246	5	.174E+03
539	140	284	4	.701E+00	595	192	191	5	.174E+03	651	248	247	5	.174E+03
540	140	301	1	.840E+01	596	193	192	5	.174E+03	652	249	248	5	.174E+03
541	141	142	1	.178E+01	597	194	193	5	.174E+03	653	250	249	5	.174E+03
542	141	285	4	.576E+00	598	195	194	5	.174E+03	654	251	250	5	.174E+03
543	142	143	1	.178E+01	599	196	195	5	.174E+03	655	252	251	5	.174E+03
544	142	286	4	.576E+00	600	197	196	5	.174E+03	656	253	252	5	.174E+03
545	143	144	1	.178E+01	601	198	197	5	.174E+03	657	254	253	5	.174E+03
546	143	287	4	.576E+00	602	199	198	5	.174E+03	658	255	254	5	.174E+03
547	144	288	4	.576E+00	603	200	199	5	.174E+03	659	256	255	5	.174E+03
548	145	302	5	.174E+03	604	201	200	5	.174E+03	660	257	256	5	.174E+03
549	146	145	5	.174E+03	605	202	201	5	.174E+03	661	258	257	5	.174E+03
550	147	146	5	.174E+03	606	203	202	5	.174E+03	662	259	258	5	.174E+03
551	148	147	5	.174E+03	607	204	203	5	.174E+03	663	260	259	5	.174E+03
552	149	148	5	.174E+03	608	205	204	5	.174E+03	664	261	260	5	.174E+03
553	150	149	5	.174E+03	609	206	205	5	.174E+03	665	262	261	5	.174E+03
554	151	150	5	.174E+03	610	207	206	5	.174E+03	666	263	262	5	.174E+03
555	152	151	5	.174E+03	611	208	207	5	.174E+03	667	264	263	5	.174E+03
556	153	152	5	.174E+03	612	209	208	5	.174E+03	668	265	264	5	.174E+03
557	154	153	5	.174E+03	613	210	209	5	.174E+03	669	266	265	5	.174E+03
558	155	154	5	.174E+03	614	211	210	5	.174E+03	670	267	266	5	.174E+03
559	156	155	5	.174E+03	615	212	211	5	.174E+03	671	268	267	5	.174E+03
560	157	156	5	.174E+03	616	213	212	5	.174E+03	672	269	268	5	.174E+03

Brnh	From	To	Tag	Conduct
673	270	269	5	.174E+03
674	271	270	5	.174E+03
675	272	271	5	.174E+03
676	273	272	5	.174E+03
677	274	273	5	.174E+03
678	275	274	5	.174E+03
679	276	275	5	.174E+03
680	277	276	5	.174E+03
681	278	277	5	.174E+03
682	279	278	5	.174E+03
683	280	279	5	.174E+03
684	281	280	5	.174E+03
685	282	281	5	.174E+03
686	283	282	5	.174E+03
687	284	283	5	.174E+03
688	285	284	5	.174E+03
689	286	285	5	.174E+03
690	287	286	5	.174E+03
691	288	287	5	.174E+03

TASS GENERAL INPUT MENU - SI Units

(1) Case Title:

TALSR(METRIC)----RUN 2. COMPLEX MODEL 149.7 kg/hr (330 lbm/hr)

(2) Nodes	288
(3) Constant Temperatures	2
(4) Unique Exponents	0
(5) Temperature Dependent Conductances	0
(6) Temperature Dependent Heat Inputs	0
(7) Computational Accuracy	.0100
(8) Starting Temperature	25.0

Are these inputs correct (Y/N) ? Y

NODE	TEMPERATURE (Celsius)	ABSOLUTE VALUE OF THETA (b) (Celsius)
5	26.34	13.66
6	26.63	13.37
7	26.91	13.09
8	27.19	12.81
9	27.42	12.58
10	27.62	12.38
11	27.77	12.23
12	27.88	12.12
13	27.95	12.05
14	27.98	12.02
15	27.97	12.03
16	27.93	12.07
17	27.85	12.15
18	27.73	12.27
19	27.57	12.43
20	27.38	12.62
21	27.15	12.85
22	27.01	12.99
23	27.02	12.98
24	27.29	12.71
25	27.52	12.48
26	27.7	12.3
27	27.84	12.16
28	27.93	12.07
29	27.99	12.01
30	28.04	11.96
31	28.07	11.93
32	28.1	11.9
33	28.12	11.88
34	28.13	11.87
35	28.14	11.86
36	28.15	11.85
37	28.15	11.85
38	28.15	11.85
39	28.14	11.86
40	28.12	11.88
41	28.09	11.91
42	28.04	11.96
43	27.94	12.06
44	27.77	12.23
45	27.61	12.39
46	27.78	12.22
47	27.93	12.07
48	28.03	11.97
49	28.13	11.87
50	28.19	11.81
51	28.24	11.76
52	28.27	11.73

53	28.3	11.7
54	28.32	11.68
55	28.34	11.66
56	28.35	11.65
57	28.37	11.63
58	28.38	11.62
59	28.39	11.61
60	28.41	11.59
61	28.42	11.58
62	28.44	11.56
63	28.47	11.53
64	28.5	11.5
65	28.56	11.44
66	28.8	11.2
67	28.98	11.02
68	29.04	10.96
69	29	11
70	28.78	11.22
71	28.53	11.47
72	28.31	11.69
73	28.32	11.68
74	28.57	11.43
75	28.83	11.17
76	29.07	10.93
77	29.14	10.86
78	29.09	10.91
79	28.93	11.07
80	28.72	11.28
81	28.68	11.32
82	28.67	11.33
83	28.66	11.34
84	28.66	11.34
85	28.66	11.34
86	28.67	11.33
87	28.67	11.33
88	28.68	11.32
89	28.68	11.32
90	28.68	11.32
91	28.68	11.32
92	28.68	11.32
93	28.67	11.33
94	28.66	11.34
95	28.63	11.37
96	28.59	11.41
97	28.51	11.49
98	28.43	11.57
99	28.31	11.69
100	28.17	11.83
101	28.34	11.66
102	28.52	11.48

103	28.63	11.37
104	28.69	11.31
105	28.74	11.26
106	28.78	11.22
107	28.8	11.2
108	28.82	11.18
109	28.84	11.16
110	28.85	11.15
111	28.85	11.15
112	28.86	11.14
113	28.86	11.14
114	28.85	11.15
115	28.84	11.16
116	28.81	11.19
117	28.77	11.23
118	28.7	11.3
119	28.58	11.42
120	28.44	11.56
121	28.25	11.75
122	28.01	11.99
123	28.02	11.98
124	28.16	11.84
125	28.4	11.6
126	28.59	11.41
127	28.74	11.26
128	28.87	11.13
129	28.96	11.04
130	29.01	10.99
131	29.03	10.97
132	29.02	10.98
133	28.97	11.03
134	28.89	11.11
135	28.77	11.23
136	28.61	11.39
137	28.4	11.6
138	28.17	11.83
139	27.92	12.08
140	27.67	12.33

INTEGRITY

Fin Length (L) (mm)	Fin Thickness (mm)	Fin Spacing (s) (mm)	Thermal Conductivity of Copper (W/m-K)	Prandtl Number	Outer pipe radius (cm)	Inner Pipe Radius (cm)	Pipe Area (sq. cm.)	
9.318	0.015	0.055	4.01	0.707	0.015	0.015	0.503	
Model Fin Spacing Plate Channel (MM) (in)								
Fin Length (L) (mm)	Fin Thickness (mm)	Effective Diameter (mm)	Heat Transfer Coefficient (h) (W/m ² -K)	m (1/mm)	Lambda	R: Thrua (cm)	t2: Term (cm)	t1: Term (cm)
5-42	1.143	0.10192	0.03626	1.08929	3.473	1.142	0.461	0.902
7-41	1.143	0.10192	0.03626	1.08929	3.473	1.123	0.475	0.864
7-40	1.143	0.10192	0.03626	1.08929	3.473	1.123	0.475	0.864
8-39	1.143	0.10192	0.03626	1.08929	3.473	1.080	0.508	0.835
8-38	1.143	0.10192	0.03626	1.08929	3.473	1.062	0.522	0.821
10-37	1.143	0.10192	0.03626	1.08929	3.473	1.045	0.535	0.808
11-36	1.143	0.10192	0.03626	1.08929	3.473	1.032	0.545	0.798
12-35	1.143	0.10192	0.03626	1.08929	3.473	1.015	0.559	0.784
13-34	1.143	0.10192	0.03626	1.08929	3.473	1.012	0.562	0.781
14-33	1.143	0.10192	0.03626	1.08929	3.473	1.012	0.562	0.781
15-32	1.143	0.10192	0.03626	1.08929	3.473	1.012	0.562	0.781
16-31	1.143	0.10192	0.03626	1.08929	3.473	1.012	0.562	0.781
17-30	1.143	0.10192	0.03626	1.08929	3.473	1.016	0.568	0.785
18-29	1.143	0.10192	0.03626	1.08929	3.473	1.022	0.573	0.790
19-28	1.143	0.10192	0.03626	1.08929	3.473	1.030	0.581	0.796
20-27	1.143	0.10192	0.03626	1.08929	3.473	1.038	0.587	0.802
21-26	1.104	0.10178	0.03629	1.08966	3.331	1.045	0.594	0.809
22-25	0.808	0.10068	0.03670	1.09066	2.425	1.041	0.590	0.805
23-24	0.296	0.09038	0.03748	1.13381	1.399	1.041	0.590	0.805
24-23	0.146	0.08018	0.03844	1.18545	0.744	1.151	0.610	0.822
25-22	0.073	0.07021	0.03965	1.25445	0.405	1.114	0.622	0.822
26-21	0.036	0.06028	0.04122	1.34173	0.200	1.075	0.634	0.851
27-20	0.018	0.05092	0.04326	1.44829	0.100	1.057	0.658	0.878
28-19	0.009	0.04192	0.04568	1.57629	0.050	1.047	0.683	0.903
29-18	0.004	0.03342	0.04848	1.72829	0.025	1.039	0.710	0.930
30-17	0.002	0.02542	0.05168	1.90629	0.012	1.033	0.740	0.960
31-16	0.001	0.01792	0.05528	2.11329	0.006	1.029	0.770	0.990
32-15	0.000	0.01092	0.05948	2.35329	0.003	1.025	0.800	1.020
33-14	0.000	0.00792	0.06428	2.63329	0.001	1.022	0.830	1.050
34-13	0.000	0.00592	0.06968	2.95329	0.000	1.021	0.860	1.080
35-12	0.000	0.00392	0.07568	3.31329	0.000	1.018	0.890	1.110
36-11	0.000	0.00292	0.08228	3.71329	0.000	1.016	0.920	1.140
37-10	0.000	0.00192	0.08948	4.15329	0.000	1.015	0.950	1.170
38-09	0.000	0.00142	0.09728	4.63329	0.000	1.013	0.980	1.200
39-08	0.000	0.00092	0.10568	5.15329	0.000	1.011	1.010	1.230
40-07	0.000	0.00042	0.11468	5.71329	0.000	1.010	1.040	1.260

41.50	1.143	0.10192	0.00026	1.08520	3.473	1.008	0.565	0.578
42.49	1.143	0.10192	0.00026	1.08520	3.473	1.008	0.565	0.578
43.48	1.104	0.10170	0.00029	1.08520	3.473	1.008	0.565	0.578
44.47	1.068	0.10098	0.00032	1.08520	3.473	1.008	0.565	0.578
45.46	1.032	0.10026	0.00035	1.08520	3.473	1.008	0.565	0.578
46.45	1.000	0.09954	0.00038	1.08520	3.473	1.008	0.565	0.578
47.44	0.968	0.09882	0.00041	1.08520	3.473	1.008	0.565	0.578
48.43	0.936	0.09810	0.00044	1.08520	3.473	1.008	0.565	0.578
49.42	0.904	0.09738	0.00047	1.08520	3.473	1.008	0.565	0.578
50.41	0.872	0.09666	0.00050	1.08520	3.473	1.008	0.565	0.578
51.40	0.840	0.09594	0.00053	1.08520	3.473	1.008	0.565	0.578
52.39	0.808	0.09522	0.00056	1.08520	3.473	1.008	0.565	0.578
53.38	0.776	0.09450	0.00059	1.08520	3.473	1.008	0.565	0.578
54.37	0.744	0.09378	0.00062	1.08520	3.473	1.008	0.565	0.578
55.36	0.712	0.09306	0.00065	1.08520	3.473	1.008	0.565	0.578
56.35	0.680	0.09234	0.00068	1.08520	3.473	1.008	0.565	0.578
57.34	0.648	0.09162	0.00071	1.08520	3.473	1.008	0.565	0.578
58.33	0.616	0.09090	0.00074	1.08520	3.473	1.008	0.565	0.578
59.32	0.584	0.09018	0.00077	1.08520	3.473	1.008	0.565	0.578
60.31	0.552	0.08946	0.00080	1.08520	3.473	1.008	0.565	0.578
61.30	0.520	0.08874	0.00083	1.08520	3.473	1.008	0.565	0.578
62.29	0.488	0.08802	0.00086	1.08520	3.473	1.008	0.565	0.578
63.28	0.456	0.08730	0.00089	1.08520	3.473	1.008	0.565	0.578
64.27	0.424	0.08658	0.00092	1.08520	3.473	1.008	0.565	0.578
65.26	0.392	0.08586	0.00095	1.08520	3.473	1.008	0.565	0.578
66.25	0.360	0.08514	0.00098	1.08520	3.473	1.008	0.565	0.578
67.24	0.328	0.08442	0.00101	1.08520	3.473	1.008	0.565	0.578
68.23	0.296	0.08370	0.00104	1.08520	3.473	1.008	0.565	0.578
69.22	0.264	0.08298	0.00107	1.08520	3.473	1.008	0.565	0.578
70.21	0.232	0.08226	0.00110	1.08520	3.473	1.008	0.565	0.578
71.20	0.200	0.08154	0.00113	1.08520	3.473	1.008	0.565	0.578
72.19	0.168	0.08082	0.00116	1.08520	3.473	1.008	0.565	0.578
73.18	0.136	0.08010	0.00119	1.08520	3.473	1.008	0.565	0.578
74.17	0.104	0.07938	0.00122	1.08520	3.473	1.008	0.565	0.578
75.16	0.072	0.07866	0.00125	1.08520	3.473	1.008	0.565	0.578
76.15	0.040	0.07794	0.00128	1.08520	3.473	1.008	0.565	0.578
77.14	0.008	0.07722	0.00131	1.08520	3.473	1.008	0.565	0.578
78.13	0.000	0.07650	0.00134	1.08520	3.473	1.008	0.565	0.578
79.12	0.000	0.07578	0.00137	1.08520	3.473	1.008	0.565	0.578
80.11	0.000	0.07506	0.00140	1.08520	3.473	1.008	0.565	0.578
81.10	0.000	0.07434	0.00143	1.08520	3.473	1.008	0.565	0.578
82.09	0.000	0.07362	0.00146	1.08520	3.473	1.008	0.565	0.578
83.08	0.000	0.07290	0.00149	1.08520	3.473	1.008	0.565	0.578
84.07	0.000	0.07218	0.00152	1.08520	3.473	1.008	0.565	0.578
85.06	0.000	0.07146	0.00155	1.08520	3.473	1.008	0.565	0.578
86.05	0.000	0.07074	0.00158	1.08520	3.473	1.008	0.565	0.578
87.04	0.000	0.07002	0.00161	1.08520	3.473	1.008	0.565	0.578
88.03	0.000	0.06930	0.00164	1.08520	3.473	1.008	0.565	0.578
89.02	0.000	0.06858	0.00167	1.08520	3.473	1.008	0.565	0.578
90.01	0.000	0.06786	0.00170	1.08520	3.473	1.008	0.565	0.578
91.00	0.000	0.06714	0.00173	1.08520	3.473	1.008	0.565	0.578
92.00	0.000	0.06642	0.00176	1.08520	3.473	1.008	0.565	0.578

93-106	1.143	0.10192	0.03626	1.08539	3.473	1.010	0.563	0.539
94-115	1.143	0.10192	0.03626	1.08539	3.473	1.010	0.562	0.537
95-124	1.143	0.10192	0.03626	1.08539	3.473	1.015	0.567	0.516
96-134	1.143	0.10192	0.03626	1.08539	3.473	1.015	0.568	0.515
97-102	1.104	0.10176	0.03629	1.08540	3.331	1.011	0.551	0.553
98-101	0.838	0.10068	0.03670	1.08546	2.425	0.992	0.413	0.395
99-100	0.296	0.09018	0.03628	1.13381	1.399	0.988	0.180	0.116
100-139	1.143	0.10192	0.03626	1.08520	3.473	0.992	0.639	0.504
101-138	1.143	0.10192	0.03626	1.08520	3.473	0.986	0.608	0.517
102-137	1.143	0.10192	0.03626	1.08520	3.473	0.982	0.602	0.512
103-136	1.143	0.10192	0.03626	1.08520	3.473	0.982	0.598	0.514
104-135	1.143	0.10192	0.03626	1.08520	3.473	0.985	0.596	0.557
105-134	1.143	0.10192	0.03626	1.08520	3.473	0.986	0.575	0.569
106-133	1.143	0.10192	0.03626	1.08520	3.473	1.005	0.567	0.576
107-132	1.143	0.10192	0.03626	1.08520	3.473	1.011	0.562	0.581
108-131	1.143	0.10192	0.03626	1.08520	3.473	1.015	0.559	0.584
109-130	1.143	0.10192	0.03626	1.08520	3.473	1.015	0.559	0.584
110-129	1.143	0.10192	0.03626	1.08520	3.473	1.014	0.560	0.583
111-128	1.143	0.10192	0.03626	1.08520	3.473	1.015	0.563	0.583
112-127	1.143	0.10192	0.03626	1.08520	3.473	1.014	0.565	0.583
113-126	1.143	0.10192	0.03626	1.08520	3.473	1.014	0.566	0.584
114-125	1.143	0.10192	0.03626	1.08520	3.473	0.994	0.576	0.567
115-124	1.143	0.10192	0.03626	1.08520	3.473	0.984	0.595	0.559
116-123	1.143	0.10192	0.03626	1.08520	3.473	0.974	0.593	0.550
117-122	1.143	0.10192	0.03626	1.08520	3.473	0.965	0.562	0.522
118-121	1.104	0.10176	0.03629	1.08540	3.331	0.965	0.443	0.365
119-120	0.838	0.10068	0.03670	1.08546	2.425	0.965	0.443	0.365
120-119	0.296	0.09018	0.03628	1.13381	1.399	0.965	0.202	0.094
121-118	0.296	0.09018	0.03628	1.13381	1.399	0.965	0.202	0.094

INSUL DATA

Pin Length (L) (cm)	Pin Thickness (cm)	Fin spacing (S) (cm)	Thermal Conductivity of Copper (K)(Watts-K)	Heat Transfer Coefficient (h) (Watts-K)	Dr Term (cm)	Yield (W/K)	Dist. between Nodes (cm)	Fracture (cm)	Pipe Area (sq. cm.)	K-Value (W/K)
0.318	0.018	0.0533	4.01	1500.00	0.307	0.453	0.633	0.483	0.134	
K1			N/A	N/A					N/A	1.7784
K2			1.360	0.0000					N/A	0.5762
K3			N/A	N/A					N/A	1.6543
K4			1.290	0.0000					N/A	1.4612
K5	1.143	0.0109	0.03626	0.0000		0.0133	0.307		N/A	0.7013
K6	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K7	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K8	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K9	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K10	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K11	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K12	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K13	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K14	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K15	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K16	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K17	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K18	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K19	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K20	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K21	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K22	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K23	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K24	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K25	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K26	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K27	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K28	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K29	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K30	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K31	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K32	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K33	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K34	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K35	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K36	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K37	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K38	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K39	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K40	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945
K41	1.143	0.0109	0.03626	0.0000		0.0134	0.307		N/A	0.6945

842	1.43	0.1019	0.03526	0.61800	0.01241	0.367	6.800	0.0590
843	1.43	0.1019	0.03526	0.64100	0.01119	0.367	6.800	0.0590
844	1.43	0.1019	0.03526	0.66400	0.01000	0.367	6.800	0.0590
845	1.43	0.1019	0.03526	0.68700	0.00880	0.367	6.800	0.0590
846	1.43	0.1019	0.03526	0.71000	0.00760	0.367	6.800	0.0590
847	1.43	0.1019	0.03526	0.73300	0.00640	0.367	6.800	0.0590
848	1.43	0.1019	0.03526	0.75600	0.00520	0.367	6.800	0.0590
849	1.43	0.1019	0.03526	0.77900	0.00400	0.367	6.800	0.0590
850	1.43	0.1019	0.03526	0.80200	0.00280	0.367	6.800	0.0590
851	1.43	0.1019	0.03526	0.82500	0.00160	0.367	6.800	0.0590
852	1.43	0.1019	0.03526	0.84800	0.00040	0.367	6.800	0.0590
853	1.43	0.1019	0.03526	0.87100	0.00000	0.367	6.800	0.0590
854	1.43	0.1019	0.03526	0.89400	0.00000	0.367	6.800	0.0590
855	1.43	0.1019	0.03526	0.91700	0.00000	0.367	6.800	0.0590
856	1.43	0.1019	0.03526	0.94000	0.00000	0.367	6.800	0.0590
857	1.43	0.1019	0.03526	0.96300	0.00000	0.367	6.800	0.0590
858	1.43	0.1019	0.03526	0.98600	0.00000	0.367	6.800	0.0590
859	1.43	0.1019	0.03526	1.00900	0.00000	0.367	6.800	0.0590
860	1.43	0.1019	0.03526	1.03200	0.00000	0.367	6.800	0.0590
861	1.43	0.1019	0.03526	1.05500	0.00000	0.367	6.800	0.0590
862	1.43	0.1019	0.03526	1.07800	0.00000	0.367	6.800	0.0590
863	1.43	0.1019	0.03526	1.10100	0.00000	0.367	6.800	0.0590
864	1.43	0.1019	0.03526	1.12400	0.00000	0.367	6.800	0.0590
865	1.43	0.1019	0.03526	1.14700	0.00000	0.367	6.800	0.0590
866	1.43	0.1019	0.03526	1.17000	0.00000	0.367	6.800	0.0590
867	1.43	0.1019	0.03526	1.19300	0.00000	0.367	6.800	0.0590
868	1.43	0.1019	0.03526	1.21600	0.00000	0.367	6.800	0.0590
869	1.43	0.1019	0.03526	1.23900	0.00000	0.367	6.800	0.0590
870	1.43	0.1019	0.03526	1.26200	0.00000	0.367	6.800	0.0590
871	1.43	0.1019	0.03526	1.28500	0.00000	0.367	6.800	0.0590
872	1.43	0.1019	0.03526	1.30800	0.00000	0.367	6.800	0.0590
873	1.43	0.1019	0.03526	1.33100	0.00000	0.367	6.800	0.0590
874	1.43	0.1019	0.03526	1.35400	0.00000	0.367	6.800	0.0590
875	1.43	0.1019	0.03526	1.37700	0.00000	0.367	6.800	0.0590
876	1.43	0.1019	0.03526	1.40000	0.00000	0.367	6.800	0.0590
877	1.43	0.1019	0.03526	1.42300	0.00000	0.367	6.800	0.0590
878	1.43	0.1019	0.03526	1.44600	0.00000	0.367	6.800	0.0590
879	1.43	0.1019	0.03526	1.46900	0.00000	0.367	6.800	0.0590
880	1.43	0.1019	0.03526	1.49200	0.00000	0.367	6.800	0.0590
881	1.43	0.1019	0.03526	1.51500	0.00000	0.367	6.800	0.0590
882	1.43	0.1019	0.03526	1.53800	0.00000	0.367	6.800	0.0590
883	1.43	0.1019	0.03526	1.56100	0.00000	0.367	6.800	0.0590
884	1.43	0.1019	0.03526	1.58400	0.00000	0.367	6.800	0.0590
885	1.43	0.1019	0.03526	1.60700	0.00000	0.367	6.800	0.0590
886	1.43	0.1019	0.03526	1.63000	0.00000	0.367	6.800	0.0590
887	1.43	0.1019	0.03526	1.65300	0.00000	0.367	6.800	0.0590
888	1.43	0.1019	0.03526	1.67600	0.00000	0.367	6.800	0.0590
889	1.43	0.1019	0.03526	1.69900	0.00000	0.367	6.800	0.0590
890	1.43	0.1019	0.03526	1.72200	0.00000	0.367	6.800	0.0590
891	1.43	0.1019	0.03526	1.74500	0.00000	0.367	6.800	0.0590
892	1.43	0.1019	0.03526	1.76800	0.00000	0.367	6.800	0.0590
893	1.43	0.1019	0.03526	1.79100	0.00000	0.367	6.800	0.0590

K146	1.143	0.0326	0.5700	0.0161	0.429	8.540	0.0077
K147	1.143	0.0326	0.5690	0.0157	0.429	8.540	0.0073
K148	2.037	0.0326	0.5690	0.0167	0.255	7.540	0.0142
K149	1.143	0.0326	0.5630	0.0155	0.255	7.540	0.0091
K150	1.060	0.0326	0.5630	0.0175	0.012	7.540	0.0012
K151	1.143	0.0326	0.5630	0.0175	0.317	7.540	0.0070
K152	1.143	0.0326	0.5630	0.0175	0.317	7.540	0.0070
K153	1.144	0.0327	0.5650	0.0184	0.541	7.540	0.0033
K154	1.143	0.0326	0.5650	0.0186	0.541	7.540	0.0067
K155	1.143	0.0326	0.5730	0.0171	0.367	6.800	0.0042
K156	1.143	0.0326	0.5690	0.0147	0.367	6.800	0.0025
K157	1.143	0.0326	0.5690	0.0147	0.367	6.800	0.0025
K158	1.143	0.0326	0.5690	0.0145	0.367	6.800	0.0048
K159	1.143	0.0326	0.5650	0.0185	0.367	6.800	0.0024
K160	1.143	0.0326	0.5650	0.0144	0.367	6.800	0.0023
K161	1.143	0.0326	0.5650	0.0190	0.367	6.800	0.0025
K162	1.143	0.0326	0.5650	0.0190	0.367	6.800	0.0025
K163	1.143	0.0326	0.5650	0.0190	0.367	6.800	0.0025
K164	1.143	0.0326	0.5650	0.0190	0.367	6.800	0.0025
K165	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K166	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K167	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K168	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K169	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K170	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K171	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K172	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K173	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K174	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K175	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K176	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K177	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K178	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K179	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K180	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K181	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K182	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K183	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K184	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K185	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K186	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K187	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K188	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K189	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K190	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K191	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K192	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K193	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K194	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K195	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K196	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K197	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K198	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K199	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317
K200	1.143	0.0326	0.5650	0.0135	0.367	6.800	0.00317

P250	1.143	0.0119	0.00836	0.00660	0.01253	0.387	6.940	0.0096
P251	1.143	0.0119	0.00836	0.00660	0.01272	0.387	6.940	0.0096
P252	NA	NA	NA	NA	NA	NA	NA	173.8900

BRANCH	NODE	TON	TAG	I, C, S	BRANCH	NODE	TON	TAG	I, C, S
1	1	2	1	K1	51	16	17	1	S9
2		145	4	K2	52		160	4	S10
3	2	3	1	S1	53		301	1	K25
4		146	4	S2	54		301	1	S38
5	3	4	1	S1	55	17	18	1	S9
6		147	4	S2	56		161	4	S10
7	4	5	1	K3	57		301	1	K26
8		148	4	S2	58		301	1	S34
9	5	6	1	K4	59	18	19	1	S9
10		149	4	K5	60		162	4	S10
11		301	1	K6	61		301	1	K27
12	6	7	1	S9	62		301	1	S30
13		150	4	S10	63	19	20	1	S9
14		301	1	K7	64		163	4	S10
15	7	8	1	S9	65		301	1	K28
16		151	4	S10	66		301	1	S26
17		301	1	K8	67	20	21	1	K29
18		301	1	K9	68		164	4	S10
19	8	9	1	S9	69		301	1	K30
20		152	4	S10	70		301	1	S22
21		301	1	K10	71	21	22	1	K31
22		301	1	K11	72		165	4	K32
23	9	10	1	S9	73		301	1	K33
24		153	4	S10	74	22	23	1	S71
25		301	1	K12	75		166	4	S72
26		301	1	K13	76		301	1	K34
27	10	11	1	S9	77	23	24	1	S71
28		154	4	S10	78		167	4	S72
29		301	1	K14	79		301	1	K35
30		301	1	K15	80	24	25	1	S71
31	11	12	1	S9	81		168	4	S72
32		155	4	S10	82		301	1	K36
33		301	1	K16	83		301	1	K37
34		301	1	K17	84	25	26	1	S71
35	12	13	1	S9	85		169	4	S72
36		156	4	S10	86		301	1	K38
37		301	1	K18	87		301	1	K39
38		301	1	K19	88	26	27	1	S67
39	13	14	1	S9	89		170	4	S72
40		157	4	S10	90		301	1	K40
41		301	1	K20	91		301	1	K41
42		301	1	K21	92	27	28	1	S9
43	14	15	1	S9	93		171	4	S10
44		158	4	S10	94		301	1	K42
45		301	1	K22	95		301	1	K43
46		301	1	K23	96	28	29	1	S9
47	15	16	1	S9	97		172	4	S10
48		159	4	S10	98		301	1	K44
49		301	1	K24	99		301	1	K45
50		301	1	S42	100	29	30	1	S9

BRANCH	NODE	TON	TAG	I, C, S	BRANCH	NODE	TON	TAG	I, C, S
101		173	4	S10	151		301	1	K71
102		301	1	K46	152	42	43	1	S67
103		301	1	K47	153		186	4	S10
104	30	31	1	S9	154		301	1	K72
105		174	4	S10	155		301	1	K73
106		301	1	K48	156	43	44	1	S71
107		301	1	K49	157		187	4	S72
108	31	32	1	S9	158		301	1	K74
109		175	4	S10	159		301	1	K75
110		301	1	K50	160	44	45	1	S71
111		301	1	K51	161		188	4	S72
112	32	33	1	S9	162		301	1	K76
113		176	4	S10	163		301	1	K77
114		301	1	K52	164	45	46	1	S71
115		301	1	K53	165		189	4	S72
116	33	34	1	S9	166		301	1	K78
117		177	4	S10	167	46	47	1	S71
118		301	1	K54	168		190	4	S72
119		301	1	K55	169		301	1	K79
120	34	35	1	S9	170		301	1	K80
121		178	4	S10	171	47	48	1	S71
122		301	1	K56	172		191	4	S72
123		301	1	K57	173		301	1	K81
124	35	36	1	S9	174		301	1	K82
125		179	4	S10	175	48	49	1	S67
126		301	1	K58	176		192	4	S72
127		301	1	K59	177		301	1	K83
128	36	37	1	S9	178		301	1	K84
129		180	4	S10	179	49	50	1	S9
130		301	1	K60	180		193	4	S10
131		301	1	K61	181		301	1	K85
132	37	38	1	S9	182		301	1	K86
133		181	4	S10	183	50	51	1	S9
134		301	1	K62	184		194	4	S10
135		301	1	K63	185		301	1	K87
136	38	39	1	S9	186		301	1	K88
137		182	4	S10	187	51	52	1	S9
138		301	1	K64	188		195	4	S10
139		301	1	K65	189		301	1	K89
140	39	40	1	S9	190		301	1	K90
141		183	4	S10	191	52	53	1	S9
142		301	1	K66	192		196	4	S10
143		301	1	K67	193		301	1	K91
144	40	41	1	S9	194		301	1	K92
145		184	4	S10	195	53	54	1	S9
146		301	1	K68	196		197	4	S10
147		301	1	K69	197		301	1	K93
148	41	42	1	S9	198		301	1	K94
149		185	4	S10	199	54	55	1	S9
150		301	1	K70	200		198	4	S10

BRANCH	NODE	TON	TAG	I. C. S	BRANCH	NODE	TON	TAG	I. C. S
201		301	1	K95	251	67	68	1	K126
202		301	1	K96	252		211	4	K127
203	55	56	1	S9	253		301	1	K128
204		199	4	S10	254		301	1	K129
205		301	1	K97	255	68	69	1	K130
206		301	1	K98	256		212	4	K131
207	56	57	1	S9	257		301	1	K132
208		200	4	S10	258		301	1	K133
209		301	1	K99	259	69	70	1	K134
210		301	1	K100	260		213	4	S256
211	57	58	1	S9	261		301	1	K135
212		201	4	S10	262		301	1	K136
213		301	1	K101	263	70	71	1	S71
214		301	1	K102	264		214	4	S72
215	58	59	1	S9	265		301	1	K137
216		202	4	S10	266		301	1	K138
217		301	1	K103	267	71	72	1	S71
218		301	1	K104	268		215	4	S72
219	59	60	1	S9	269		301	1	K139
220		203	4	S10	270		301	1	K140
221		301	1	K105	271	72	73	1	S71
222		301	1	K106	272		216	4	S72
223	60	61	1	S9	273		301	1	K141
224		204	4	S10	274		301	1	K142
225		301	1	K107	275	73	74	1	S71
226		301	1	K108	276		217	4	S72
227	61	62	1	S9	277		301	1	S274
228		205	4	S10	278		301	1	K143
229		301	1	K109	279	74	75	1	S71
230		301	1	K110	280		218	4	S72
231	62	63	1	S9	281		301	1	S270
232		206	4	S10	282		301	1	K144
233		301	1	K111	283	75	76	1	S259
234		301	1	K112	284		219	4	S72
235	63	64	1	S9	285		301	1	S266
236		207	4	S10	286		301	1	K145
237		301	1	K113	287	76	77	1	S255
238		301	1	K114	288		220	4	S256
239	64	65	1	K115	289		301	1	S262
240		208	4	S10	290		301	1	K146
241		301	1	K116	291	77	78	1	S251
242		301	1	K117	292		221	4	S256
243	65	66	1	K118	293		301	1	S258
244		209	4	K119	294		301	1	K147
245		301	1	K120	295	78	79	1	S247
246		301	1	K121	296		222	4	S252
247	66	67	1	K122	297		301	1	K148
248		210	4	K123	298		301	1	K149
249		301	1	K124	299	79	80	1	S243
250		301	1	K125	300		223	4	S248

BRANCH	NODE	TON	TAG	I. C. S	BRANCH	NODE	TON	TAG	I. C. S
301		301	1	K150	352		236	4	S10
302		301	1	K151	353		301	1	K176
303	80	81	1	S239	354		301	1	K177
304		224	4	S244	355	93	94	1	S9
305		301	1	K152	356		237	4	S10
306		301	1	K153	357		301	1	K178
307	81	82	1	S9	358		301	1	K179
308		225	4	S10	359	94	95	1	S9
309		301	1	K154	360		238	4	S10
310		301	1	K155	361		301	1	K180
311	82	83	1	S9	362		301	1	K181
312		226	4	S10	363	95	96	1	S9
313		301	1	K156	364		239	4	S10
314		301	1	K157	365		301	1	K182
315	83	84	1	S9	366		301	1	K183
316		227	4	S10	367	96	97	1	S67
317		301	1	K158	368		240	4	S10
318		301	1	K159	369		301	1	K184
319	84	85	1	S9	370		301	1	K185
320		228	4	S10	371	97	98	1	S71
321		301	1	K160	372		241	4	S72
322		301	1	K161	373		301	1	K186
323	85	86	1	S9	374		301	1	K187
324		229	4	S10	375	98	99	1	S71
325		301	1	K162	376		242	4	S72
326		301	1	K163	377		301	1	K188
327	86	87	1	S9	378		301	1	K189
328		230	4	S10	379	99	100	1	S71
329		301	1	K164	380		243	4	S72
330		301	1	K165	381		301	1	K190
331	87	88	1	S9	382		301	1	K191
332		231	4	S10	383	100	101	1	S71
333		301	1	K166	384		244	4	S72
334		301	1	K167	385		301	1	K192
335	88	89	1	S9	386	101	102	1	S71
336		232	4	S10	387		245	4	S72
337		301	1	K168	388		301	1	S163
338		301	1	K169	389		301	1	K193
339	89	90	1	S9	390	102	103	1	S67
340		233	4	S10	391		246	4	S72
341		301	1	K170	392		301	1	S159
342		301	1	K171	393		301	1	K194
343	90	91	1	S9	394	103	104	1	S9
344		234	4	S10	395		247	4	S10
345		301	1	K172	396		301	1	K195
346		301	1	K173	397		301	1	K196
347	91	92	1	S9	398	104	105	1	S9
348		235	4	S10	399		248	4	S10
349		301	1	K174	400		301	1	K197
350		301	1	K175	401		301	1	K198
351	92	93	1	S9	402	105	106	1	S9

BRANCH	NODE	TON	TAG	I. C. S	BRANCH	NODE	TON	TAG	I. C. S
403		249	4	S10	453		301	1	K224
404		301	1	K199	454	118	119	1	S67
405		301	1	K200	455		262	4	S10
406	106	107	1	S9	456		301	1	K225
407		250	4	S10	457		301	1	K226
408		301	1	K201	458	119	120	1	S71
409		301	1	K202	459		263	4	S72
410	107	108	1	S9	460		301	1	K227
411		251	4	S10	461		301	1	K228
412		301	1	K203	462	120	121	1	S71
413		301	1	K204	463		264	4	S72
414	108	109	1	S9	464		301	1	K229
415		252	4	S10	465		301	1	K230
416		301	1	K205	466	121	122	1	S71
417		301	1	K206	467		265	4	S72
418	109	110	1	S9	468		301	1	K231
419		253	4	S10	469		301	1	K232
420		301	1	K207	470	122	123	1	S71
421		301	1	K208	471		266	4	S72
422	110	111	1	S9	472		301	1	K233
423		254	4	S10	473	123	124	1	S71
424		301	1	K209	474		267	4	S72
425		301	1	K210	475		301	1	K234
426	111	112	1	S9	476	124	125	1	S67
427		255	4	S10	477		268	4	S72
428		301	1	K211	478		301	1	K235
429		301	1	K212	479	125	126	1	S9
430	112	113	1	S9	480		269	4	S10
431		256	4	S10	481		301	1	S22
432		301	1	K213	482		301	1	K236
433		301	1	K214	483	126	127	1	S9
434	113	114	1	S9	484		270	4	S10
435		257	4	S10	485		301	1	S26
436		301	1	K215	486		301	1	K237
437		301	1	K216	487	127	128	1	S9
438	114	115	1	S9	488		271	4	S10
439		258	4	S10	489		301	1	S30
440		301	1	K217	490		301	1	K238
441		301	1	K218	491	128	129	1	S9
442	115	116	1	S9	492		272	4	S10
443		259	4	S10	493		301	1	S34
444		301	1	K219	494		301	1	K239
445		301	1	K220	495	129	130	1	S9
446	116	117	1	S9	496		273	4	S10
447		260	4	S10	497		301	1	S38
448		301	1	K221	498		301	1	K240
449		301	1	K222	499	130	131	1	S9
450	117	118	1	S9	500		274	4	S10
451		261	4	S10	501		301	1	S42
452		301	1	K223	502		301	1	K241

BRANCH	NODE	TON	TAG	I, C, S	BRANCH	NODE	TON	TAG	I, C, S
503	131	132	1	S9	553				
504		275	4	S10	554				
505		301	1	S46	555				
506		301	1	K242	556				
507	132	133	1	S9	557				
508		276	4	S10	558				
509		301	1	S42	559				
510		301	1	K243	560				
511	133	134	1	S9	561				
512		277	4	S10	562				
513		301	1	S38	563				
514		301	1	K244	564				
515	134	135	1	S9	565				
516		278	4	S10	566				
517		301	1	S34	567				
518		301	1	K245	568				
519	135	136	1	S9	569				
520		279	4	S10	570				
521		301	1	S30	571				
522		301	1	K246	572				
523	136	137	1	S9	573				
524		280	4	S10	574				
525		301	1	S26	575				
526		301	1	K247	576				
527	137	138	1	S9	577				
528		281	4	S10	578				
529		301	1	S22	579				
530		301	1	K248	580				
531	138	139	1	S9	581				
532		282	4	S10	582				
533		301	1	S18	583				
534		301	1	K249	584				
535	139	140	1	S9	585				
536		283	4	S10	586				
537		301	1	K250	587				
538	140	141	1	S7	588				
539		284	4	S10	589				
540		301	1	K251	590				
541	141	142	1	S1	591				
542		285	4	S2	592				
543	142	143	1	S1	593				
544		286	4	S2	594				
545	143	144	1	S1	595				
546		287	4	S2	596				
547	144	288	4	S2	597				
548					598				
549					599				
550					600				
551					601				
552					602				

BRANCH	NODE	TON	TAG	I, C, S	BRANCH	NODE	TON	TAG	I, C, S
701	145	302	5	k252	751	195	194	5	S701
702	146	145	5	S701	752	196	195	5	S701
703	147	146	5	S701	753	197	196	5	S701
704	148	147	5	S701	754	198	197	5	S701
705	149	148	5	S701	755	199	198	5	S701
706	150	149	5	S701	756	200	199	5	S701
707	151	150	5	S701	757	201	200	5	S701
708	152	151	5	S701	758	202	201	5	S701
709	153	152	5	S701	759	203	202	5	S701
710	154	153	5	S701	760	204	203	5	S701
711	155	154	5	S701	761	205	204	5	S701
712	156	155	5	S701	762	206	205	5	S701
713	157	156	5	S701	763	207	206	5	S701
714	158	157	5	S701	764	208	207	5	S701
715	159	158	5	S701	765	209	208	5	S701
716	160	159	5	S701	766	210	209	5	S701
717	161	160	5	S701	767	211	210	5	S701
718	162	161	5	S701	768	212	211	5	S701
719	163	162	5	S701	769	213	212	5	S701
720	164	163	5	S701	770	214	213	5	S701
721	165	164	5	S701	771	215	214	5	S701
722	166	165	5	S701	772	216	215	5	S701
723	167	166	5	S701	773	217	216	5	S701
724	168	167	5	S701	774	218	217	5	S701
725	169	168	5	S701	775	219	218	5	S701
726	170	169	5	S701	776	220	219	5	S701
727	171	170	5	S701	777	221	220	5	S701
728	172	171	5	S701	778	222	221	5	S701
729	173	172	5	S701	779	223	222	5	S701
730	174	173	5	S701	780	224	223	5	S701
731	175	174	5	S701	781	225	224	5	S701
732	176	175	5	S701	782	226	225	5	S701
733	177	176	5	S701	783	227	226	5	S701
734	178	177	5	S701	784	228	227	5	S701
735	179	178	5	S701	785	229	228	5	S701
736	180	179	5	S701	786	230	229	5	S701
737	181	180	5	S701	787	231	230	5	S701
738	182	181	5	S701	788	232	231	5	S701
739	183	182	5	S701	789	233	232	5	S701
740	184	183	5	S701	790	234	233	5	S701
741	185	184	5	S701	791	235	234	5	S701
742	186	185	5	S701	792	236	235	5	S701
743	187	186	5	S701	793	237	236	5	S701
744	188	187	5	S701	794	238	237	5	S701
745	189	188	5	S701	795	239	238	5	S701
746	190	189	5	S701	796	240	239	5	S701
747	191	190	5	S701	797	241	240	5	S701
748	192	191	5	S701	798	242	241	5	S701
749	193	192	5	S701	799	243	242	5	S701
750	194	193	5	S701	800	244	243	5	S701

BRANCH	NODE	TON	TAG	I, C, S	BRANCH	NODE	TON	TAG	I, C, S
801	245	244	5	S701	851				
802	246	245	5	S701	852				
803	247	246	5	S701	853				
804	248	247	5	S701	854				
805	249	248	5	S701	855				
806	250	249	5	S701	856				
807	251	250	5	S701	857				
808	252	251	5	S701	858				
809	253	252	5	S701	859				
810	254	253	5	S701	860				
811	255	254	5	S701	861				
812	256	255	5	S701	862				
813	257	256	5	S701	863				
814	258	257	5	S701	864				
815	259	258	5	S701	865				
816	260	259	5	S701	866				
817	261	260	5	S701	867				
818	262	261	5	S701	868				
819	263	262	5	S701	869				
820	264	263	5	S701	870				
821	265	264	5	S701	871				
822	266	265	5	S701	872				
823	267	266	5	S701	873				
824	268	267	5	S701	874				
825	269	268	5	S701	875				
826	270	269	5	S701	876				
827	271	270	5	S701	877				
828	272	271	5	S701	878				
829	273	272	5	S701	879				
830	274	273	5	S701	880				
831	275	274	5	S701	881				
832	276	275	5	S701	882				
833	277	276	5	S701	883				
834	278	277	5	S701	884				
835	279	278	5	S701	885				
836	280	279	5	S701	886				
837	281	280	5	S701	887				
838	282	281	5	S701	888				
839	283	282	5	S701	889				
840	284	283	5	S701	890				
841	285	284	5	S701	891				
842	286	285	5	S701	892				
843	287	286	5	S701	893				
844	288	287	5	S701	894				
845					895				
846					896				
847					897				
848					898				
849					899				
850					900				

TASS Branch Connection Summary in W/degC or Watts if Tag = 10

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
1	1	2	1	.178E+01	57	17	301	1	.860E-01	113	32	176	4	.701E+00
2	1	145	4	.576E+00	58	17	301	1	.910E-01	114	32	301	1	.860E-01
3	2	3	1	.178E+01	59	18	19	1	.146E+01	115	32	301	1	.830E-01
4	2	146	4	.576E+00	60	18	162	4	.701E+00	116	33	34	1	.146E+01
5	3	4	1	.178E+01	61	18	301	1	.860E-01	117	33	177	4	.701E+00
6	3	147	4	.576E+00	62	18	301	1	.820E-01	118	33	301	1	.860E-01
7	4	5	1	.160E+01	63	19	20	1	.146E+01	119	33	301	1	.830E-01
8	4	148	4	.576E+00	64	19	163	4	.701E+00	120	34	35	1	.146E+01
9	5	6	1	.146E+01	65	19	301	1	.870E-01	121	34	178	4	.701E+00
10	5	149	4	.701E+00	66	19	301	1	.680E-01	122	34	301	1	.860E-01
11	5	301	1	.954E-01	67	20	21	1	.129E+01	123	34	301	1	.830E-01
12	6	7	1	.146E+01	68	20	164	4	.701E+00	124	35	36	1	.146E+01
13	6	150	4	.701E+00	69	20	301	1	.870E-01	125	35	179	4	.701E+00
14	6	301	1	.940E-01	70	20	301	1	.490E-01	126	35	301	1	.860E-01
15	7	8	1	.146E+01	71	21	22	1	.115E+01	127	35	301	1	.820E-01
16	7	151	4	.701E+00	72	21	165	4	.889E+00	128	36	37	1	.146E+01
17	7	301	1	.920E-01	73	21	301	1	.940E-01	129	36	180	4	.701E+00
18	7	301	1	.240E-01	74	22	23	1	.115E+01	130	36	301	1	.860E-01
19	8	9	1	.146E+01	75	22	166	4	.889E+00	131	36	301	1	.810E-01
20	8	152	4	.701E+00	76	22	301	1	.770E-01	132	37	38	1	.146E+01
21	8	301	1	.910E-01	77	23	24	1	.115E+01	133	37	181	4	.701E+00
22	8	301	1	.490E-01	78	23	167	4	.889E+00	134	37	301	1	.850E-01
23	9	10	1	.146E+01	79	23	301	1	.420E-01	135	37	301	1	.800E-01
24	9	153	4	.701E+00	80	24	25	1	.115E+01	136	38	39	1	.146E+01
25	9	301	1	.890E-01	81	24	168	4	.889E+00	137	38	182	4	.701E+00
26	9	301	1	.680E-01	82	24	301	1	.136E+00	138	38	301	1	.850E-01
27	10	11	1	.146E+01	83	24	301	1	.220E-01	139	38	301	1	.780E-01
28	10	154	4	.701E+00	84	25	26	1	.115E+01	140	39	40	1	.146E+01
29	10	301	1	.880E-01	85	25	169	4	.889E+00	141	39	183	4	.701E+00
30	10	301	1	.820E-01	86	25	301	1	.117E+00	142	39	301	1	.850E-01
31	11	12	1	.146E+01	87	25	301	1	.640E-01	143	39	301	1	.770E-01
32	11	155	4	.701E+00	88	26	27	1	.128E+01	144	40	41	1	.146E+01
33	11	301	1	.870E-01	89	26	170	4	.889E+00	145	40	184	4	.701E+00
34	11	301	1	.910E-01	90	26	301	1	.101E+00	146	40	301	1	.850E-01
35	12	13	1	.146E+01	91	26	301	1	.850E-01	147	40	301	1	.750E-01
36	12	156	4	.701E+00	92	27	28	1	.146E+01	148	41	42	1	.146E+01
37	12	301	1	.860E-01	93	27	171	4	.701E+00	149	41	185	4	.701E+00
38	12	301	1	.970E-01	94	27	301	1	.890E-01	150	41	301	1	.850E-01
39	13	14	1	.146E+01	95	27	301	1	.810E-01	151	41	301	1	.730E-01
40	13	157	4	.701E+00	96	28	29	1	.146E+01	152	42	43	1	.129E+01
41	13	301	1	.850E-01	97	28	172	4	.701E+00	153	42	186	4	.701E+00
42	13	301	1	.100E+00	98	28	301	1	.880E-01	154	42	301	1	.850E-01
43	14	15	1	.146E+01	99	28	301	1	.810E-01	155	42	301	1	.710E-01
44	14	158	4	.701E+00	100	29	30	1	.146E+01	156	43	44	1	.115E+01
45	14	301	1	.850E-01	101	29	173	4	.701E+00	157	43	187	4	.889E+00
46	14	301	1	.101E+00	102	29	301	1	.870E-01	158	43	301	1	.910E-01
47	15	16	1	.146E+01	103	29	301	1	.820E-01	159	43	301	1	.124E+00
48	15	159	4	.701E+00	104	30	31	1	.146E+01	160	44	45	1	.115E+01
49	15	301	1	.850E-01	105	30	174	4	.701E+00	161	44	188	4	.889E+00
50	15	301	1	.100E+00	106	30	301	1	.870E-01	162	44	301	1	.730E-01
51	16	17	1	.146E+01	107	30	301	1	.830E-01	163	44	301	1	.920E-01
52	16	160	4	.701E+00	108	31	32	1	.146E+01	164	45	46	1	.115E+01
53	16	301	1	.850E-01	109	31	175	4	.701E+00	165	45	189	4	.889E+00
54	16	301	1	.970E-01	110	31	301	1	.870E-01	166	45	301	1	.390E-01
55	17	18	1	.146E+01	111	31	301	1	.830E-01	167	46	47	1	.115E+01
56	17	161	4	.701E+00	112	32	33	1	.146E+01	168	46	190	4	.889E+00

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
169	46	301	1	.150E+00	225	60	301	1	.860E-01	281	74	301	1	.138E+00
170	46	301	1	.250E-01	226	60	301	1	.810E-01	282	74	301	1	.700E-01
171	47	48	1	.115E+01	227	61	62	1	.146E+01	283	75	76	1	.120E+01
172	47	191	4	.889E+00	228	61	205	4	.701E+00	284	75	219	4	.889E+00
173	47	301	1	.127E+00	229	61	301	1	.860E-01	285	75	301	1	.157E+00
174	47	301	1	.690E-01	230	61	301	1	.810E-01	286	75	301	1	.900E-01
175	48	49	1	.129E+01	231	62	63	1	.146E+01	287	76	77	1	.125E+01
176	48	192	4	.889E+00	232	62	206	4	.701E+00	288	76	220	4	.655E+00
177	48	301	1	.100E+00	233	62	301	1	.860E-01	289	76	301	1	.171E+00
178	48	301	1	.890E-01	234	62	301	1	.810E-01	290	76	301	1	.980E-01
179	49	50	1	.146E+01	235	63	64	1	.146E+01	291	77	78	1	.210E+01
180	49	193	4	.701E+00	236	63	207	4	.701E+00	292	77	221	4	.655E+00
181	49	301	1	.880E-01	237	63	301	1	.860E-01	293	77	301	1	.172E+00
182	49	301	1	.830E-01	238	63	301	1	.800E-01	294	77	301	1	.970E-01
183	50	51	1	.146E+01	239	64	65	1	.108E+01	295	78	79	1	.172E+01
184	50	194	4	.701E+00	240	64	208	4	.701E+00	296	78	222	4	.542E+00
185	50	301	1	.870E-01	241	64	301	1	.860E-01	297	78	301	1	.124E+00
186	50	301	1	.830E-01	242	64	301	1	.790E-01	298	78	301	1	.910E-01
187	51	52	1	.146E+01	243	65	66	1	.992E+00	299	79	80	1	.992E+00
188	51	195	4	.701E+00	244	65	209	4	.990E+00	300	79	223	4	.815E+00
189	51	301	1	.870E-01	245	65	301	1	.940E-01	301	79	301	1	.108E+00
190	51	301	1	.830E-01	246	65	301	1	.870E-01	302	79	301	1	.870E-01
191	52	53	1	.146E+01	247	66	67	1	.172E+01	303	80	81	1	.108E+01
192	52	196	4	.701E+00	248	66	210	4	.815E+00	304	80	224	4	.990E+00
193	52	301	1	.870E-01	249	66	301	1	.930E-01	305	80	301	1	.930E-01
194	52	301	1	.830E-01	250	66	301	1	.103E+00	306	80	301	1	.910E-01
195	53	54	1	.146E+01	251	67	68	1	.210E+01	307	81	82	1	.146E+01
196	53	197	4	.701E+00	252	67	211	4	.542E+00	308	81	225	4	.701E+00
197	53	301	1	.870E-01	253	67	301	1	.930E-01	309	81	301	1	.840E-01
198	53	301	1	.830E-01	254	67	301	1	.125E+00	310	81	301	1	.830E-01
199	54	55	1	.146E+01	255	68	69	1	.125E+01	311	82	83	1	.146E+01
200	54	198	4	.701E+00	256	68	212	4	.655E+00	312	82	226	4	.701E+00
201	54	301	1	.870E-01	257	68	301	1	.990E-01	313	82	301	1	.850E-01
202	54	301	1	.830E-01	258	68	301	1	.172E+00	314	82	301	1	.820E-01
203	55	56	1	.146E+01	259	69	70	1	.120E+01	315	83	84	1	.146E+01
204	55	199	4	.701E+00	260	69	213	4	.655E+00	316	83	227	4	.701E+00
205	55	301	1	.870E-01	261	69	301	1	.990E-01	317	83	301	1	.850E-01
206	55	301	1	.830E-01	262	69	301	1	.171E+00	318	83	301	1	.820E-01
207	56	57	1	.146E+01	263	70	71	1	.115E+01	319	84	85	1	.146E+01
208	56	200	4	.701E+00	264	70	214	4	.889E+00	320	84	228	4	.701E+00
209	56	301	1	.870E-01	265	70	301	1	.900E-01	321	84	301	1	.860E-01
210	56	301	1	.820E-01	266	70	301	1	.157E+00	322	84	301	1	.820E-01
211	57	58	1	.146E+01	267	71	72	1	.115E+01	323	85	86	1	.146E+01
212	57	201	4	.701E+00	268	71	215	4	.889E+00	324	85	229	4	.701E+00
213	57	301	1	.860E-01	269	71	301	1	.710E-01	325	85	301	1	.860E-01
214	57	301	1	.820E-01	270	71	301	1	.138E+00	326	85	301	1	.820E-01
215	58	59	1	.146E+01	271	72	73	1	.115E+01	327	86	87	1	.146E+01
216	58	202	4	.701E+00	272	72	216	4	.889E+00	328	86	230	4	.701E+00
217	58	301	1	.860E-01	273	72	301	1	.1330E-01	329	86	301	1	.860E-01
218	58	301	1	.820E-01	274	72	301	1	.670E-01	330	86	301	1	.820E-01
219	59	60	1	.146E+01	275	73	74	1	.115E+01	331	87	88	1	.146E+01
220	59	203	4	.701E+00	276	73	217	4	.889E+00	332	87	231	4	.701E+00
221	59	301	1	.860E-01	277	73	301	1	.670E-01	333	87	301	1	.860E-01
222	59	301	1	.820E-01	278	73	301	1	.1310E-01	334	87	301	1	.820E-01
223	60	61	1	.146E+01	279	74	75	1	.115E+01	335	88	89	1	.146E+01
224	60	204	4	.701E+00	280	74	218	4	.889E+00	336	88	232	4	.701E+00

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
337	88	301	1	.850E+01	393	102	301	1	.900E+01	449	116	301	1	.830E+01
338	88	301	1	.820E+01	394	103	104	1	.146E+01	450	117	118	1	.146E+01
339	89	90	1	.146E+01	395	103	247	4	.701E+00	451	117	261	4	.701E+00
340	89	233	4	.701E+00	396	103	301	1	.760E+01	452	117	301	1	.830E+01
341	89	301	1	.850E+01	397	103	301	1	.840E+01	453	117	301	1	.830E+01
342	89	301	1	.810E+01	398	104	105	1	.146E+01	454	118	119	1	.129E+01
343	90	91	1	.146E+01	399	104	248	4	.701E+00	455	118	262	4	.701E+00
344	90	234	4	.701E+00	400	104	301	1	.780E+01	456	118	301	1	.820E+01
345	90	301	1	.850E+01	401	104	301	1	.840E+01	457	118	301	1	.840E+01
346	90	301	1	.810E+01	402	105	106	1	.146E+01	458	119	120	1	.115E+01
347	91	92	1	.146E+01	403	105	249	4	.701E+00	459	119	263	4	.889E+00
348	91	235	4	.701E+00	404	105	301	1	.790E+01	460	119	301	1	.860E+01
349	91	301	1	.850E+01	405	105	301	1	.830E+01	461	119	301	1	.960E+01
350	91	301	1	.810E+01	406	106	107	1	.146E+01	462	120	121	1	.115E+01
351	92	93	1	.146E+01	407	106	250	4	.701E+00	463	120	264	4	.889E+00
352	92	236	4	.701E+00	408	106	301	1	.810E+01	464	120	301	1	.650E+01
353	92	301	1	.850E+01	409	106	301	1	.830E+01	465	120	301	1	.113E+00
354	92	301	1	.810E+01	410	107	108	1	.146E+01	466	121	122	1	.115E+01
355	93	94	1	.146E+01	411	107	251	4	.701E+00	467	121	265	4	.889E+00
356	93	237	4	.701E+00	412	107	301	1	.820E+01	468	121	301	1	.133E+01
357	93	301	1	.850E+01	413	107	301	1	.830E+01	469	121	301	1	.133E+01
358	93	301	1	.810E+01	414	108	109	1	.146E+01	470	122	123	1	.115E+01
359	94	95	1	.146E+01	415	108	252	4	.701E+00	471	122	266	4	.889E+00
360	94	238	4	.701E+00	416	108	301	1	.840E+01	472	122	301	1	.420E+01
361	94	301	1	.850E+01	417	108	301	1	.830E+01	473	123	124	1	.115E+01
362	94	301	1	.810E+01	418	109	110	1	.146E+01	474	123	267	4	.889E+00
363	95	96	1	.146E+01	419	109	253	4	.701E+00	475	123	301	1	.760E+01
364	95	239	4	.701E+00	420	109	301	1	.850E+01	476	124	125	1	.129E+01
365	95	301	1	.850E+01	421	109	301	1	.830E+01	477	124	268	4	.889E+00
366	95	301	1	.810E+01	422	110	111	1	.146E+01	478	124	301	1	.940E+01
367	96	97	1	.129E+01	423	110	254	4	.701E+00	479	125	126	1	.146E+01
368	96	240	4	.701E+00	424	110	301	1	.850E+01	480	125	269	4	.701E+00
369	96	301	1	.840E+01	425	110	301	1	.830E+01	481	125	301	1	.490E+01
370	96	301	1	.800E+01	426	111	112	1	.146E+01	482	125	301	1	.860E+01
371	97	98	1	.115E+01	427	111	255	4	.701E+00	483	126	127	1	.146E+01
372	97	241	4	.889E+00	428	111	301	1	.850E+01	484	126	270	4	.701E+00
373	97	301	1	.900E+01	429	111	301	1	.830E+01	485	126	301	1	.680E+01
374	97	301	1	.930E+01	430	112	113	1	.146E+01	486	126	301	1	.860E+01
375	98	99	1	.115E+01	431	112	256	4	.701E+00	487	127	128	1	.146E+01
376	98	242	4	.889E+00	432	112	301	1	.850E+01	488	127	271	4	.701E+00
377	98	301	1	.690E+01	433	112	301	1	.830E+01	489	127	301	1	.820E+01
378	98	301	1	.123E+00	434	113	114	1	.146E+01	490	127	301	1	.850E+01
379	99	100	1	.115E+01	435	113	257	4	.701E+00	491	128	129	1	.146E+01
380	99	243	4	.889E+00	436	113	301	1	.850E+01	492	128	272	4	.701E+00
381	99	301	1	.260E+01	437	113	301	1	.830E+01	493	128	301	1	.910E+01
382	99	301	1	.149E+00	438	114	115	1	.146E+01	494	128	301	1	.840E+01
383	100	101	1	.115E+01	439	114	258	4	.701E+00	495	129	130	1	.146E+01
384	100	244	4	.889E+00	440	114	301	1	.850E+01	496	129	273	4	.701E+00
385	100	301	1	.380E+01	441	114	301	1	.830E+01	497	129	301	1	.970E+01
386	101	102	1	.115E+01	442	115	116	1	.146E+01	498	129	301	1	.830E+01
387	101	245	4	.889E+00	443	115	259	4	.701E+00	499	130	131	1	.146E+01
388	101	301	1	.920E+01	444	115	301	1	.840E+01	500	130	274	4	.701E+00
389	101	301	1	.720E+01	445	115	301	1	.830E+01	501	130	301	1	.100E+00
390	102	103	1	.129E+01	446	116	117	1	.146E+01	502	130	301	1	.830E+01
391	102	246	4	.889E+00	447	116	260	4	.701E+00	503	131	132	1	.146E+01
392	102	301	1	.124E+00	448	116	301	1	.840E+01	504	131	275	4	.701E+00

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
505	131	301	1	.101E+00	561	158	157	5	.174E+03	617	214	213	5	.174E+03
506	131	301	1	.830E-01	562	159	158	5	.174E+03	618	215	214	5	.174E+03
507	132	133	1	.146E+01	563	160	159	5	.174E+03	619	216	215	5	.174E+03
508	132	276	4	.701E+00	564	161	160	5	.174E+03	620	217	216	5	.174E+03
509	132	301	1	1.000E+00	565	162	161	5	.174E+03	621	218	217	5	.174E+03
510	132	301	1	.830E-01	566	163	162	5	.174E+03	622	219	218	5	.174E+03
511	133	134	1	.146E+01	567	164	163	5	.174E+03	623	220	219	5	.174E+03
512	133	277	4	.701E+00	568	165	164	5	.174E+03	624	221	220	5	.174E+03
513	133	301	1	.970E-01	569	166	165	5	.174E+03	625	222	221	5	.174E+03
514	133	301	1	.830E-01	570	167	166	5	.174E+03	626	223	222	5	.174E+03
515	134	135	1	.146E+01	571	168	167	5	.174E+03	627	224	223	5	.174E+03
516	134	278	4	.701E+00	572	169	168	5	.174E+03	628	225	224	5	.174E+03
517	134	301	1	.910E-01	573	170	169	5	.174E+03	629	226	225	5	.174E+03
518	134	301	1	.840E-01	574	171	170	5	.174E+03	630	227	226	5	.174E+03
519	135	136	1	.146E+01	575	172	171	5	.174E+03	631	228	227	5	.174E+03
520	135	279	4	.701E+00	576	173	172	5	.174E+03	632	229	228	5	.174E+03
521	135	301	1	.820E-01	577	174	173	5	.174E+03	633	230	229	5	.174E+03
522	135	301	1	.840E-01	578	175	174	5	.174E+03	634	231	230	5	.174E+03
523	136	137	1	.146E+01	579	176	175	5	.174E+03	635	232	231	5	.174E+03
524	136	280	4	.701E+00	580	177	176	5	.174E+03	636	233	232	5	.174E+03
525	136	301	1	.680E-01	581	178	177	5	.174E+03	637	234	233	5	.174E+03
526	136	301	1	.860E-01	582	179	178	5	.174E+03	638	235	234	5	.174E+03
527	137	138	1	.146E+01	583	180	179	5	.174E+03	639	236	235	5	.174E+03
528	137	281	4	.701E+00	584	181	180	5	.174E+03	640	237	236	5	.174E+03
529	137	301	1	.490E-01	585	182	181	5	.174E+03	641	238	237	5	.174E+03
530	137	301	1	.870E-01	586	183	182	5	.174E+03	642	239	238	5	.174E+03
531	138	139	1	.146E+01	587	184	183	5	.174E+03	643	240	239	5	.174E+03
532	138	282	4	.701E+00	588	185	184	5	.174E+03	644	241	240	5	.174E+03
533	138	301	1	.240E-01	589	186	185	5	.174E+03	645	242	241	5	.174E+03
534	138	301	1	.880E-01	590	187	186	5	.174E+03	646	243	242	5	.174E+03
535	139	140	1	.146E+01	591	188	187	5	.174E+03	647	244	243	5	.174E+03
536	139	283	4	.701E+00	592	189	188	5	.174E+03	648	245	244	5	.174E+03
537	139	301	1	.900E-01	593	190	189	5	.174E+03	649	246	245	5	.174E+03
538	140	141	1	.160E+01	594	191	190	5	.174E+03	650	247	246	5	.174E+03
539	140	284	4	.701E+00	595	192	191	5	.174E+03	651	248	247	5	.174E+03
540	140	301	1	.910E-01	596	193	192	5	.174E+03	652	249	248	5	.174E+03
541	141	142	1	.178E+01	597	194	193	5	.174E+03	653	250	249	5	.174E+03
542	141	285	4	.576E+00	598	195	194	5	.174E+03	654	251	250	5	.174E+03
543	142	143	1	.178E+01	599	196	195	5	.174E+03	655	252	251	5	.174E+03
544	142	286	4	.576E+00	600	197	196	5	.174E+03	656	253	252	5	.174E+03
545	143	144	1	.178E+01	601	198	197	5	.174E+03	657	254	253	5	.174E+03
546	143	287	4	.576E+00	602	199	198	5	.174E+03	658	255	254	5	.174E+03
547	144	288	4	.576E+00	603	200	199	5	.174E+03	659	256	255	5	.174E+03
548	145	302	5	.174E+03	604	201	200	5	.174E+03	660	257	256	5	.174E+03
549	146	145	5	.174E+03	605	202	201	5	.174E+03	661	258	257	5	.174E+03
550	147	146	5	.174E+03	606	203	202	5	.174E+03	662	259	258	5	.174E+03
551	148	147	5	.174E+03	607	204	203	5	.174E+03	663	260	259	5	.174E+03
552	149	148	5	.174E+03	608	205	204	5	.174E+03	664	261	260	5	.174E+03
553	150	149	5	.174E+03	609	206	205	5	.174E+03	665	262	261	5	.174E+03
554	151	150	5	.174E+03	610	207	206	5	.174E+03	666	263	262	5	.174E+03
555	152	151	5	.174E+03	611	208	207	5	.174E+03	667	264	263	5	.174E+03
556	153	152	5	.174E+03	612	209	208	5	.174E+03	668	265	264	5	.174E+03
557	154	153	5	.174E+03	613	210	209	5	.174E+03	669	266	265	5	.174E+03
558	155	154	5	.174E+03	614	211	210	5	.174E+03	670	267	266	5	.174E+03
559	156	155	5	.174E+03	615	212	211	5	.174E+03	671	268	267	5	.174E+03
560	157	156	5	.174E+03	616	213	212	5	.174E+03	672	269	268	5	.174E+03

Brnh	From	To	Tag	Conduct
673	270	269	5	.174E+03
674	271	270	5	.174E+03
675	272	271	5	.174E+03
676	273	272	5	.174E+03
677	274	273	5	.174E+03
678	275	274	5	.174E+03
679	276	275	5	.174E+03
680	277	276	5	.174E+03
681	278	277	5	.174E+03
682	279	278	5	.174E+03
683	280	279	5	.174E+03
684	281	280	5	.174E+03
685	282	281	5	.174E+03
686	283	282	5	.174E+03
687	284	283	5	.174E+03
688	285	284	5	.174E+03
689	286	285	5	.174E+03
690	287	286	5	.174E+03
691	288	287	5	.174E+03

TASS GENERAL INPUT MENU - SI Units

(1) Case Title:

TALSR(METRIC)---RUN 3. COMPLEX MODEL, MASS FLOW OF 68 kg/hr (150 lba/hr)

(2) Nodes	288
(3) Constant Temperatures	2
(4) Unique Exponents	0
(5) Temperature Dependent Conductances	0
(6) Temperature Dependent Heat Inputs	0
(7) Computational Accuracy	.0100
(8) Starting Temperature	25.0

Are these inputs correct (Y/N) ? Y

1111 DATA

Fin Length (L)	Fin Thickness	Fin Spacing (S)	Thermal Conductivity of Copper (k _{cu})	Thermal Conductivity of Clayon (k _{clayon})	Prandtl Number	Outer Pipe Diameter	Inner Pipe Diameter	Pipe Area
(in)	(in)	(in)	(W/m·K)	(W/m·K)		(in)	(in)	(in ²)
0.218	0.013	0.0232	4.81	0.0232	0.742	0.825	0.665	0.134

R-Value	Channel Width (W)	Effective Diameter	Heat Transfer Coefficient (h)	h-Term	Test	Distance Between Fins	Fins/Inch	K-Value
(in)	(in)	(in)	(Btu/hr·ft ² ·°F)	(in)	(W/m ² ·°C)	(in)		(W/m·K)
K1			N/A			0.302	N/A	1.7784
K2			0.610			0.302	N/A	0.2644
K3			N/A			0.334	N/A	1.6243
K4			N/A			0.367	N/A	1.4612
K5			0.02628			0.367	6.600	0.7254
K6	1.143	0.0119	0.02628	0.60200	0.01353	0.367	6.600	0.9440
K7	1.143	0.0119	0.02628	0.60200	0.01314	0.367	6.600	0.9264
K8	1.143	0.0119	0.02628	0.60200	0.01261	0.367	6.600	0.9241
K9	0.994	0.0081	0.04140	0.63500	0.02802	0.367	6.600	0.9807
K10	1.143	0.0119	0.02628	0.60200	0.01288	0.367	6.600	0.9607
K11	1.143	0.0119	0.02628	0.60200	0.01270	0.367	6.600	0.9582
K12	1.143	0.0119	0.02628	0.60200	0.01245	0.367	6.600	0.9620
K13	0.914	0.0045	0.03813	0.66000	0.00927	0.367	6.600	0.9078
K14	1.143	0.0119	0.02628	0.60200	0.01228	0.367	6.600	0.9019
K15	0.931	0.0069	0.02746	0.66000	0.01136	0.367	6.600	0.9089
K16	1.143	0.0119	0.02628	0.60200	0.01210	0.367	6.600	0.9089
K17	0.931	0.0069	0.02746	0.66000	0.01170	0.367	6.600	0.9089
K18	1.143	0.0119	0.02628	0.60200	0.01196	0.367	6.600	0.9089
K19	0.601	0.0069	0.05668	0.58000	0.01354	0.367	6.600	0.6609
K20	1.143	0.0119	0.02628	0.58400	0.01188	0.367	6.600	0.6854
K21	0.716	0.0060	0.03900	0.58400	0.01400	0.367	6.600	0.7000
K22	1.143	0.0119	0.02628	0.58400	0.01196	0.367	6.600	0.7000
K23	0.716	0.0060	0.03900	0.58400	0.01416	0.367	6.600	0.7000
K24	1.143	0.0119	0.02628	0.58400	0.01184	0.367	6.600	0.6850
K25	0.914	0.0119	0.02628	0.58400	0.01184	0.367	6.600	0.6850
K26	1.143	0.0119	0.02628	0.58400	0.01180	0.367	6.600	0.6850
K27	1.143	0.0119	0.02628	0.58400	0.01180	0.367	6.600	0.6850
K28	1.143	0.0119	0.02628	0.58400	0.01207	0.367	6.600	0.6850
K29	1.143	0.0119	N/A	0.66000	0.01216	0.418	N/A	1.2907
K30	1.143	0.0119	0.02628	0.66000	0.01216	0.367	6.600	0.9872
K31			N/A			0.465	N/A	1.1254
K32			0.610			0.465	N/A	0.4128
K33	1.104	0.0118	0.02628	0.94000	0.01199	0.465	N/A	0.9944
K34	0.994	0.0081	0.04140	0.94000	0.02802	0.465	N/A	1.0418
K35	0.906	0.0064	0.03928	0.70300	0.00498	0.465	7.540	0.6118
K36	2.037	0.040	0.03248	1.01000	0.01745	0.465	7.540	0.1325
K37	0.964	0.0064	0.02928	0.94000	0.00231	0.465	7.540	0.0218
K38	1.104	0.0100	0.00960	0.82200	0.01561	0.465	7.540	0.1171
K39	0.906	0.0031	0.02010	0.26000	0.00196	0.465	7.540	0.0642
K40	0.906	0.0031	0.02010	0.26000	0.00196	0.465	7.540	0.0642
K41	1.104	0.0118	0.02628	0.51400	0.01015	0.465	7.540	0.0609

K64	1.143	0.1019	0.03026	0.06160	0.01152	0.367	6.604	0.0512
K65	1.143	0.1019	0.03026	0.06050	0.01215	0.367	6.604	0.0509
K66	1.143	0.1019	0.03026	0.05940	0.01148	0.367	6.604	0.0506
K67	1.143	0.1019	0.03026	0.05830	0.01114	0.367	6.604	0.0503
K68	1.143	0.1019	0.03026	0.05720	0.01046	0.367	6.604	0.0500
K69	1.143	0.1019	0.03026	0.05610	0.01006	0.367	6.604	0.0497
K70	1.143	0.1019	0.03026	0.05500	0.01145	0.367	6.604	0.0494
K71	1.143	0.1019	0.03026	0.05400	0.01204	0.367	6.604	0.0491
K72	1.143	0.1019	0.03026	0.05300	0.01140	0.367	6.604	0.0488
K73	1.143	0.1019	0.03026	0.05200	0.01140	0.367	6.604	0.0485
K74	1.143	0.1019	0.03026	0.05100	0.01138	0.367	6.604	0.0482
K75	1.143	0.1019	0.03026	0.05000	0.01201	0.367	6.604	0.0479
K76	1.143	0.1019	0.03026	0.04900	0.01125	0.367	6.604	0.0476
K77	1.143	0.1019	0.03026	0.04800	0.01198	0.367	6.604	0.0473
K78	1.143	0.1019	0.03026	0.04700	0.01148	0.367	6.604	0.0470
K79	1.143	0.1019	0.03026	0.04600	0.01140	0.367	6.604	0.0467
K80	1.143	0.1019	0.03026	0.04500	0.01136	0.367	6.604	0.0464
K81	1.143	0.1019	0.03026	0.04400	0.01128	0.367	6.604	0.0461
K82	1.143	0.1019	0.03026	0.04300	0.01193	0.367	6.604	0.0458
K83	1.143	0.1019	0.03026	0.04200	0.01163	0.367	6.604	0.0455
K84	1.143	0.1019	0.03026	0.04100	0.01117	0.367	6.604	0.0452
K85	1.143	0.1019	0.03026	0.04000	0.01182	0.367	6.604	0.0449
K86	1.143	0.1019	0.03026	0.03900	0.01106	0.367	6.604	0.0446
K87	1.143	0.1019	0.03026	0.03800	0.01190	0.367	6.604	0.0443
K88	1.143	0.1019	0.03026	0.03700	0.01160	0.367	6.604	0.0440
K89	1.143	0.1019	0.03026	0.03600	0.01192	0.367	6.604	0.0437
K90	1.143	0.1019	0.03026	0.03500	0.01106	0.367	6.604	0.0434
K91	1.143	0.1019	0.03026	0.03400	0.01190	0.367	6.604	0.0431
K92	1.143	0.1019	0.03026	0.03300	0.01162	0.367	6.604	0.0428
K93	1.143	0.1019	0.03026	0.03200	0.01190	0.367	6.604	0.0425
K94	1.143	0.1019	0.03026	0.03100	0.01164	0.367	6.604	0.0422
K95	1.143	0.1019	0.03026	0.03000	0.01184	0.367	6.604	0.0419
K96	1.143	0.1019	0.03026	0.02900	0.01114	0.367	6.604	0.0416
K97	1.143	0.1019	0.03026	0.02800	0.01194	0.367	6.604	0.0413
K98	1.143	0.1019	0.03026	0.02700	0.01166	0.367	6.604	0.0410
K99	1.143	0.1019	0.03026	0.02600	0.01190	0.367	6.604	0.0407
K100	1.143	0.1019	0.03026	0.02500	0.01162	0.367	6.604	0.0404
K101	1.143	0.1019	0.03026	0.02400	0.01190	0.367	6.604	0.0401
K102	1.143	0.1019	0.03026	0.02300	0.01164	0.367	6.604	0.0398
K103	1.143	0.1019	0.03026	0.02200	0.01194	0.367	6.604	0.0395
K104	1.143	0.1019	0.03026	0.02100	0.01166	0.367	6.604	0.0392
K105	1.143	0.1019	0.03026	0.02000	0.01190	0.367	6.604	0.0389
K106	1.143	0.1019	0.03026	0.01900	0.01162	0.367	6.604	0.0386
K107	1.143	0.1019	0.03026	0.01800	0.01190	0.367	6.604	0.0383
K108	1.143	0.1019	0.03026	0.01700	0.01164	0.367	6.604	0.0380
K109	1.143	0.1019	0.03026	0.01600	0.01194	0.367	6.604	0.0377
K110	1.143	0.1019	0.03026	0.01500	0.01166	0.367	6.604	0.0374
K111	1.143	0.1019	0.03026	0.01400	0.01190	0.367	6.604	0.0371
K112	1.143	0.1019	0.03026	0.01300	0.01162	0.367	6.604	0.0368
K113	1.143	0.1019	0.03026	0.01200	0.01190	0.367	6.604	0.0365
K114	1.143	0.1019	0.03026	0.01100	0.01164	0.367	6.604	0.0362
K115	1.143	0.1019	0.03026	0.01000	0.01194	0.367	6.604	0.0359
K116	1.143	0.1019	0.03026	0.00900	0.01166	0.367	6.604	0.0356
K117	1.143	0.1019	0.03026	0.00800	0.01190	0.367	6.604	0.0353
K118	1.143	0.1019	0.03026	0.00700	0.01162	0.367	6.604	0.0350
K119	1.143	0.1019	0.03026	0.00600	0.01190	0.367	6.604	0.0347
K120	1.143	0.1019	0.03026	0.00500	0.01164	0.367	6.604	0.0344
K121	1.144	0.1021	0.03027	0.00400	0.01190	0.367	6.604	0.0341
K122	1.144	0.1021	0.03027	0.00300	0.01166	0.367	6.604	0.0338
K123	1.143	0.1019	0.03026	0.00200	0.01190	0.367	6.604	0.0335
K124	1.143	0.1019	0.03026	0.00100	0.01162	0.367	6.604	0.0332
K125	1.066	0.1030	0.03026	0.00000	0.01194	0.367	6.604	0.0329
K126	1.066	0.1030	0.03026	0.00000	0.01166	0.367	6.604	0.0326
K127	1.066	0.1030	0.03026	0.00000	0.01190	0.367	6.604	0.0323
K128	1.143	0.1019	0.03026	0.00000	0.01162	0.367	6.604	0.0320
K129	2.027	0.1040	0.03026	0.00000	0.01194	0.367	6.604	0.0317
K130	2.027	0.1040	0.03026	0.00000	0.01166	0.367	6.604	0.0314
K131	1.143	0.1019	0.03026	0.00000	0.01190	0.367	6.604	0.0311
K132	1.143	0.1019	0.03026	0.00000	0.01162	0.367	6.604	0.0308
K133	2.027	0.1040	0.03026	0.00000	0.01194	0.367	6.604	0.0305
K134	1.143	0.1019	0.03026	0.00000	0.01166	0.367	6.604	0.0302
K135	1.143	0.1019	0.03026	0.00000	0.01190	0.367	6.604	0.0299
K136	2.027	0.1040	0.03026	0.00000	0.01162	0.367	6.604	0.0296
K137	1.143	0.1019	0.03026	0.00000	0.01194	0.367	6.604	0.0293
K138	2.027	0.1040	0.03026	0.00000	0.01166	0.367	6.604	0.0290
K139	1.143	0.1019	0.03026	0.00000	0.01190	0.367	6.604	0.0287
K140	1.119	0.10182	0.03026	0.00000	0.01162	0.367	6.604	0.0284
K141	0.266	0.0804	0.03026	0.00000	0.01194	0.367	6.604	0.0281
K142	0.266	0.0804	0.03026	0.00000	0.01166	0.367	6.604	0.0278
K143	0.266	0.0804	0.03026	0.00000	0.01190	0.367	6.604	0.0275
K144	0.266	0.0804	0.03026	0.00000	0.01162	0.367	6.604	0.0272
K145	0.266	0.0804	0.03026	0.00000	0.01194	0.367	6.604	0.0269
K146	1.104	0.1018	0.03026	0.00000	0.01166	0.367	6.604	0.0266

K198	1.143	0.1019	0.00295	0.36700	0.01161	0.367	0.000	0.0005
K199	1.143	0.1019	0.00294	0.33100	0.01162	0.367	0.000	0.0005
K200	1.143	0.1019	0.00294	0.36600	0.01160	0.367	0.000	0.0014
K201	1.143	0.1019	0.00295	0.34600	0.01174	0.367	0.000	0.0005
K202	1.143	0.1019	0.00295	0.36700	0.01165	0.367	0.000	0.0005
K203	1.143	0.1019	0.00295	0.36700	0.01165	0.367	0.000	0.0014
K204	1.143	0.1019	0.00295	0.36500	0.01163	0.367	0.000	0.0030
K205	1.143	0.1019	0.00295	0.36600	0.01163	0.367	0.000	0.0036
K206	1.143	0.1019	0.00295	0.36100	0.01152	0.367	0.000	0.0008
K207	1.143	0.1019	0.00295	0.33600	0.01176	0.367	0.000	0.0008
K208	1.143	0.1019	0.00295	0.36600	0.01165	0.367	0.000	0.0005
K209	1.143	0.1019	0.00295	0.36200	0.01169	0.367	0.000	0.0027
K210	1.143	0.1019	0.00295	0.36100	0.01164	0.367	0.000	0.0050
K211	1.143	0.1019	0.00295	0.36600	0.01168	0.367	0.000	0.0029
K212	1.143	0.1019	0.00295	0.36600	0.01168	0.367	0.000	0.0054
K213	1.143	0.1019	0.00295	0.36600	0.01168	0.367	0.000	0.0030
K214	1.143	0.1019	0.00295	0.36600	0.01168	0.367	0.000	0.0030
K215	1.143	0.1019	0.00295	0.36600	0.01167	0.367	0.000	0.0025
K216	1.143	0.1019	0.00295	0.36500	0.01167	0.367	0.000	0.0053
K217	1.143	0.1019	0.00295	0.36500	0.01167	0.367	0.000	0.0053
K218	1.143	0.1019	0.00295	0.36600	0.01167	0.367	0.000	0.0049
K219	1.143	0.1019	0.00295	0.36600	0.01147	0.367	0.000	0.0005
K220	1.143	0.1019	0.00295	0.36600	0.01167	0.367	0.000	0.0005
K221	1.143	0.1019	0.00295	0.36600	0.01147	0.367	0.000	0.0025
K222	1.143	0.1019	0.00295	0.36700	0.01161	0.367	0.000	0.0025
K223	1.143	0.1019	0.00295	0.36100	0.01152	0.367	0.000	0.0028
K224	1.143	0.1019	0.00295	0.36600	0.01147	0.367	0.000	0.0025
K225	1.143	0.1019	0.00295	0.36600	0.01147	0.367	0.000	0.0005
K226	1.143	0.1019	0.00295	0.36600	0.01147	0.367	0.000	0.0005
K227	1.143	0.1019	0.00295	0.36600	0.01147	0.367	0.000	0.0016
K228	1.154	0.1021	0.00299	0.32000	0.01166	0.367	0.000	0.0008
K229	0.008	0.1001	0.00297	0.32000	0.01215	0.465	7.549	0.0061
K230	1.006	0.1020	0.00297	0.36600	0.00608	0.465	7.549	0.0050
K231	1.006	0.1020	0.00297	0.36600	0.01147	0.465	7.549	0.0050
K232	2.037	0.1040	0.00308	0.36600	0.01134	0.465	7.549	0.0020
K233	0.006	0.1004	0.00298	0.36600	0.01116	0.465	7.549	0.1353
K234	0.006	0.1004	0.00298	0.36600	0.00465	0.465	7.549	0.0417
K235	1.104	0.1019	0.00299	0.41500	0.00598	0.465	7.549	0.0163
K236	1.143	0.1019	0.00299	0.36100	0.01186	0.465	7.549	0.0035
K237	1.143	0.1019	0.00299	0.36600	0.01186	0.465	7.549	0.0035
K238	1.143	0.1019	0.00299	0.36500	0.01169	0.465	7.549	0.0055
K239	1.143	0.1019	0.00299	0.36600	0.01118	0.367	0.000	0.0045
K240	1.143	0.1019	0.00299	0.36600	0.01165	0.367	0.000	0.0037
K241	1.143	0.1019	0.00299	0.36600	0.01155	0.367	0.000	0.0031
K242	1.143	0.1019	0.00299	0.36600	0.01148	0.367	0.000	0.0031
K243	1.143	0.1019	0.00299	0.36600	0.01148	0.367	0.000	0.0050
K244	1.143	0.1019	0.00299	0.36200	0.01163	0.367	0.000	0.0030
K245	1.143	0.1019	0.00299	0.36100	0.01161	0.367	0.000	0.0035
K246	1.143	0.1019	0.00299	0.36600	0.01174	0.367	0.000	0.0044
K247	1.143	0.1019	0.00299	0.36600	0.01162	0.367	0.000	0.0005
K248	1.143	0.1019	0.00299	0.36600	0.01162	0.367	0.000	0.0005
K249	1.143	0.1019	0.00299	0.36600	0.01162	0.367	0.000	0.0005
K250	1.143	0.1019	0.00299	0.36100	0.01232	0.367	0.000	0.0084

K249	1.143	0.1019	0.02826	0.02900	0.01253	0.357	0.800	0.0098
K251	1.143	0.1019	0.02826	0.02900	0.01253	0.347	0.800	0.0098
K252	N/A	N/A	N/A	N/A	N/A	N/A	N/A	29.8161

TASS Branch Connection Summary in W/degC or Watts if Tag = 10

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
1	1	2	1	.178E+01	57	17	301	1	.860E-01	113	32	176	4	.373E+00
2	1	145	4	.306E+00	58	17	301	1	.910E-01	114	32	301	1	.860E-01
3	2	3	1	.178E+01	59	18	19	1	.146E+01	115	32	301	1	.830E-01
4	2	146	4	.306E+00	60	18	162	4	.373E+00	116	33	34	1	.146E+01
5	3	4	1	.178E+01	61	18	301	1	.860E-01	117	33	177	4	.373E+00
6	3	147	4	.306E+00	62	18	301	1	.820E-01	118	33	301	1	.860E-01
7	4	5	1	.160E+01	63	19	20	1	.146E+01	119	33	301	1	.830E-01
8	4	148	4	.306E+00	64	19	163	4	.373E+00	120	34	35	1	.146E+01
9	5	6	1	.146E+01	65	19	301	1	.870E-01	121	34	178	4	.373E+00
10	5	149	4	.373E+00	66	19	301	1	.680E-01	122	34	301	1	.860E-01
11	5	301	1	.954E+01	67	20	21	1	.129E+01	123	34	301	1	.830E-01
12	6	7	1	.146E+01	68	20	164	4	.373E+00	124	35	36	1	.146E+01
13	6	150	4	.373E+00	69	20	301	1	.870E-01	125	35	179	4	.373E+00
14	6	301	1	.940E-01	70	20	301	1	.490E-01	126	35	301	1	.860E-01
15	7	8	1	.146E+01	71	21	22	1	.115E+01	127	35	301	1	.820E-01
16	7	151	4	.373E+00	72	21	165	4	.473E+00	128	36	37	1	.146E+01
17	7	301	1	.920E-01	73	21	301	1	.940E-01	129	36	180	4	.373E+00
18	7	301	1	.240E-01	74	22	23	1	.115E+01	130	36	301	1	.860E-01
19	8	9	1	.146E+01	75	22	166	4	.473E+00	131	36	301	1	.810E-01
20	8	152	4	.373E+00	76	22	301	1	.770E-01	132	37	38	1	.146E+01
21	8	301	1	.910E-01	77	23	24	1	.115E+01	133	37	181	4	.373E+00
22	8	301	1	.490E-01	78	23	167	4	.473E+00	134	37	301	1	.850E-01
23	9	10	1	.146E+01	79	23	301	1	.420E-01	135	37	301	1	.800E-01
24	9	153	4	.373E+00	80	24	25	1	.115E+01	136	38	39	1	.146E+01
25	9	301	1	.890E-01	81	24	168	4	.473E+00	137	38	182	4	.373E+00
26	9	301	1	.680E-01	82	24	301	1	.136E+00	138	38	301	1	.850E-01
27	10	11	1	.146E+01	83	24	301	1	.220E-01	139	38	301	1	.780E-01
28	10	154	4	.373E+00	84	25	26	1	.115E+01	140	39	40	1	.146E+01
29	10	301	1	.880E-01	85	25	169	4	.473E+00	141	39	183	4	.373E+00
30	10	301	1	.820E-01	86	25	301	1	.117E+00	142	39	301	1	.850E-01
31	11	12	1	.146E+01	87	25	301	1	.640E-01	143	39	301	1	.770E-01
32	11	155	4	.373E+00	88	26	27	1	.129E+01	144	40	41	1	.146E+01
33	11	301	1	.870E-01	89	26	170	4	.473E+00	145	40	184	4	.373E+00
34	11	301	1	.910E-01	90	26	301	1	.101E+00	146	40	301	1	.850E-01
35	12	13	1	.146E+01	91	26	301	1	.850E-01	147	40	301	1	.750E-01
36	12	156	4	.373E+00	92	27	28	1	.146E+01	148	41	42	1	.146E+01
37	12	301	1	.860E-01	93	27	171	4	.373E+00	149	41	185	4	.373E+00
38	12	301	1	.970E-01	94	27	301	1	.890E-01	150	41	301	1	.850E-01
39	13	14	1	.146E+01	95	27	301	1	.810E-01	151	41	301	1	.730E-01
40	13	157	4	.373E+00	96	28	29	1	.146E+01	152	42	43	1	.129E+01
41	13	301	1	.850E-01	97	28	172	4	.373E+00	153	42	186	4	.373E+00
42	13	301	1	.100E+00	98	28	301	1	.880E-01	154	42	301	1	.850E-01
43	14	15	1	.146E+01	99	28	301	1	.810E-01	155	42	301	1	.710E-01
44	14	158	4	.373E+00	100	29	30	1	.146E+01	156	43	44	1	.115E+01
45	14	301	1	.850E-01	101	29	173	4	.373E+00	157	43	187	4	.473E+00
46	14	301	1	.101E+00	102	29	301	1	.870E-01	158	43	301	1	.910E-01
47	15	16	1	.146E+01	103	29	301	1	.820E-01	159	43	301	1	.124E+00
48	15	159	4	.373E+00	104	30	31	1	.146E+01	160	44	45	1	.115E+01
49	15	301	1	.850E-01	105	30	174	4	.373E+00	161	44	188	4	.473E+00
50	15	301	1	.100E+00	106	30	301	1	.870E-01	162	44	301	1	.730E-01
51	16	17	1	.146E+01	107	30	301	1	.830E-01	163	44	301	1	.920E-01
52	16	160	4	.373E+00	108	31	32	1	.146E+01	164	45	46	1	.115E+01
53	16	301	1	.850E-01	109	31	175	4	.373E+00	165	45	189	4	.473E+00
54	16	301	1	.970E-01	110	31	301	1	.870E-01	166	45	301	1	.390E-01
55	17	18	1	.146E+01	111	31	301	1	.830E-01	167	46	47	1	.115E+01
56	17	161	4	.373E+00	112	32	33	1	.146E+01	168	46	190	4	.473E+00

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
169	46	301	1	.150E+00	225	60	301	1	.860E-01	281	74	301	1	.138E+00
170	46	301	1	.250E-01	226	60	301	1	.810E-01	282	74	301	1	.700E-01
171	47	48	1	.115E+01	227	61	62	1	.146E+01	283	75	76	1	.120E+01
172	47	191	4	.473E+00	228	61	205	4	.373E+00	284	75	219	4	.473E+00
173	47	301	1	.127E+00	229	61	301	1	.860E-01	285	75	301	1	.157E+00
174	47	301	1	.690E-01	230	61	301	1	.810E-01	286	75	301	1	.900E-01
175	48	49	1	.129E+01	231	62	63	1	.146E+01	287	76	77	1	.125E+01
176	48	192	4	.473E+00	232	62	206	4	.373E+00	288	76	220	4	.348E+00
177	48	301	1	.100E+00	233	62	301	1	.860E-01	289	76	301	1	.171E+00
178	48	301	1	.890E-01	234	62	301	1	.810E-01	290	76	301	1	.980E-01
179	49	50	1	.146E+01	235	63	64	1	.146E+01	291	77	78	1	.210E+01
180	49	193	4	.373E+00	236	63	207	4	.373E+00	292	77	221	4	.348E+00
181	49	301	1	.880E-01	237	63	301	1	.860E-01	293	77	301	1	.172E+00
182	49	301	1	.830E-01	238	63	301	1	.800E-01	294	77	301	1	.970E-01
183	50	51	1	.146E+01	239	64	65	1	.108E+01	295	78	79	1	.128E+01
184	50	194	4	.373E+00	240	64	208	4	.373E+00	296	78	222	4	.288E+00
185	50	301	1	.870E-01	241	64	301	1	.860E-01	297	78	301	1	.124E+00
186	50	301	1	.830E-01	242	64	301	1	.790E-01	298	78	301	1	.910E-01
187	51	52	1	.146E+01	243	65	66	1	.992E+00	299	79	80	1	.992E+00
188	51	195	4	.373E+00	244	65	209	4	.526E+00	300	79	223	4	.433E+00
189	51	301	1	.870E-01	245	65	301	1	.940E-01	301	79	301	1	.108E+00
190	51	301	1	.830E-01	246	65	301	1	.870E-01	302	79	301	1	.870E-01
191	52	53	1	.146E+01	247	66	67	1	.172E+01	303	80	81	1	.108E+01
192	52	196	4	.373E+00	248	66	210	4	.433E+00	304	80	224	4	.526E+00
193	52	301	1	.870E-01	249	66	301	1	.930E-01	305	80	301	1	.930E-01
194	52	301	1	.830E-01	250	66	301	1	.103E+00	306	80	301	1	.910E-01
195	53	54	1	.146E+01	251	67	68	1	.210E+01	307	81	82	1	.146E+01
196	53	197	4	.373E+00	252	67	211	4	.288E+00	308	81	225	4	.373E+00
197	53	301	1	.870E-01	253	67	301	1	.930E-01	309	81	301	1	.840E-01
198	53	301	1	.830E-01	254	67	301	1	.125E+00	310	81	301	1	.830E-01
199	54	55	1	.146E+01	255	68	69	1	.125E+01	311	82	83	1	.146E+01
200	54	198	4	.373E+00	256	68	212	4	.348E+00	312	82	226	4	.373E+00
201	54	301	1	.870E-01	257	68	301	1	.990E-01	313	82	301	1	.850E-01
202	54	301	1	.830E-01	258	68	301	1	.172E+00	314	82	301	1	.820E-01
203	55	56	1	.146E+01	259	69	70	1	.120E+01	315	83	84	1	.146E+01
204	55	199	4	.373E+00	260	69	213	4	.348E+00	316	83	227	4	.373E+00
205	55	301	1	.870E-01	261	69	301	1	.990E-01	317	83	301	1	.850E-01
206	55	301	1	.830E-01	262	69	301	1	.171E+00	318	83	301	1	.820E-01
207	56	57	1	.146E+01	263	70	71	1	.115E+01	319	84	85	1	.146E+01
208	56	200	4	.373E+00	264	70	214	4	.473E+00	320	84	228	4	.373E+00
209	56	301	1	.870E-01	265	70	301	1	.900E-01	321	84	301	1	.860E-01
210	56	301	1	.820E-01	266	70	301	1	.157E+00	322	84	301	1	.820E-01
211	57	58	1	.146E+01	267	71	72	1	.115E+01	323	85	86	1	.146E+01
212	57	201	4	.373E+00	268	71	215	4	.473E+00	324	85	229	4	.373E+00
213	57	301	1	.860E-01	269	71	301	1	.710E-01	325	85	301	1	.860E-01
214	57	301	1	.820E-01	270	71	301	1	.138E+00	326	85	301	1	.820E-01
215	58	59	1	.146E+01	271	72	73	1	.115E+01	327	86	87	1	.146E+01
216	58	202	4	.373E+00	272	72	216	4	.473E+00	328	86	300	4	.373E+00
217	58	301	1	.860E-01	273	72	301	1	.310E-01	329	86	301	1	.860E-01
218	58	301	1	.820E-01	274	72	301	1	.670E-01	330	86	301	1	.820E-01
219	59	60	1	.146E+01	275	73	74	1	.115E+01	331	87	88	1	.146E+01
220	59	203	4	.373E+00	276	73	217	4	.473E+00	332	87	231	4	.373E+00
221	59	301	1	.860E-01	277	73	301	1	.670E-01	333	87	301	1	.860E-01
222	59	301	1	.820E-01	278	73	301	1	.310E-01	334	87	301	1	.820E-01
223	60	61	1	.146E+01	279	74	75	1	.115E+01	335	88	89	1	.146E+01
224	60	204	4	.373E+00	280	74	218	4	.473E+00	336	88	232	4	.373E+00

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
137	88	301	1	.850E-01	393	102	301	1	.900E-01	449	116	301	1	.830E-01
138	88	301	1	.820E-01	394	103	104	1	.146E+01	450	117	118	1	.146E+01
139	89	90	1	.146E+01	395	103	247	4	.373E+00	451	117	261	4	.373E+00
140	89	233	4	.373E+00	396	103	301	1	.760E-01	452	117	301	1	.830E-01
141	89	301	1	.850E-01	397	103	301	1	.840E-01	453	117	301	1	.830E-01
142	89	301	1	.810E-01	398	104	105	1	.146E+01	454	118	119	1	.129E+01
143	90	91	1	.146E+01	399	104	248	4	.373E+00	455	118	262	4	.373E+00
144	90	234	4	.373E+00	400	104	301	1	.780E-01	456	118	301	1	.820E-01
145	90	301	1	.850E-01	401	104	301	1	.840E-01	457	118	301	1	.840E-01
146	90	301	1	.810E-01	402	105	106	1	.146E+01	458	119	120	1	.115E+01
147	91	92	1	.146E+01	403	105	249	4	.373E+00	459	119	263	4	.473E+00
148	91	235	4	.373E+00	404	105	301	1	.790E-01	460	119	301	1	.860E-01
149	91	301	1	.850E-01	405	105	301	1	.830E-01	461	119	301	1	.960E-01
150	91	301	1	.810E-01	406	106	107	1	.146E+01	462	120	121	1	.115E+01
151	92	93	1	.146E+01	407	106	250	4	.373E+00	463	120	264	4	.473E+00
152	92	236	4	.373E+00	408	106	301	1	.810E-01	464	120	301	1	.650E-01
153	92	301	1	.850E-01	409	106	301	1	.830E-01	465	120	301	1	.113E+00
154	92	301	1	.810E-01	410	107	108	1	.146E+01	466	121	122	1	.115E+01
155	93	94	1	.146E+01	411	107	251	4	.373E+00	467	121	265	4	.473E+00
156	93	237	4	.373E+00	412	107	301	1	.820E-01	468	121	301	1	.220E-01
157	93	301	1	.850E-01	413	107	301	1	.830E-01	469	121	301	1	.133E+00
158	93	301	1	.810E-01	414	108	109	1	.146E+01	470	122	123	1	.115E+01
159	94	95	1	.146E+01	415	108	252	4	.373E+00	471	122	266	4	.473E+00
160	94	238	4	.373E+00	416	108	301	1	.840E-01	472	122	301	1	.420E-01
161	94	301	1	.850E-01	417	108	301	1	.830E-01	473	123	124	1	.115E+01
162	94	301	1	.810E-01	418	109	110	1	.146E+01	474	123	267	4	.473E+00
163	95	96	1	.146E+01	419	109	253	4	.373E+00	475	123	301	1	.760E-01
164	95	239	4	.373E+00	420	109	301	1	.850E-01	476	124	125	1	.129E+01
165	95	301	1	.850E-01	421	109	301	1	.830E-01	477	124	268	4	.473E+00
166	95	301	1	.810E-01	422	110	111	1	.146E+01	478	124	301	1	.940E-01
167	96	97	1	.129E+01	423	110	254	4	.373E+00	479	125	126	1	.146E+01
168	96	240	4	.373E+00	424	110	301	1	.850E-01	480	125	269	4	.373E+00
169	96	301	1	.840E-01	425	110	301	1	.830E-01	481	125	301	1	.490E-01
170	96	301	1	.800E-01	426	111	112	1	.146E+01	482	125	301	1	.860E-01
171	97	98	1	.115E+01	427	111	255	4	.373E+00	483	126	127	1	.146E+01
172	97	241	4	.473E+00	428	111	301	1	.850E-01	484	126	270	4	.373E+00
173	97	301	1	.900E-01	429	111	301	1	.830E-01	485	126	301	1	.680E-01
174	97	301	1	.930E-01	430	112	113	1	.146E+01	486	126	301	1	.860E-01
175	98	99	1	.115E+01	431	112	256	4	.373E+00	487	127	128	1	.146E+01
176	98	242	4	.473E+00	432	112	301	1	.850E-01	488	127	271	4	.373E+00
177	98	301	1	.690E-01	433	112	301	1	.830E-01	489	127	301	1	.820E-01
178	98	301	1	.123E+00	434	113	114	1	.146E+01	490	127	301	1	.850E-01
179	99	100	1	.115E+01	435	113	257	4	.373E+00	491	128	129	1	.146E+01
180	99	243	4	.473E+00	436	113	301	1	.850E-01	492	128	272	4	.373E+00
181	99	301	1	.260E-01	437	113	301	1	.830E-01	493	128	301	1	.910E-01
182	99	301	1	.149E+00	438	114	115	1	.146E+01	494	128	301	1	.840E-01
183	100	101	1	.115E+01	439	114	258	4	.373E+00	495	129	130	1	.146E+01
184	100	244	4	.473E+00	440	114	301	1	.850E-01	496	129	273	4	.373E+00
185	100	301	1	.380E-01	441	114	301	1	.830E-01	497	129	301	1	.970E-01
186	101	102	1	.115E+01	442	115	116	1	.146E+01	498	129	301	1	.830E-01
187	101	245	4	.473E+00	443	115	259	4	.373E+00	499	130	131	1	.146E+01
188	101	301	1	.920E-01	444	115	301	1	.840E-01	500	130	274	4	.373E+00
189	101	301	1	.720E-01	445	115	301	1	.830E-01	501	130	301	1	.100E+00
190	102	103	1	.129E+01	446	116	117	1	.146E+01	502	130	301	1	.830E-01
191	102	246	4	.473E+00	447	116	260	4	.373E+00	503	131	132	1	.146E+01
192	102	301	1	.124E+00	448	116	301	1	.840E-01	504	131	275	4	.373E+00

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
505	131	301	1	.101E+00	561	158	157	5	.790E+02	617	214	213	5	.790E+02
506	131	301	1	.830E+01	562	159	158	5	.790E+02	618	215	214	5	.790E+02
507	132	133	1	.146E+01	563	160	159	5	.790E+02	619	216	215	5	.790E+02
508	132	276	4	.373E+00	564	161	160	5	.790E+02	620	217	216	5	.790E+02
509	132	301	1	.100E+00	565	162	161	5	.790E+02	621	218	217	5	.790E+02
510	132	301	1	.830E+01	566	163	162	5	.790E+02	622	219	218	5	.790E+02
511	133	134	1	.146E+01	567	164	163	5	.790E+02	623	220	219	5	.790E+02
512	133	277	4	.373E+00	568	165	164	5	.790E+02	624	221	220	5	.790E+02
513	133	301	1	.970E+01	569	166	165	5	.790E+02	625	222	221	5	.790E+02
514	133	301	1	.830E+01	570	167	166	5	.790E+02	626	223	222	5	.790E+02
515	134	135	1	.146E+01	571	168	167	5	.790E+02	627	224	223	5	.790E+02
516	134	278	4	.373E+00	572	169	168	5	.790E+02	628	225	224	5	.790E+02
517	134	301	1	.910E+01	573	170	169	5	.790E+02	629	226	225	5	.790E+02
518	134	301	1	.840E+01	574	171	170	5	.790E+02	630	227	226	5	.790E+02
519	135	136	1	.146E+01	575	172	171	5	.790E+02	631	228	227	5	.790E+02
520	135	279	4	.373E+00	576	173	172	5	.790E+02	632	229	228	5	.790E+02
521	135	301	1	.820E+01	577	174	173	5	.790E+02	633	230	229	5	.790E+02
522	135	301	1	.840E+01	578	175	174	5	.790E+02	634	231	230	5	.790E+02
523	136	137	1	.146E+01	579	176	175	5	.790E+02	635	232	231	5	.790E+02
524	136	280	4	.373E+00	580	177	176	5	.790E+02	636	233	232	5	.790E+02
525	136	301	1	.680E+01	581	178	177	5	.790E+02	637	234	233	5	.790E+02
526	136	301	1	.860E+01	582	179	178	5	.790E+02	638	235	234	5	.790E+02
527	137	138	1	.146E+01	583	180	179	5	.790E+02	639	236	235	5	.790E+02
528	137	281	4	.373E+00	584	181	180	5	.790E+02	640	237	236	5	.790E+02
529	137	301	1	.490E+01	585	182	181	5	.790E+02	641	238	237	5	.790E+02
530	137	301	1	.870E+01	586	183	182	5	.790E+02	642	239	238	5	.790E+02
531	138	139	1	.146E+01	587	184	183	5	.790E+02	643	240	239	5	.790E+02
532	138	282	4	.373E+00	588	185	184	5	.790E+02	644	241	240	5	.790E+02
533	138	301	1	.240E+01	589	186	185	5	.790E+02	645	242	241	5	.790E+02
534	138	301	1	.880E+01	590	187	186	5	.790E+02	646	243	242	5	.790E+02
535	139	140	1	.146E+01	591	188	187	5	.790E+02	647	244	243	5	.790E+02
536	139	283	4	.373E+00	592	189	188	5	.790E+02	648	245	244	5	.790E+02
537	139	301	1	.900E+01	593	190	189	5	.790E+02	649	246	245	5	.790E+02
538	140	141	1	.160E+01	594	191	190	5	.790E+02	650	247	246	5	.790E+02
539	140	284	4	.373E+00	595	192	191	5	.790E+02	651	248	247	5	.790E+02
540	140	301	1	.910E+01	596	193	192	5	.790E+02	652	249	248	5	.790E+02
541	141	142	1	.178E+01	597	194	193	5	.790E+02	653	250	249	5	.790E+02
542	141	285	4	.306E+00	598	195	194	5	.790E+02	654	251	250	5	.790E+02
543	142	143	1	.178E+01	599	196	195	5	.790E+02	655	252	251	5	.790E+02
544	142	286	4	.306E+00	600	197	196	5	.790E+02	656	253	252	5	.790E+02
545	143	144	1	.178E+01	601	198	197	5	.790E+02	657	254	253	5	.790E+02
546	143	287	4	.306E+00	602	199	198	5	.790E+02	658	255	254	5	.790E+02
547	144	288	4	.306E+00	603	200	199	5	.790E+02	659	256	255	5	.790E+02
548	145	102	5	.790E+02	604	201	200	5	.790E+02	660	257	256	5	.790E+02
549	146	145	5	.790E+02	605	202	201	5	.790E+02	661	258	257	5	.790E+02
550	147	146	5	.790E+02	606	203	202	5	.790E+02	662	259	258	5	.790E+02
551	148	147	5	.790E+02	607	204	203	5	.790E+02	663	260	259	5	.790E+02
552	149	148	5	.790E+02	608	205	204	5	.790E+02	664	261	260	5	.790E+02
553	150	149	5	.790E+02	609	206	205	5	.790E+02	665	262	261	5	.790E+02
554	151	150	5	.790E+02	610	207	206	5	.790E+02	666	263	262	5	.790E+02
555	152	151	5	.790E+02	611	208	207	5	.790E+02	667	264	263	5	.790E+02
556	153	152	5	.790E+02	612	209	208	5	.790E+02	668	265	264	5	.790E+02
557	154	153	5	.790E+02	613	210	209	5	.790E+02	669	266	265	5	.790E+02
558	155	154	5	.790E+02	614	211	210	5	.790E+02	670	267	266	5	.790E+02
559	156	155	5	.790E+02	615	212	211	5	.790E+02	671	268	267	5	.790E+02
560	157	156	5	.790E+02	616	213	212	5	.790E+02	672	269	268	5	.790E+02

Brnh	From	To	Tag	Conduct
673	270	269	5	.790E+02
674	271	270	5	.790E+02
675	272	271	5	.790E+02
676	273	272	5	.790E+02
677	274	273	5	.790E+02
678	275	274	5	.790E+02
679	276	275	5	.790E+02
680	277	276	5	.790E+02
681	278	277	5	.790E+02
682	279	278	5	.790E+02
683	280	279	5	.790E+02
684	281	280	5	.790E+02
685	282	281	5	.790E+02
686	283	282	5	.790E+02
687	284	283	5	.790E+02
688	285	284	5	.790E+02
689	286	285	5	.790E+02
690	287	286	5	.790E+02
691	288	287	5	.790E+02

TASS GENERAL INPUT MENU - SI Units

(1) Case Title:

TALSR(METRIC)---RUN 4. COMPLEX MODEL, MASS FLOW OF 272.2 kg/hr (600 lbm/hr)

(2) Nodes 288

(3) Constant Temperatures 2

(4) Unique Exponents 0

(5) Temperature Dependent Conductances 0

(6) Temperature Dependent Heat Inputs 0

(7) Computational Accuracy .0100

(8) Starting Temperature 25.0

Are these inputs correct (Y/N) ? Y

REPORT DATA

Fin Length (ft)	Fin Thickness (in)	Fin spacing (ft)	Thermal Conductivity of Copper (W/m ² °K)	Finlet Number	Finlet Diameter (in)	Finlet Area (in ²)
0.318	0.015	0.0253	4.01	1000.00	0.027	0.033

K-Value	Crossed Width (ft)	Effective Diameter (in)	Heat Transfer Coefficient (ft)	Finlet Number	Finlet Diameter (in)	Finlet Area (in ²)
K1	1.143	0.0119	0.0253	1000.00	0.027	0.033
K2	1.143	0.0119	0.0253	1000.00	0.027	0.033
K3	1.143	0.0119	0.0253	1000.00	0.027	0.033
K4	1.143	0.0119	0.0253	1000.00	0.027	0.033
K5	1.143	0.0119	0.0253	1000.00	0.027	0.033
K6	1.143	0.0119	0.0253	1000.00	0.027	0.033
K7	1.143	0.0119	0.0253	1000.00	0.027	0.033
K8	1.143	0.0119	0.0253	1000.00	0.027	0.033
K9	1.143	0.0119	0.0253	1000.00	0.027	0.033
K10	1.143	0.0119	0.0253	1000.00	0.027	0.033
K11	1.143	0.0119	0.0253	1000.00	0.027	0.033
K12	1.143	0.0119	0.0253	1000.00	0.027	0.033
K13	1.143	0.0119	0.0253	1000.00	0.027	0.033
K14	1.143	0.0119	0.0253	1000.00	0.027	0.033
K15	1.143	0.0119	0.0253	1000.00	0.027	0.033
K16	1.143	0.0119	0.0253	1000.00	0.027	0.033
K17	1.143	0.0119	0.0253	1000.00	0.027	0.033
K18	1.143	0.0119	0.0253	1000.00	0.027	0.033
K19	1.143	0.0119	0.0253	1000.00	0.027	0.033
K20	1.143	0.0119	0.0253	1000.00	0.027	0.033
K21	1.143	0.0119	0.0253	1000.00	0.027	0.033
K22	1.143	0.0119	0.0253	1000.00	0.027	0.033
K23	1.143	0.0119	0.0253	1000.00	0.027	0.033
K24	1.143	0.0119	0.0253	1000.00	0.027	0.033
K25	1.143	0.0119	0.0253	1000.00	0.027	0.033
K26	1.143	0.0119	0.0253	1000.00	0.027	0.033
K27	1.143	0.0119	0.0253	1000.00	0.027	0.033
K28	1.143	0.0119	0.0253	1000.00	0.027	0.033
K29	1.143	0.0119	0.0253	1000.00	0.027	0.033
K30	1.143	0.0119	0.0253	1000.00	0.027	0.033
K31	1.143	0.0119	0.0253	1000.00	0.027	0.033
K32	1.143	0.0119	0.0253	1000.00	0.027	0.033
K33	1.143	0.0119	0.0253	1000.00	0.027	0.033
K34	1.143	0.0119	0.0253	1000.00	0.027	0.033
K35	1.143	0.0119	0.0253	1000.00	0.027	0.033
K36	1.143	0.0119	0.0253	1000.00	0.027	0.033
K37	1.143	0.0119	0.0253	1000.00	0.027	0.033
K38	1.143	0.0119	0.0253	1000.00	0.027	0.033
K39	1.143	0.0119	0.0253	1000.00	0.027	0.033
K40	1.143	0.0119	0.0253	1000.00	0.027	0.033
K41	1.143	0.0119	0.0253	1000.00	0.027	0.033

0.0546
9.0411
210.1050

6.8902
6.8902
N/A

0.367
0.367
N/A

0.01253
0.01272
N/A

0.62000
0.62000
N/A

0.05026
0.05045
N/A

0.10106
0.10106
N/A

1.143
1.143
N/A

PC150
PC151
PC152

1.1

TASS Branch Connection Summary in W/degC or Watts if Tag = 10

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
1	1	2	1	.178E+01	57	17	301	1	.860E-01	113	32	176	4	.114E+01
2	1	145	4	.933E+00	58	17	301	1	.910E-01	114	32	301	1	.860E-01
3	2	3	1	.178E+01	59	18	19	1	.146E+01	115	32	301	1	.830E-01
4	2	146	4	.933E+00	60	18	162	4	.114E+01	116	33	14	1	.146E+01
5	3	4	1	.178E+01	61	18	301	1	.860E-01	117	33	177	4	.114E+01
6	3	147	4	.933E+00	62	18	301	1	.820E-01	118	33	301	1	.860E-01
7	4	5	1	.160E+01	63	19	20	1	.146E+01	119	33	301	1	.830E-01
8	4	148	4	.933E+00	64	19	163	4	.114E+01	120	34	35	1	.146E+01
9	5	6	1	.146E+01	65	19	301	1	.870E-01	121	34	178	4	.114E+01
10	5	149	4	.114E+01	66	19	301	1	.680E-01	122	34	301	1	.860E-01
11	5	301	1	.954E-01	67	20	21	1	.129E+01	123	34	301	1	.830E-01
12	6	7	1	.146E+01	68	20	164	4	.114E+01	124	35	36	1	.146E+01
13	6	150	4	.114E+01	69	20	301	1	.870E-01	125	35	179	4	.114E+01
14	6	301	1	.940E-01	70	20	301	1	.490E-01	126	35	301	1	.860E-01
15	7	8	1	.146E+01	71	21	22	1	.115E+01	127	35	301	1	.820E-01
16	7	151	4	.114E+01	72	21	165	4	.144E+01	128	36	37	1	.146E+01
17	7	301	1	.920E-01	73	21	301	1	.940E-01	129	36	180	4	.114E+01
18	7	301	1	.240E-01	74	22	32	1	.115E+01	130	36	301	1	.860E-01
19	8	9	1	.146E+01	75	22	166	4	.144E+01	131	36	301	1	.810E-01
20	8	152	4	.114E+01	76	22	301	1	.770E-01	132	37	38	1	.146E+01
21	8	301	1	.910E-01	77	23	24	1	.115E+01	133	37	181	4	.114E+01
22	8	301	1	.490E-01	78	23	167	4	.144E+01	134	37	301	1	.850E-01
23	9	10	1	.146E+01	79	23	301	1	.420E-01	135	37	301	1	.800E-01
24	9	153	4	.114E+01	80	24	25	1	.115E+01	136	38	39	1	.146E+01
25	9	301	1	.890E-01	81	24	168	4	.144E+01	137	38	182	4	.114E+01
26	9	301	1	.680E-01	82	24	301	1	.136E+00	138	38	301	1	.850E-01
27	10	11	1	.146E+01	83	24	301	1	.220E-01	139	38	301	1	.780E-01
28	10	154	4	.114E+01	84	25	26	1	.115E+01	140	39	40	1	.146E+01
29	10	301	1	.880E-01	85	25	169	4	.144E+01	141	39	183	4	.114E+01
30	10	301	1	.820E-01	86	25	301	1	.117E+00	142	39	301	1	.850E-01
31	11	12	1	.146E+01	87	25	301	1	.640E-01	143	39	301	1	.770E-01
32	11	155	4	.114E+01	88	26	27	1	.129E+01	144	40	41	1	.146E+01
33	11	301	1	.870E-01	89	26	170	4	.144E+01	145	40	184	4	.114E+01
34	11	301	1	.910E-01	90	26	301	1	.101E+00	146	40	301	1	.850E-01
35	12	13	1	.146E+01	91	26	301	1	.850E-01	147	40	301	1	.750E-01
36	12	156	4	.114E+01	92	27	28	1	.146E+01	148	41	42	1	.146E+01
37	12	301	1	.860E-01	93	27	171	4	.114E+01	149	41	185	4	.114E+01
38	12	301	1	.970E-01	94	27	301	1	.890E-01	150	41	301	1	.850E-01
39	13	14	1	.146E+01	95	27	301	1	.810E-01	151	41	301	1	.730E-01
40	13	157	4	.114E+01	96	28	29	1	.146E+01	152	42	43	1	.129E+01
41	13	301	1	.850E-01	97	28	172	4	.114E+01	153	42	186	4	.114E+01
42	13	301	1	.100E+00	98	28	301	1	.880E-01	154	42	301	1	.850E-01
43	14	15	1	.146E+01	99	28	301	1	.810E-01	155	42	301	1	.710E-01
44	14	158	4	.114E+01	100	29	30	1	.146E+01	156	43	44	1	.115E+01
45	14	301	1	.850E-01	101	29	173	4	.114E+01	157	43	187	4	.144E+01
46	14	301	1	.101E+00	102	29	301	1	.870E-01	158	43	301	1	.910E-01
47	15	16	1	.146E+01	103	29	301	1	.820E-01	159	43	301	1	.124E+00
48	15	159	4	.114E+01	104	30	31	1	.146E+01	160	44	45	1	.115E+01
49	15	301	1	.850E-01	105	30	174	4	.114E+01	161	44	188	4	.144E+01
50	15	301	1	.100E+00	106	30	301	1	.870E-01	162	44	301	1	.730E-01
51	16	17	1	.146E+01	107	30	301	1	.830E-01	163	44	301	1	.920E-01
52	16	160	4	.114E+01	108	31	32	1	.146E+01	164	45	46	1	.115E+01
53	16	301	1	.850E-01	109	31	175	4	.114E+01	165	45	189	4	.144E+01
54	16	301	1	.970E-01	110	31	301	1	.870E-01	166	45	301	1	.390E-01

55	17	18	1	.146E+01	111	31	301	1	.830E-01	167	46	47	1	.115E+01
56	17	161	4	.114E+01	112	32	33	1	.146E+01	168	46	190	4	.144E+01

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
169	46	301	1	.150E+00	225	60	301	1	.860E-01	281	74	301	1	.138E+00
170	46	301	1	.250E-01	226	60	301	1	.810E-01	282	74	301	1	.700E-01
171	47	48	1	.115E+01	227	61	62	1	.146E+01	283	75	76	1	.120E+01
172	47	191	4	.144E+01	228	61	205	4	.114E+01	284	75	219	4	.144E+01
173	47	301	1	.127E+00	229	61	301	1	.860E-01	285	75	301	1	.157E+00
174	47	301	1	.690E-01	230	61	301	1	.810E-01	286	75	301	1	.900E-01
175	48	49	1	.129E+01	231	62	63	1	.146E+01	287	76	77	1	.125E+01
176	48	192	4	.144E+01	232	62	206	4	.114E+01	288	76	220	4	.106E+01
177	48	301	1	.100E+00	233	62	301	1	.860E-01	289	76	301	1	.171E+00
178	48	301	1	.890E-01	234	62	301	1	.810E-01	290	76	301	1	.980E-01
179	49	50	1	.146E+01	235	63	64	1	.146E+01	291	77	78	1	.210E+01
180	49	193	4	.114E+01	236	63	207	4	.114E+01	292	77	221	4	.106E+01
181	49	301	1	.880E-01	237	63	301	1	.860E-01	293	77	301	1	.172E+00
182	49	301	1	.830E-01	238	63	301	1	.800E-01	294	77	301	1	.970E-01
183	50	51	1	.146E+01	239	64	65	1	.108E+01	295	78	79	1	.172E+01
184	50	194	4	.114E+01	240	64	208	4	.114E+01	296	78	222	4	.878E+00
185	50	301	1	.870E-01	241	64	301	1	.860E-01	297	78	301	1	.124E+00
186	50	301	1	.830E-01	242	64	301	1	.790E-01	298	78	301	1	.910E-01
187	51	52	1	.146E+01	243	65	66	1	.992E+00	299	79	80	1	.992E+00
188	51	195	4	.114E+01	244	65	209	4	.160E+01	300	79	223	4	.132E+01
189	51	301	1	.870E-01	245	65	301	1	.940E-01	301	79	301	1	.108E+00
190	51	301	1	.830E-01	246	65	301	1	.870E-01	302	79	301	1	.870E-01
191	52	53	1	.146E+01	247	66	67	1	.172E+01	303	80	81	1	.108E+01
192	52	196	4	.114E+01	248	66	210	4	.132E+01	304	80	224	4	.160E+01
193	52	301	1	.870E-01	249	66	301	1	.930E-01	305	80	301	1	.930E-01
194	52	301	1	.830E-01	250	66	301	1	.103E+00	306	80	301	1	.910E-01
195	53	54	1	.146E+01	251	67	68	1	.210E+01	307	81	82	1	.146E+01
196	53	197	4	.114E+01	252	67	211	4	.878E+00	308	81	225	4	.114E+01
197	53	301	1	.870E-01	253	67	301	1	.930E-01	309	81	301	1	.840E-01
198	53	301	1	.830E-01	254	67	301	1	.125E+00	310	81	301	1	.830E-01
199	54	55	1	.146E+01	255	68	69	1	.125E+01	311	82	83	1	.146E+01
200	54	198	4	.114E+01	256	68	212	4	.106E+01	312	82	226	4	.114E+01
201	54	301	1	.870E-01	257	68	301	1	.990E-01	313	82	301	1	.850E-01
202	54	301	1	.830E-01	258	68	301	1	.172E+00	314	82	301	1	.820E-01
203	55	56	1	.146E+01	259	69	70	1	.120E+01	315	83	84	1	.146E+01
204	55	199	4	.114E+01	260	69	213	4	.106E+01	316	83	227	4	.114E+01
205	55	301	1	.870E-01	261	69	301	1	.990E-01	317	83	301	1	.850E-01
206	55	301	1	.830E-01	262	69	301	1	.171E+00	318	83	301	1	.820E-01
207	56	57	1	.146E+01	263	70	71	1	.115E+01	319	84	85	1	.146E+01
208	56	200	4	.114E+01	264	70	214	4	.144E+01	320	84	228	4	.114E+01
209	56	301	1	.870E-01	265	70	301	1	.900E-01	321	84	301	1	.860E-01
210	56	301	1	.820E-01	266	70	301	1	.157E+00	322	84	301	1	.820E-01
211	57	58	1	.146E+01	267	71	72	1	.115E+01	323	85	86	1	.146E+01
212	57	201	4	.114E+01	268	71	215	4	.144E+01	324	85	229	4	.114E+01
213	57	301	1	.860E-01	269	71	301	1	.710E-01	325	85	301	1	.860E-01
214	57	301	1	.820E-01	270	71	301	1	.138E+00	326	85	301	1	.820E-01
215	58	59	1	.146E+01	271	72	73	1	.115E+01	327	86	87	1	.146E+01
216	58	202	4	.114E+01	272	72	216	4	.144E+01	328	86	230	4	.114E+01
217	58	301	1	.860E-01	273	72	301	1	.330E-01	329	86	301	1	.860E-01
218	58	301	1	.820E-01	274	72	301	1	.670E-01	330	86	301	1	.820E-01
219	59	60	1	.146E+01	275	73	74	1	.115E+01	331	87	88	1	.146E+01
220	59	203	4	.114E+01	276	73	217	4	.144E+01	332	87	231	4	.114E+01
221	59	301	1	.860E-01	277	73	301	1	.670E-01	333	87	301	1	.860E-01
222	59	301	1	.820E-01	278	73	301	1	.310E-01	334	87	301	1	.820E-01
223	60	61	1	.146E+01	279	74	75	1	.115E+01	335	88	89	1	.146E+01
224	60	204	4	.114E+01	280	74	218	4	.144E+01	336	88	232	4	.114E+01

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
337	88	301	1	.850E-01	393	102	301	1	.900E-01	449	116	301	1	.830E-01
338	88	301	1	.820E-01	394	103	104	1	.146E+01	450	117	118	1	.146E+01
339	89	90	1	.146E+01	395	103	247	4	.114E+01	451	117	261	4	.114E+01
340	89	233	4	.114E+01	396	103	301	1	.760E-01	452	117	301	1	.830E-01
341	89	301	1	.850E-01	397	103	301	1	.840E-01	453	117	301	1	.830E-01
342	89	301	1	.810E-01	398	104	105	1	.146E+01	454	118	119	1	.129E+01
343	90	91	1	.146E+01	399	104	248	4	.114E+01	455	118	262	4	.114E+01
344	90	234	4	.114E+01	400	104	301	1	.780E-01	456	118	301	1	.820E-01
345	90	301	1	.850E-01	401	104	301	1	.840E-01	457	118	301	1	.840E-01
346	90	301	1	.810E-01	402	105	106	1	.146E+01	458	119	120	1	.115E+01
347	91	92	1	.146E+01	403	105	249	4	.114E+01	459	119	263	4	.144E+01
348	91	235	4	.114E+01	404	105	301	1	.790E-01	460	119	301	1	.860E-01
349	91	301	1	.850E-01	405	105	301	1	.830E-01	461	119	301	1	.960E-01
350	91	301	1	.810E-01	406	106	107	1	.146E+01	462	120	121	1	.115E+01
351	92	93	1	.146E+01	407	106	250	4	.114E+01	463	120	264	4	.144E+01
352	92	236	4	.114E+01	408	106	301	1	.810E-01	464	120	301	1	.650E-01
353	92	301	1	.850E-01	409	106	301	1	.830E-01	465	120	301	1	.113E+00
354	92	301	1	.810E-01	410	107	108	1	.146E+01	466	121	122	1	.115E+01
355	93	94	1	.146E+01	411	107	251	4	.114E+01	467	121	265	4	.144E+01
356	93	237	4	.114E+01	412	107	301	1	.820E-01	468	121	301	1	.120E+01
357	93	301	1	.850E-01	413	107	301	1	.830E-01	469	121	301	1	.133E+00
358	93	301	1	.810E-01	414	108	109	1	.146E+01	470	122	123	1	.115E+01
359	94	95	1	.146E+01	415	108	252	4	.114E+01	471	122	266	4	.144E+01
360	94	238	4	.114E+01	416	108	301	1	.840E-01	472	122	301	1	.420E-01
361	94	301	1	.850E-01	417	108	301	1	.830E-01	473	123	124	1	.115E+01
362	94	301	1	.810E-01	418	109	110	1	.146E+01	474	123	267	4	.144E+01
363	95	96	1	.146E+01	419	109	253	4	.114E+01	475	123	301	1	.760E-01
364	95	239	4	.114E+01	420	109	301	1	.850E-01	476	124	125	1	.129E+01
365	95	301	1	.850E-01	421	109	301	1	.830E-01	477	124	268	4	.144E+01
366	95	301	1	.810E-01	422	110	111	1	.146E+01	478	124	301	1	.940E-01
367	96	97	1	.129E+01	423	110	254	4	.114E+01	479	125	126	1	.146E+01
368	96	240	4	.114E+01	424	110	301	1	.850E-01	480	125	269	4	.114E+01
369	96	301	1	.840E-01	425	110	301	1	.830E-01	481	125	301	1	.490E-01
370	96	301	1	.800E-01	426	111	112	1	.146E+01	482	125	301	1	.860E-01
371	97	98	1	.115E+01	427	111	255	4	.114E+01	483	126	127	1	.146E+01
372	97	241	4	.114E+01	428	111	301	1	.850E-01	484	126	270	4	.114E+01
373	97	301	1	.900E-01	429	111	301	1	.830E-01	485	126	301	1	.680E-01
374	97	301	1	.930E-01	430	112	113	1	.146E+01	486	126	301	1	.860E-01
375	98	99	1	.115E+01	431	112	256	4	.114E+01	487	127	128	1	.146E+01
376	98	242	4	.114E+01	432	112	301	1	.850E-01	488	127	271	4	.114E+01
377	98	301	1	.690E-01	433	112	301	1	.830E-01	489	127	301	1	.820E-01
378	98	301	1	.123E+00	434	113	114	1	.146E+01	490	127	301	1	.850E-01
379	99	100	1	.115E+01	435	113	257	4	.114E+01	491	128	129	1	.146E+01
380	99	243	4	.114E+01	436	113	301	1	.850E-01	492	128	272	4	.114E+01
381	99	301	1	.1260E-01	437	113	301	1	.830E-01	493	128	301	1	.910E-01
382	99	301	1	.149E+00	438	114	115	1	.146E+01	494	128	301	1	.840E-01
383	100	101	1	.115E+01	439	114	258	4	.114E+01	495	129	130	1	.146E+01
384	100	244	4	.114E+01	440	114	301	1	.850E-01	496	129	273	4	.114E+01
385	100	301	1	.380E-01	441	114	301	1	.830E-01	497	129	301	1	.970E-01
386	101	102	1	.115E+01	442	115	116	1	.146E+01	498	129	301	1	.830E-01
387	101	245	4	.114E+01	443	115	259	4	.114E+01	499	130	131	1	.146E+01
388	101	301	1	.920E-01	444	115	301	1	.840E-01	500	130	274	4	.114E+01
389	101	301	1	.720E-01	445	115	301	1	.830E-01	501	130	301	1	.100E+00
390	102	103	1	.129E+01	446	116	117	1	.146E+01	502	130	301	1	.830E-01
391	102	246	4	.114E+01	447	116	260	4	.114E+01	503	131	132	1	.146E+01
392	102	301	1	.124E+00	448	116	301	1	.840E-01	504	131	275	4	.114E+01

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
505	131	301	1	.101E+00	561	158	157	5	.316E+03	617	214	213	5	.316E+03
506	131	301	1	.830E-01	562	159	158	5	.316E+03	618	215	214	5	.316E+03
507	132	133	1	.146E+01	563	160	159	5	.316E+03	619	216	215	5	.316E+03
508	132	276	4	.114E+01	564	161	160	5	.316E+03	620	217	216	5	.316E+03
509	132	301	1	.100E+00	565	162	161	5	.316E+03	621	218	217	5	.316E+03
510	132	301	1	.830E-01	566	163	162	5	.316E+03	622	219	218	5	.316E+03
511	133	134	1	.146E+01	567	164	163	5	.316E+03	623	220	219	5	.316E+03
512	133	277	4	.114E+01	568	165	164	5	.316E+03	624	221	220	5	.316E+03
513	133	301	1	.970E-01	569	166	165	5	.316E+03	625	222	221	5	.316E+03
514	133	301	1	.830E-01	570	167	166	5	.316E+03	626	223	222	5	.316E+03
515	134	135	1	.146E+01	571	168	167	5	.316E+03	627	224	223	5	.316E+03
516	134	278	4	.114E+01	572	169	168	5	.316E+03	628	225	224	5	.316E+03
517	134	301	1	.910E-01	573	170	169	5	.316E+03	629	226	225	5	.316E+03
518	134	301	1	.840E-01	574	171	170	5	.316E+03	630	227	226	5	.316E+03
519	135	136	1	.146E+01	575	172	171	5	.316E+03	631	228	227	5	.316E+03
520	135	279	4	.114E+01	576	173	172	5	.316E+03	632	229	228	5	.316E+03
521	135	301	1	.820E-01	577	174	173	5	.316E+03	633	230	229	5	.316E+03
522	135	301	1	.840E-01	578	175	174	5	.316E+03	634	231	230	5	.316E+03
523	136	137	1	.146E+01	579	176	175	5	.316E+03	635	232	231	5	.316E+03
524	136	280	4	.114E+01	580	177	176	5	.316E+03	636	233	232	5	.316E+03
525	136	301	1	.680E-01	581	178	177	5	.316E+03	637	234	233	5	.316E+03
526	136	301	1	.860E-01	582	179	178	5	.316E+03	638	235	234	5	.316E+03
527	137	138	1	.146E+01	583	180	179	5	.316E+03	639	236	235	5	.316E+03
528	137	281	4	.114E+01	584	181	180	5	.316E+03	640	237	236	5	.316E+03
529	137	301	1	.490E-01	585	182	181	5	.316E+03	641	238	237	5	.316E+03
530	137	301	1	.870E-01	586	183	182	5	.316E+03	642	239	238	5	.316E+03
531	138	139	1	.146E+01	587	184	183	5	.316E+03	643	240	239	5	.316E+03
532	138	282	4	.114E+01	588	185	184	5	.316E+03	644	241	240	5	.316E+03
533	138	301	1	.240E-01	589	186	185	5	.316E+03	645	242	241	5	.316E+03
534	138	301	1	.880E-01	590	187	186	5	.316E+03	646	243	242	5	.316E+03
535	139	140	1	.146E+01	591	188	187	5	.316E+03	647	244	243	5	.316E+03
536	139	283	4	.114E+01	592	189	188	5	.316E+03	648	245	244	5	.316E+03
537	139	301	1	.900E-01	593	190	189	5	.316E+03	649	246	245	5	.316E+03
538	140	141	1	.160E+01	594	191	190	5	.316E+03	650	247	246	5	.316E+03
539	140	284	4	.114E+01	595	192	191	5	.316E+03	651	248	247	5	.316E+03
540	140	301	1	.910E-01	596	193	192	5	.316E+03	652	249	248	5	.316E+03
541	141	142	1	.178E+01	597	194	193	5	.316E+03	653	250	249	5	.316E+03
542	141	285	4	.933E+00	598	195	194	5	.316E+03	654	251	250	5	.316E+03
543	142	143	1	.178E+01	599	196	195	5	.316E+03	655	252	251	5	.316E+03
544	142	286	4	.933E+00	600	197	196	5	.316E+03	656	253	252	5	.316E+03
545	143	144	1	.178E+01	601	198	197	5	.316E+03	657	254	253	5	.316E+03
546	143	287	4	.933E+00	602	199	198	5	.316E+03	658	255	254	5	.316E+03
547	144	288	4	.933E+00	603	200	199	5	.316E+03	659	256	255	5	.316E+03
548	145	302	5	.316E+03	604	201	200	5	.316E+03	660	257	256	5	.316E+03
549	146	145	5	.316E+03	605	202	201	5	.316E+03	661	258	257	5	.316E+03
550	147	146	5	.316E+03	606	203	202	5	.316E+03	662	259	258	5	.316E+03
551	148	147	5	.316E+03	607	204	203	5	.316E+03	663	260	259	5	.316E+03
552	149	148	5	.316E+03	608	205	204	5	.316E+03	664	261	260	5	.316E+03
553	150	149	5	.316E+03	609	206	205	5	.316E+03	665	262	261	5	.316E+03
554	151	150	5	.316E+03	610	207	206	5	.316E+03	666	263	262	5	.316E+03
555	152	151	5	.316E+03	611	208	207	5	.316E+03	667	264	263	5	.316E+03
556	153	152	5	.316E+03	612	209	208	5	.316E+03	668	265	264	5	.316E+03
557	154	153	5	.316E+03	613	210	209	5	.316E+03	669	266	265	5	.316E+03
558	155	154	5	.316E+03	614	211	210	5	.316E+03	670	267	266	5	.316E+03
559	156	155	5	.316E+03	615	212	211	5	.316E+03	671	268	267	5	.316E+03
560	157	156	5	.316E+03	616	213	212	5	.316E+03	672	269	268	5	.316E+03

Brnh	From	To	Tag	Conduct
673	270	269	5	.316E+03
674	271	270	5	.316E+03
675	272	271	5	.316E+03
676	273	272	5	.316E+03
677	274	273	5	.316E+03
678	275	274	5	.316E+03
679	276	275	5	.316E+03
680	277	276	5	.316E+03
681	278	277	5	.316E+03
682	279	278	5	.316E+03
683	280	279	5	.316E+03
684	281	280	5	.316E+03
685	282	281	5	.316E+03
686	283	282	5	.316E+03
687	284	283	5	.316E+03
688	285	284	5	.316E+03
689	286	285	5	.316E+03
690	287	286	5	.316E+03
691	288	287	5	.316E+03

TASS GENERAL INPUT MENU - SI Units

(1) Case Title:
TALSR(METRIC)--RUN 5. COMPLEX MODEL, MASS FLOW OF 362.9 kg/hr (800 lbm/hr)

(2) Nodes	288
(3) Constant Temperatures	2
(4) Unique Exponents	0
(5) Temperature Dependent Conductances	0
(6) Temperature Dependent Heat Inputs	0
(7) Computational Accuracy	.0100
(8) Starting Temperature	25.0

Are these inputs correct (Y/N) ? Y

K504	1.143	0.0109	0.03450	0.56100	0.01152	0.367	0.850	0.0628
K505	1.143	0.0109	0.03450	0.56600	0.01120	0.367	0.850	0.0646
K506	1.143	0.0109	0.03450	0.55500	0.01146	0.367	0.850	0.0628
K507	1.143	0.0109	0.03450	0.56600	0.01207	0.367	0.850	0.0667
K508	1.143	0.0109	0.03450	0.55500	0.01147	0.367	0.850	0.0625
K509	1.143	0.0109	0.03450	0.55500	0.01146	0.367	0.850	0.0625
K510	1.143	0.0109	0.03450	0.55500	0.01146	0.367	0.850	0.0625
K511	1.143	0.0109	0.03450	0.55500	0.01146	0.367	0.850	0.0625
K512	1.143	0.0109	0.03450	0.56600	0.01254	0.367	0.850	0.0644
K513	1.143	0.0109	0.03450	0.55400	0.01146	0.367	0.850	0.0621
K514	1.143	0.0109	0.03450	0.56600	0.01202	0.367	0.850	0.0663
K515	1.143	0.0109	0.03450	0.55500	0.01139	0.367	0.850	0.0626
K516	1.143	0.0109	0.03450	0.55500	0.01139	0.367	0.850	0.0626
K517	1.143	0.0109	0.03450	0.55500	0.01135	0.367	0.850	0.0617
K518	1.143	0.0109	0.03450	0.56600	0.01198	0.367	0.850	0.0659
K519	1.143	0.0109	0.03450	0.54400	0.01120	0.367	0.850	0.0614
K520	1.143	0.0109	0.03450	0.56600	0.01196	0.367	0.850	0.0659
K521	1.143	0.0109	0.03450	0.55500	0.01139	0.367	0.850	0.0626
K522	1.143	0.0109	0.03450	0.56600	0.01198	0.367	0.850	0.0657
K523	1.143	0.0109	0.03450	0.54400	0.01117	0.367	0.850	0.0605
K524	1.143	0.0109	0.03450	0.56600	0.01182	0.367	0.850	0.0656
K525	1.143	0.0109	0.03450	0.53500	0.01166	0.367	0.850	0.0597
K526	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K527	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K528	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K529	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K530	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K531	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K532	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K533	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K534	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K535	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K536	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K537	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K538	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K539	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K540	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K541	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K542	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K543	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K544	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618
K545	1.143	0.0109	0.03450	0.55500	0.01190	0.367	0.850	0.0618

142

143

0250	01113	01019	01000	01123	01017	01000	01000
0251	0113	01018	01000	01122	01017	01000	01000
0252	0101	0101	0101	0101	0101	0101	0101

TASS Branch Connection Summary in W/degC or Watts if Tag = 10

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
1	1	2	1	.178E+01	57	17	301	1	.860E-01	113	32	176	4	.701E+00
2	1	145	4	.576E+00	58	17	301	1	.910E-01	114	32	301	1	.860E-01
3	2	3	1	.178E+01	59	18	19	1	.146E+01	115	32	301	1	.830E-01
4	2	146	4	.576E+00	60	18	162	4	.701E+00	116	33	34	1	.146E+01
5	3	4	1	.178E+01	61	18	301	1	.860E-01	117	33	177	4	.701E+00
6	3	147	4	.576E+00	62	18	301	1	.820E-01	118	33	301	1	.860E-01
7	4	5	1	.160E+01	63	19	20	1	.146E+01	119	33	301	1	.830E-01
8	4	148	4	.576E+00	64	19	163	4	.701E+00	120	34	35	1	.146E+01
9	5	6	1	.146E+01	65	19	301	1	.870E-01	121	34	178	4	.701E+00
10	5	149	4	.701E+00	66	19	301	1	.680E-01	122	34	301	1	.860E-01
11	5	301	1	.954E-01	67	20	21	1	.129E+01	123	34	301	1	.830E-01
12	6	7	1	.146E+01	68	20	164	4	.701E+00	124	35	36	1	.146E+01
13	6	150	4	.701E+00	69	20	301	1	.870E-01	125	35	179	4	.701E+00
14	6	301	1	.940E-01	70	20	301	1	.490E-01	126	35	301	1	.860E-01
15	7	8	1	.146E+01	71	21	22	1	.115E+01	127	35	301	1	.820E-01
16	7	151	4	.701E+00	72	21	165	4	.889E+00	128	36	37	1	.146E+01
17	7	301	1	.920E-01	73	21	301	1	.940E-01	129	36	180	4	.701E+00
18	7	301	1	.240E-01	74	22	23	1	.115E+01	130	36	301	1	.860E-01
19	8	9	1	.146E+01	75	22	166	4	.889E+00	131	36	301	1	.810E-01
20	8	152	4	.701E+00	76	22	301	1	.770E-01	132	37	38	1	.146E+01
21	8	301	1	.910E-01	77	23	24	1	.115E+01	133	37	181	4	.701E+00
22	8	301	1	.490E-01	78	23	167	4	.889E+00	134	37	301	1	.850E-01
23	9	10	1	.146E+01	79	23	301	1	.420E-01	135	37	301	1	.800E-01
24	9	153	4	.701E+00	80	24	25	1	.115E+01	136	38	39	1	.146E+01
25	9	301	1	.890E-01	81	24	168	4	.889E+00	137	38	182	4	.701E+00
26	9	301	1	.680E-01	82	24	301	1	.136E+00	138	38	301	1	.850E-01
27	10	11	1	.146E+01	83	24	301	1	.220E-01	139	38	301	1	.780E-01
28	10	154	4	.701E+00	84	25	26	1	.115E+01	140	39	40	1	.146E+01
29	10	301	1	.880E-01	85	25	169	4	.889E+00	141	39	183	4	.701E+00
30	10	301	1	.820E-01	86	25	301	1	.117E+00	142	39	301	1	.850E-01
31	11	12	1	.146E+01	87	25	301	1	.640E-01	143	39	301	1	.770E-01
32	11	155	4	.701E+00	88	26	27	1	.129E+01	144	40	41	1	.146E+01
33	11	301	1	.870E-01	89	26	170	4	.889E+00	145	40	184	4	.701E+00
34	11	301	1	.910E-01	90	26	301	1	.101E+00	146	40	301	1	.850E-01
35	12	13	1	.146E+01	91	26	301	1	.850E-01	147	40	301	1	.750E-01
36	12	156	4	.701E+00	92	27	28	1	.146E+01	148	41	42	1	.146E+01
37	12	301	1	.860E-01	93	27	171	4	.701E+00	149	41	185	4	.701E+00
38	12	301	1	.970E-01	94	27	301	1	.890E-01	150	41	301	1	.850E-01
39	13	14	1	.146E+01	95	27	301	1	.810E-01	151	41	301	1	.730E-01
40	13	157	4	.701E+00	96	28	29	1	.146E+01	152	42	43	1	.129E+01
41	13	301	1	.850E-01	97	28	172	4	.701E+00	153	42	186	4	.701E+00
42	13	301	1	.100E+00	98	28	301	1	.880E-01	154	42	301	1	.850E-01
43	14	15	1	.146E+01	99	28	301	1	.810E-01	155	42	301	1	.710E-01
44	14	158	4	.701E+00	100	29	30	1	.146E+01	156	43	44	1	.115E+01
45	14	301	1	.850E-01	101	29	173	4	.701E+00	157	43	187	4	.889E+00
46	14	301	1	.101E+00	102	29	301	1	.870E-01	158	43	301	1	.910E-01
47	15	16	1	.146E+01	103	29	301	1	.820E-01	159	43	301	1	.124E+00
48	15	159	4	.701E+00	104	30	31	1	.146E+01	160	44	45	1	.115E+01
49	15	301	1	.850E-01	105	30	174	4	.701E+00	161	44	188	4	.889E+00
50	15	301	1	.100E+00	106	30	301	1	.870E-01	162	44	301	1	.730E-01
51	16	17	1	.146E+01	107	30	301	1	.830E-01	163	44	301	1	.920E-01
52	16	160	4	.701E+00	108	31	32	1	.146E+01	164	45	46	1	.115E+01
53	16	301	1	.850E-01	109	31	175	4	.701E+00	165	45	189	4	.889E+00
54	16	301	1	.970E-01	110	31	301	1	.870E-01	166	45	301	1	.390E-01
55	17	18	1	.146E+01	111	31	301	1	.830E-01	167	46	47	1	.115E+01
56	17	161	4	.701E+00	112	32	33	1	.146E+01	168	46	190	4	.889E+00

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
169	46	301	1	.150E+00	225	60	301	1	.860E-01	281	74	301	1	.118E+00
170	46	301	1	.250E-01	226	60	301	1	.810E-01	282	74	301	1	.700E-01
171	47	48	1	.115E+01	227	61	62	1	.146E+01	283	75	76	1	.120E+01
172	47	191	4	.889E+00	228	61	205	4	.701E+00	284	75	219	4	.889E+00
173	47	301	1	.127E+00	229	61	301	1	.860E-01	285	75	301	1	.157E+00
174	47	301	1	.690E-01	230	61	301	1	.810E-01	286	75	301	1	.900E-01
175	48	49	1	.129E+01	231	62	63	1	.146E+01	287	76	77	1	.125E+01
176	48	192	4	.889E+00	232	62	206	4	.701E+00	288	76	220	4	.655E+00
177	48	301	1	.100E+00	233	62	301	1	.860E-01	289	76	301	1	.171E+00
178	48	301	1	.890E-01	234	62	301	1	.810E-01	290	76	301	1	.980E-01
179	49	50	1	.146E+01	235	63	64	1	.146E+01	291	77	78	1	.210E+01
180	49	193	4	.701E+00	236	63	207	4	.701E+00	292	77	301	1	.655E+00
181	49	301	1	.880E-01	237	63	301	1	.860E-01	293	77	301	1	.172E+00
182	49	301	1	.830E-01	238	63	301	1	.800E-01	294	77	301	1	.970E-01
183	50	51	1	.146E+01	239	64	65	1	.108E+01	295	78	79	1	.172E+01
184	50	194	4	.701E+00	240	64	208	4	.701E+00	296	78	222	4	.542E+00
185	50	301	1	.870E-01	241	64	301	1	.860E-01	297	78	301	1	.124E+00
186	50	301	1	.830E-01	242	64	301	1	.790E-01	298	78	301	1	.910E-01
187	51	52	1	.146E+01	243	65	66	1	.992E+00	299	79	80	1	.992E+00
188	51	195	4	.701E+00	244	65	209	4	.990E+00	300	79	223	4	.815E+00
189	51	301	1	.870E-01	245	65	301	1	.940E-01	301	79	301	1	.108E+00
190	51	301	1	.830E-01	246	65	301	1	.870E-01	302	79	301	1	.870E-01
191	52	53	1	.146E+01	247	66	67	1	.172E+01	303	80	81	1	.108E+01
192	52	196	4	.701E+00	248	66	210	4	.815E+00	304	80	224	4	.990E+00
193	52	301	1	.870E-01	249	66	301	1	.930E-01	305	80	301	1	.930E-01
194	52	301	1	.830E-01	250	66	301	1	.103E+00	306	80	301	1	.910E-01
195	53	54	1	.146E+01	251	67	68	1	.210E+01	307	81	82	1	.146E+01
196	53	197	4	.701E+00	252	67	211	4	.542E+00	308	81	225	4	.701E+00
197	53	301	1	.870E-01	253	67	301	1	.930E-01	309	81	301	1	.840E-01
198	53	301	1	.830E-01	254	67	301	1	.125E+00	310	81	301	1	.830E-01
199	54	55	1	.146E+01	255	68	69	1	.125E+01	311	82	83	1	.146E+01
200	54	198	4	.701E+00	256	68	212	4	.655E+00	312	82	226	4	.701E+00
201	54	301	1	.870E-01	257	68	301	1	.990E-01	313	82	301	1	.850E-01
202	54	301	1	.830E-01	258	68	301	1	.172E+00	314	82	301	1	.820E-01
203	55	56	1	.146E+01	259	69	70	1	.120E+01	315	83	84	1	.146E+01
204	55	199	4	.701E+00	260	69	213	4	.655E+00	316	83	227	4	.701E+00
205	55	301	1	.870E-01	261	69	301	1	.990E-01	317	83	301	1	.850E-01
206	55	301	1	.830E-01	262	69	301	1	.171E+00	318	83	301	1	.820E-01
207	56	57	1	.146E+01	263	70	71	1	.115E+01	319	84	85	1	.146E+01
208	56	200	4	.701E+00	264	70	214	4	.889E+00	320	84	228	4	.701E+00
209	56	301	1	.870E-01	265	70	301	1	.900E-01	321	84	301	1	.860E-01
210	56	301	1	.820E-01	266	70	301	1	.157E+00	322	84	301	1	.820E-01
211	57	58	1	.146E+01	267	71	72	1	.115E+01	323	85	86	1	.146E+01
212	57	201	4	.701E+00	268	71	215	4	.889E+00	324	85	229	4	.701E+00
213	57	301	1	.860E-01	269	71	301	1	.710E-01	325	85	301	1	.860E-01
214	57	301	1	.820E-01	270	71	301	1	.138E+00	326	85	301	1	.820E-01
215	58	59	1	.146E+01	271	72	73	1	.115E+01	327	86	87	1	.146E+01
216	58	202	4	.701E+00	272	72	216	4	.889E+00	328	86	230	4	.701E+00
217	58	301	1	.860E-01	273	72	301	1	.330E-01	329	86	301	1	.860E-01
218	58	301	1	.820E-01	274	72	301	1	.670E-01	330	86	301	1	.820E-01
219	59	60	1	.146E+01	275	73	74	1	.115E+01	331	87	88	1	.146E+01
220	59	203	4	.701E+00	276	73	217	4	.889E+00	332	87	231	4	.701E+00
221	59	301	1	.860E-01	277	73	301	1	.670E-01	333	87	301	1	.860E-01
222	59	301	1	.820E-01	278	73	301	1	.310E-01	334	87	301	1	.820E-01
223	60	61	1	.146E+01	279	74	75	1	.115E+01	335	88	89	1	.146E+01
224	60	204	4	.701E+00	280	74	218	4	.889E+00	336	88	232	4	.701E+00

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
337	88	301	1	.850E-01	393	102	301	1	.900E-01	449	116	301	1	.830E-01
338	88	301	1	.820E-01	394	103	104	1	.146E+01	450	117	118	1	.146E+01
339	89	90	1	.146E+01	395	103	247	4	.701E+00	451	117	261	4	.701E+00
340	89	233	4	.701E+00	396	103	301	1	.760E-01	452	117	301	1	.830E-01
341	89	301	1	.850E-01	397	103	301	1	.840E-01	453	117	301	1	.830E-01
342	89	301	1	.810E-01	398	104	105	1	.146E+01	454	118	119	1	.129E+01
343	90	91	1	.146E+01	399	104	248	4	.701E+00	455	118	262	4	.701E+00
344	90	234	4	.701E+00	400	104	301	1	.780E-01	456	118	301	1	.820E-01
345	90	301	1	.850E-01	401	104	301	1	.840E-01	457	118	301	1	.840E-01
346	90	301	1	.810E-01	402	105	106	1	.146E+01	458	119	120	1	.115E+01
347	91	92	1	.146E+01	403	105	249	4	.701E+00	459	119	263	4	.889E+00
348	91	235	4	.701E+00	404	105	301	1	.790E-01	460	119	301	1	.860E-01
349	91	301	1	.850E-01	405	105	301	1	.830E-01	461	119	301	1	.960E-01
350	91	301	1	.810E-01	406	106	107	1	.146E+01	462	120	121	1	.115E+01
351	92	93	1	.146E+01	407	106	250	4	.701E+00	463	120	264	4	.889E+00
352	92	236	4	.701E+00	408	106	301	1	.810E-01	464	120	301	1	.650E-01
353	92	301	1	.850E-01	409	106	301	1	.830E-01	465	120	301	1	.113E+00
354	92	301	1	.810E-01	410	107	108	1	.146E+01	466	121	122	1	.115E+01
355	93	94	1	.146E+01	411	107	251	4	.701E+00	467	121	265	4	.889E+00
356	93	237	4	.701E+00	412	107	301	1	.820E-01	468	121	301	1	.220E-01
357	93	301	1	.850E-01	413	107	301	1	.830E-01	469	121	301	1	.133E+00
358	93	301	1	.810E-01	414	108	109	1	.146E+01	470	122	123	1	.115E+01
359	94	95	1	.146E+01	415	108	252	4	.701E+00	471	122	266	4	.889E+00
360	94	238	4	.701E+00	416	108	301	1	.840E-01	472	122	301	1	.420E-01
361	94	301	1	.850E-01	417	108	301	1	.830E-01	473	123	124	1	.115E+01
362	94	301	1	.810E-01	418	109	110	1	.146E+01	474	123	267	4	.889E+00
363	95	96	1	.146E+01	419	109	253	4	.701E+00	475	123	301	1	.760E-01
364	95	239	4	.701E+00	420	109	301	1	.850E-01	476	124	125	1	.129E+01
365	95	301	1	.850E-01	421	109	301	1	.830E-01	477	124	268	4	.889E+00
366	95	301	1	.810E-01	422	110	111	1	.146E+01	478	124	301	1	.940E-01
367	96	97	1	.129E+01	423	110	254	4	.701E+00	479	125	126	1	.146E+01
368	96	240	4	.701E+00	424	110	301	1	.850E-01	480	125	269	4	.701E+00
369	96	301	1	.840E-01	425	110	301	1	.830E-01	481	125	301	1	.490E-01
370	96	301	1	.800E-01	426	111	112	1	.146E+01	482	125	301	1	.860E-01
371	97	98	1	.115E+01	427	111	255	4	.701E+00	483	126	127	1	.146E+01
372	97	241	4	.889E+00	428	111	301	1	.850E-01	484	126	270	4	.701E+00
373	97	301	1	.900E-01	429	111	301	1	.830E-01	485	126	301	1	.680E-01
374	97	301	1	.930E-01	430	112	113	1	.146E+01	486	126	301	1	.860E-01
375	98	99	1	.115E+01	431	112	256	4	.701E+00	487	127	128	1	.146E+01
376	98	242	4	.889E+00	432	112	301	1	.850E-01	488	127	271	4	.701E+00
377	98	301	1	.690E-01	433	112	301	1	.830E-01	489	127	301	1	.820E-01
378	98	301	1	.123E+00	434	113	114	1	.146E+01	490	127	301	1	.850E-01
379	99	100	1	.115E+01	435	113	257	4	.701E+00	491	128	129	1	.146E+01
380	99	243	4	.889E+00	436	113	301	1	.850E-01	492	128	272	4	.701E+00
381	99	301	1	.260E-01	437	113	301	1	.830E-01	493	128	301	1	.910E-01
382	99	301	1	.149E+00	438	114	115	1	.146E+01	494	128	301	1	.840E-01
383	100	101	1	.115E+01	439	114	258	4	.701E+00	495	129	130	1	.146E+01
384	100	244	4	.889E+00	440	114	301	1	.850E-01	496	129	273	4	.701E+00
385	100	301	1	.115E+01	441	114	301	1	.830E-01	497	129	301	1	.970E-01
386	101	102	1	.889E+00	442	115	116	1	.146E+01	498	129	301	1	.830E-01
387	101	245	4	.889E+00	443	115	259	4	.701E+00	499	130	131	1	.146E+01
388	101	301	1	.920E-01	444	115	301	1	.840E-01	500	130	274	4	.701E+00
389	101	301	1	.720E-01	445	115	301	1	.830E-01	501	130	301	1	.100E+00
390	102	103	1	.129E+01	446	116	117	1	.146E+01	502	130	301	1	.830E-01
391	102	246	4	.889E+00	447	116	260	4	.701E+00	503	131	132	1	.146E+01
392	102	301	1	.124E+00	448	116	301	1	.840E-01	504	131	275	4	.701E+00

Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct	Brnh	From	To	Tag	Conduct
505	131	301	1	.101E+00	561	158	157	5	.174E+03	617	214	213	5	.174E+03
506	131	301	1	.830E-01	562	159	158	5	.174E+03	618	215	214	5	.174E+03
507	132	133	1	.146E+01	563	160	159	5	.174E+03	619	216	215	5	.174E+03
508	132	276	4	.701E+00	564	161	160	5	.174E+03	620	217	216	5	.174E+03
509	132	301	1	1.00E+00	565	162	161	5	.174E+03	621	218	217	5	.174E+03
510	132	301	1	.830E-01	566	163	162	5	.174E+03	622	219	218	5	.174E+03
511	133	134	1	.146E+01	567	164	163	5	.174E+03	623	220	219	5	.174E+03
512	133	277	4	.701E+00	568	165	164	5	.174E+03	624	221	220	5	.174E+03
513	133	301	1	.970E-01	569	166	165	5	.174E+03	625	222	221	5	.174E+03
514	133	301	1	.830E-01	570	167	166	5	.174E+03	626	223	222	5	.174E+03
515	134	135	1	.146E+01	571	168	167	5	.174E+03	627	224	223	5	.174E+03
516	134	278	4	.701E+00	572	169	168	5	.174E+03	628	225	224	5	.174E+03
517	134	301	1	.910E-01	573	170	169	5	.174E+03	629	226	225	5	.174E+03
518	134	301	1	.840E-01	574	171	170	5	.174E+03	630	227	226	5	.174E+03
519	135	136	1	.146E+01	575	172	171	5	.174E+03	631	228	227	5	.174E+03
520	135	279	4	.701E+00	576	173	172	5	.174E+03	632	229	228	5	.174E+03
521	135	301	1	.820E-01	577	174	173	5	.174E+03	633	230	229	5	.174E+03
522	135	301	1	.840E-01	578	175	174	5	.174E+03	634	231	230	5	.174E+03
523	136	137	1	.146E+01	579	176	175	5	.174E+03	635	232	231	5	.174E+03
524	136	280	4	.701E+00	580	177	176	5	.174E+03	636	233	232	5	.174E+03
525	136	301	1	.680E-01	581	178	177	5	.174E+03	637	234	233	5	.174E+03
526	136	301	1	.860E-01	582	179	178	5	.174E+03	638	235	234	5	.174E+03
527	137	138	1	.146E+01	583	180	179	5	.174E+03	639	236	235	5	.174E+03
528	137	281	4	.701E+00	584	181	180	5	.174E+03	640	237	236	5	.174E+03
529	137	301	1	.490E-01	585	182	181	5	.174E+03	641	238	237	5	.174E+03
530	137	301	1	.870E-01	586	183	182	5	.174E+03	642	239	238	5	.174E+03
531	138	139	1	.146E+01	587	184	183	5	.174E+03	643	240	239	5	.174E+03
532	138	282	4	.701E+00	588	185	184	5	.174E+03	644	241	240	5	.174E+03
533	138	301	1	.240E-01	589	186	185	5	.174E+03	645	242	241	5	.174E+03
534	138	301	1	.880E-01	590	187	186	5	.174E+03	646	243	242	5	.174E+03
535	139	140	1	.146E+01	591	188	187	5	.174E+03	647	244	243	5	.174E+03
536	139	283	4	.701E+00	592	189	188	5	.174E+03	648	245	244	5	.174E+03
537	139	301	1	.900E-01	593	190	189	5	.174E+03	649	246	245	5	.174E+03
538	140	141	1	.160E+01	594	191	190	5	.174E+03	650	247	246	5	.174E+03
539	140	284	4	.701E+00	595	192	191	5	.174E+03	651	248	247	5	.174E+03
540	140	301	1	.910E-01	596	193	192	5	.174E+03	652	249	248	5	.174E+03
541	141	142	1	.178E+01	597	194	193	5	.174E+03	653	250	249	5	.174E+03
542	141	285	4	.576E+00	598	195	194	5	.174E+03	654	251	250	5	.174E+03
543	142	143	1	.178E+01	599	196	195	5	.174E+03	655	252	251	5	.174E+03
544	142	286	4	.576E+00	600	197	196	5	.174E+03	656	253	252	5	.174E+03
545	143	144	1	.178E+01	601	198	197	5	.174E+03	657	254	253	5	.174E+03
546	143	287	4	.576E+00	602	199	198	5	.174E+03	658	255	254	5	.174E+03
547	144	288	4	.576E+00	603	200	199	5	.174E+03	659	256	255	5	.174E+03
548	145	302	5	.174E+03	604	201	200	5	.174E+03	660	257	256	5	.174E+03
549	146	145	5	.174E+03	605	202	201	5	.174E+03	661	258	257	5	.174E+03
550	147	146	5	.174E+03	606	203	202	5	.174E+03	662	259	258	5	.174E+03
551	148	147	5	.174E+03	607	204	203	5	.174E+03	663	260	259	5	.174E+03
552	149	148	5	.174E+03	608	205	204	5	.174E+03	664	261	260	5	.174E+03
553	150	149	5	.174E+03	609	206	205	5	.174E+03	665	262	261	5	.174E+03
554	151	150	5	.174E+03	610	207	206	5	.174E+03	666	263	262	5	.174E+03
555	152	151	5	.174E+03	611	208	207	5	.174E+03	667	264	263	5	.174E+03
556	153	152	5	.174E+03	612	209	208	5	.174E+03	668	265	264	5	.174E+03
557	154	153	5	.174E+03	613	210	209	5	.174E+03	669	266	265	5	.174E+03
558	155	154	5	.174E+03	614	211	210	5	.174E+03	670	267	266	5	.174E+03
559	156	155	5	.174E+03	615	212	211	5	.174E+03	671	268	267	5	.174E+03
560	157	156	5	.174E+03	616	213	212	5	.174E+03	672	269	268	5	.174E+03

Brnh	From	To	Tag	Conduct
673	270	269	5	.174E+03
674	271	270	5	.174E+03
675	272	271	5	.174E+03
676	273	272	5	.174E+03
677	274	273	5	.174E+03
678	275	274	5	.174E+03
679	276	275	5	.174E+03
680	277	276	5	.174E+03
681	278	277	5	.174E+03
682	279	278	5	.174E+03
683	280	279	5	.174E+03
684	281	280	5	.174E+03
685	282	281	5	.174E+03
686	283	282	5	.174E+03
687	284	283	5	.174E+03
688	285	284	5	.174E+03
689	286	285	5	.174E+03
690	287	286	5	.174E+03
691	288	287	5	.174E+03

APPENDIX E. TASS NODAL TEMPERATURE OUTPUT

The following output summarizes the Steady State Thermal Analyzer output for the mass flow rates considered in this analysis.

TALSR(METRIC)--RUN 1. SIMPLE MODEL. MASS FLOW 149.7 kg/hr (330 lbm/hr)

Temperatures, degC

1	25.19	2	25.26	3	25.40	4	25.67	5	26.22	6	26.60
7	26.97	8	27.31	9	27.60	10	27.81	11	27.97	12	28.07
13	28.13	14	28.16	15	28.15	16	28.10	17	28.01	18	27.87
19	27.65	20	27.33	21	26.85	22	26.58	23	26.55	24	27.19
25	27.56	26	27.76	27	27.95	28	28.03	29	28.08	30	28.10
31	28.12	32	28.13	33	28.14	34	28.15	35	28.16	36	28.17
37	28.18	38	28.19	39	28.19	40	28.19	41	28.17	42	28.12
43	27.99	44	27.61	45	27.15	46	27.66	47	27.93	48	28.05
49	28.19	50	28.25	51	28.29	52	28.31	53	28.32	54	28.34
55	28.35	56	28.36	57	28.37	58	28.37	59	28.38	60	28.39
61	28.40	62	28.40	63	28.41	64	28.40	65	28.37	66	28.84
67	29.28	68	29.43	69	29.36	70	28.87	71	28.39	72	27.84
73	27.85	74	28.42	75	28.92	76	29.43	77	29.53	78	29.39
79	28.97	80	28.53	81	28.58	82	28.61	83	28.62	84	28.64
85	28.65	86	28.66	87	28.67	88	28.67	89	28.68	90	28.69
91	28.70	92	28.71	93	28.71	94	28.71	95	28.69	96	28.64
97	28.53	98	28.43	99	28.19	100	27.73	101	28.18	102	28.57
103	28.71	104	28.77	105	28.80	106	28.82	107	28.84	108	28.85
109	28.86	110	28.87	111	28.88	112	28.88	113	28.89	114	28.90
115	28.90	116	28.89	117	28.87	118	28.81	119	28.65	120	28.48
121	28.15	122	27.57	123	27.61	124	27.88	125	28.34	126	28.64
127	28.86	128	29.01	129	29.11	130	29.17	131	29.20	132	29.19
133	29.15	134	29.07	135	28.95	136	28.77	137	28.53	138	28.23
139	27.91	140	27.57	141	27.09	142	26.84	143	26.72	144	26.66
145	25.00	146	25.00	147	25.00	148	25.00	149	25.01	150	25.02
151	25.02	152	25.03	153	25.04	154	25.05	155	25.07	156	25.08
157	25.09	158	25.10	159	25.12	160	25.13	161	25.14	162	25.15
163	25.16	164	25.17	165	25.18	166	25.18	167	25.19	168	25.20
169	25.21	170	25.23	171	25.24	172	25.25	173	25.26	174	25.27
175	25.28	176	25.29	177	25.31	178	25.32	179	25.33	180	25.34
181	25.35	182	25.36	183	25.37	184	25.39	185	25.40	186	25.41
187	25.42	188	25.43	189	25.44	190	25.45	191	25.46	192	25.48
193	25.49	194	25.50	195	25.51	196	25.52	197	25.53	198	25.54
199	25.56	200	25.57	201	25.58	202	25.59	203	25.60	204	25.61
205	25.62	206	25.63	207	25.65	208	25.66	209	25.67	210	25.69
211	25.70	212	25.71	213	25.73	214	25.74	215	25.75	216	25.77
217	25.78	218	25.79	219	25.81	220	25.82	221	25.83	222	25.84
223	25.86	224	25.87	225	25.88	226	25.90	227	25.91	228	25.92
229	25.93	230	25.94	231	25.95	232	25.96	233	25.97	234	25.98
235	25.99	236	26.00	237	26.02	238	26.03	239	26.04	240	26.05
241	26.06	242	26.07	243	26.08	244	26.09	245	26.10	246	26.11
247	26.12	248	26.14	249	26.15	250	26.16	251	26.17	252	26.18
253	26.19	254	26.20	255	26.21	256	26.22	257	26.23	258	26.24
259	26.25	260	26.26	261	26.27	262	26.28	263	26.30	264	26.31
265	26.32	266	26.32	267	26.33	268	26.34	269	26.35	270	26.36
271	26.37	272	26.38	273	26.39	274	26.40	275	26.41	276	26.42
277	26.43	278	26.44	279	26.45	280	26.46	281	26.47	282	26.48
283	26.48	284	26.49	285	26.49	286	26.49	287	26.49	288	26.49
301	40.00	302	25.00								

TALSR(METRIC)--RUN 2. COMPLEX MODEL, MASS FLOW 149.7 kg/hr (330 lbm/hr)
 Temperatures, degC

1	25.21	2	25.28	3	25.44	4	25.74	5	26.33	6	26.73
7	27.09	8	27.41	9	27.68	10	27.87	11	28.01	12	28.10
13	28.16	14	28.18	15	28.17	16	28.13	17	28.04	18	27.90
19	27.69	20	27.39	21	26.91	22	26.65	23	26.62	24	27.20
25	27.56	26	27.78	27	27.98	28	28.06	29	28.10	30	28.11
31	28.15	32	28.15	33	28.16	34	28.16	35	28.16	36	28.16
37	28.14	38	28.13	39	28.11	40	28.09	41	28.07	42	28.03
43	27.97	44	27.62	45	27.18	46	27.65	47	27.93	48	28.07
49	28.22	50	28.28	51	28.32	52	28.34	53	28.35	54	28.36
55	28.37	56	28.37	57	28.37	58	28.38	59	28.38	60	28.39
61	28.39	62	28.39	63	28.38	64	28.37	65	28.32	66	28.79
67	29.24	68	29.42	69	29.35	70	28.87	71	28.39	72	27.85
73	27.85	74	28.42	75	28.91	76	29.41	77	29.49	78	29.34
79	28.91	80	28.50	81	28.57	82	28.60	83	28.62	84	28.63
85	28.65	86	28.65	87	28.66	88	28.66	89	28.66	90	28.67
91	28.68	92	28.68	93	28.68	94	28.68	95	28.66	96	28.60
97	28.49	98	28.40	99	28.16	100	27.74	101	28.18	102	28.55
103	28.65	104	28.70	105	28.74	106	28.77	107	28.80	108	28.81
109	28.85	110	28.86	111	28.87	112	28.88	113	28.89	114	28.89
115	28.89	116	28.87	117	28.84	118	28.78	119	28.62	120	28.44
121	28.13	122	27.62	123	27.67	124	27.93	125	28.37	126	28.67
127	28.87	128	29.02	129	29.11	130	29.16	131	29.19	132	29.18
133	29.15	134	29.08	135	28.96	136	28.80	137	28.57	138	28.29
139	27.97	140	27.63	141	27.12	142	26.86	143	26.73	144	26.67
145	28.00	146	25.00	147	25.00	148	25.01	149	25.01	150	25.02
151	25.03	152	25.04	153	25.05	154	25.06	155	25.07	156	25.08
157	25.09	158	25.11	159	25.12	160	25.13	161	25.14	162	25.15
163	25.16	164	25.17	165	25.18	166	25.19	167	25.20	168	25.21
169	25.22	170	25.23	171	25.24	172	25.25	173	25.27	174	25.28
175	25.29	176	25.30	177	25.31	178	25.32	179	25.33	180	25.35
181	25.36	182	25.37	183	25.38	184	25.39	185	25.40	186	25.41
187	25.42	188	25.44	189	25.44	190	25.46	191	25.47	192	25.48
193	25.49	194	25.50	195	25.51	196	25.53	197	25.54	198	25.55
199	25.56	200	25.57	201	25.58	202	25.59	203	25.60	204	25.62
205	25.63	206	25.64	207	25.65	208	25.66	209	25.68	210	25.69
211	25.70	212	25.71	213	25.73	214	25.74	215	25.76	216	25.77
217	25.78	218	25.79	219	25.81	220	25.82	221	25.84	222	25.85
223	25.86	224	25.88	225	25.89	226	25.90	227	25.91	228	25.92
229	25.93	230	25.94	231	25.95	232	25.96	233	25.97	234	25.98
235	26.00	236	26.01	237	26.02	238	26.03	239	26.04	240	26.05
241	26.06	242	26.07	243	26.08	244	26.09	245	26.10	246	26.11
247	26.12	248	26.14	249	26.15	250	26.16	251	26.17	252	26.18
253	26.19	254	26.20	255	26.21	256	26.22	257	26.23	258	26.24
259	26.25	260	26.26	261	26.27	262	26.28	263	26.30	264	26.31
265	26.32	266	26.32	267	26.33	268	26.34	269	26.35	270	26.35
271	26.36	272	26.38	273	26.39	274	26.40	275	26.41	276	26.42
277	26.43	278	26.44	279	26.45	280	26.46	281	26.47	282	26.48
283	26.48	284	26.49	285	26.49	286	26.49	287	26.49	288	26.49
301	40.00	302	25.00								

TALSR(METRIC)--RUN 3. COMPLEX MODEL, MASS FLOW OF 68 kg/hr (150 lbm/hr)

Temperatures, degC

1	25.69	2	25.81	3	26.07	4	26.51	5	27.28	6	27.87
7	28.41	8	28.88	9	29.26	10	29.55	11	29.76	12	29.89
13	29.97	14	30.01	15	30.00	16	29.93	17	29.81	18	29.62
19	29.33	20	28.95	21	28.39	22	28.07	23	28.06	24	28.71
25	29.18	26	29.50	27	29.75	28	29.88	29	29.96	30	30.01
31	30.04	32	30.06	33	30.07	34	30.08	35	30.08	36	30.07
37	30.06	38	30.04	39	30.02	40	29.99	41	29.94	42	29.88
43	29.78	44	29.40	45	28.96	46	29.44	47	29.77	48	29.96
49	30.15	50	30.25	51	30.31	52	30.34	53	30.37	54	30.39
55	30.40	56	30.41	57	30.42	58	30.42	59	30.43	60	30.44
61	30.43	62	30.45	63	30.46	64	30.46	65	30.47	66	30.97
67	31.41	68	31.59	69	31.51	70	31.03	71	30.50	72	29.94
73	29.95	74	30.54	75	31.09	76	31.60	77	31.70	78	31.56
79	31.16	80	30.73	81	30.76	82	30.78	83	30.80	84	30.81
85	30.83	86	30.84	87	30.85	88	30.86	89	30.86	90	30.87
91	30.88	92	30.88	93	30.88	94	30.87	95	30.84	96	30.77
97	30.63	98	30.50	99	30.25	100	29.85	101	30.29	102	30.68
103	30.83	104	30.92	105	30.98	106	31.02	107	31.07	108	31.10
109	31.13	110	31.15	111	31.17	112	31.18	113	31.19	114	31.19
115	31.18	116	31.16	117	31.11	118	31.02	119	30.83	120	30.59
121	30.22	122	29.69	123	29.73	124	30.03	125	30.53	126	30.88
127	31.14	128	31.33	129	31.45	130	31.53	131	31.56	132	31.56
133	31.51	134	31.41	135	31.26	136	31.04	137	30.74	138	30.37
139	29.94	140	29.48	141	28.87	142	28.53	143	28.33	144	28.24
145	25.00	146	25.01	147	25.01	148	25.02	149	25.03	150	25.04
151	25.06	152	25.07	153	25.09	154	25.11	155	25.14	156	25.16
157	25.18	158	25.20	159	25.23	160	25.25	161	25.27	162	25.29
163	25.31	164	25.33	165	25.34	166	25.36	167	25.38	168	25.40
169	25.42	170	25.44	171	25.46	172	25.48	173	25.51	174	25.53
175	25.55	176	25.57	177	25.59	178	25.61	179	25.63	180	25.65
181	25.67	182	25.69	183	25.71	184	25.73	185	25.75	186	25.77
187	25.80	188	25.82	189	25.84	190	25.86	191	25.88	192	25.91
193	25.93	194	25.95	195	25.97	196	25.99	197	26.01	198	26.03
199	26.05	200	26.07	201	26.09	202	26.11	203	26.13	204	26.15
205	26.17	206	26.19	207	26.21	208	26.23	209	26.26	210	26.28
211	26.30	212	26.33	213	26.35	214	26.38	215	26.40	216	26.42
217	26.44	218	26.47	219	26.50	220	26.52	221	26.54	222	26.56
223	26.58	224	26.61	225	26.63	226	26.65	227	26.67	228	26.69
229	26.71	230	26.73	231	26.75	232	26.77	233	26.79	234	26.80
235	26.82	236	26.84	237	26.86	238	26.88	239	26.90	240	26.92
241	26.94	242	26.96	243	26.98	244	27.00	245	27.02	246	27.04
247	27.06	248	27.07	249	27.09	250	27.11	251	27.13	252	27.15
253	27.17	254	27.19	255	27.20	256	27.22	257	27.24	258	27.26
259	27.28	260	27.30	261	27.32	262	27.33	263	27.35	264	27.37
265	27.39	266	27.40	267	27.42	268	27.43	269	27.45	270	27.46
271	27.48	272	27.50	273	27.52	274	27.54	275	27.55	276	27.57
277	27.59	278	27.61	279	27.63	280	27.64	281	27.66	282	27.67
283	27.68	284	27.69	285	27.69	286	27.70	287	27.70	288	27.70
301	40.00	302	25.00								

TALSR(METRIC)--RUN 4. COMPLEX MODEL, MASS FLOW OF 272.2 kg/hr (600 lbm/hr)

Temperatures, degC									
1	25.07	2	25.11	3	25.21	4	25.41	5	25.87
7	26.38	8	26.61	9	26.80	10	26.93	11	27.03
13	27.13	14	27.14	15	27.14	16	27.11	17	27.05
19	26.80	20	26.57	21	26.19	22	25.99	23	25.95
25	26.70	26	26.85	27	26.99	28	27.04	29	27.07
31	27.10	32	27.10	33	27.10	34	27.10	35	27.10
37	27.09	38	27.08	39	27.07	40	27.05	41	26.94
43	26.99	44	26.70	45	26.30	46	26.72	47	26.94
49	27.15	50	27.19	51	27.21	52	27.22	53	27.23
55	27.24	56	27.24	57	27.24	58	27.24	59	27.24
61	27.25	62	27.25	63	27.24	64	27.21	65	27.14
67	27.95	68	28.10	69	28.05	70	27.62	71	27.23
73	26.76	74	27.25	75	27.65	76	28.09	77	28.15
79	27.61	80	27.26	81	27.35	82	27.38	83	27.40
85	27.42	86	27.42	87	27.43	88	27.43	89	27.43
91	27.44	92	27.44	93	27.44	94	27.44	95	27.43
97	27.30	98	27.24	99	27.05	100	26.65	101	27.06
103	27.42	104	27.46	105	27.48	106	27.50	107	27.52
109	27.55	110	27.56	111	27.57	112	27.57	113	27.58
115	27.58	116	27.57	117	27.56	118	27.51	119	27.39
121	27.03	122	26.58	123	26.63	124	26.83	125	27.20
127	27.58	128	27.68	129	27.75	130	27.78	131	27.80
133	27.77	134	27.72	135	27.64	136	27.52	137	27.35
139	26.92	140	26.68	141	26.27	142	26.09	143	26.00
145	25.00	146	25.00	147	25.00	148	25.00	149	25.01
151	25.01	152	25.02	153	25.03	154	25.03	155	25.04
157	25.06	158	25.06	159	25.07	160	25.08	161	25.08
163	25.10	164	25.10	165	25.11	166	25.11	167	25.12
169	25.13	170	25.14	171	25.14	172	25.15	173	25.16
175	25.17	176	25.18	177	25.18	178	25.19	179	25.20
181	25.21	182	25.22	183	25.22	184	25.23	185	25.24
187	25.25	188	25.26	189	25.26	190	25.27	191	25.28
193	25.29	194	25.30	195	25.31	196	25.31	197	25.32
199	25.33	200	25.34	201	25.35	202	25.35	203	25.36
205	25.37	206	25.38	207	25.39	208	25.39	209	25.40
211	25.42	212	25.43	213	25.44	214	25.45	215	25.45
217	25.47	218	25.47	219	25.48	220	25.49	221	25.50
223	25.52	224	25.53	225	25.53	226	25.54	227	25.55
229	25.56	230	25.57	231	25.57	232	25.58	233	25.59
235	25.60	236	25.61	237	25.61	238	25.62	239	25.62
241	25.64	242	25.65	243	25.65	244	25.66	245	25.66
247	25.68	248	25.68	249	25.69	250	25.70	251	25.70
253	25.72	254	25.72	255	25.73	256	25.74	257	25.74
259	25.76	260	25.76	261	25.77	262	25.77	263	25.78
265	25.79	266	25.80	267	25.80	268	25.81	269	25.81
271	25.82	272	25.83	273	25.84	274	25.84	275	25.85
277	25.86	278	25.87	279	25.88	280	25.88	281	25.89
283	25.90	284	25.90	285	25.90	286	25.90	287	25.90
301	40.00	302	25.00						

TALSR(METRIC)--RUN 5. COMPLEX MODEL, MASS FLOW OF 362.9 kg/hr (800 lbm/hr)											Page No. 1
Temperatures, degC											
1	25.04	2	25.07	3	25.14	4	25.31	5	25.72	6	25.93
7	26.13	8	26.32	9	26.47	10	26.59	11	26.67	12	26.72
13	26.75	14	26.76	15	26.75	16	26.73	17	26.68	18	26.60
19	26.43	20	26.28	21	25.95	22	25.77	23	25.73	24	26.17
25	26.39	26	26.51	27	26.63	28	26.67	29	26.69	30	26.71
31	26.71	32	26.71	33	26.72	34	26.72	35	26.72	36	26.71
37	26.70	38	26.69	39	26.68	40	26.67	41	26.66	42	26.65
43	26.63	44	26.37	45	26.00	46	26.39	47	26.59	48	26.65
49	26.75	50	26.79	51	26.80	52	26.81	53	26.82	54	26.82
55	26.82	56	26.82	57	26.82	58	26.83	59	26.83	60	26.83
61	26.83	62	26.83	63	26.82	64	26.80	65	26.72	66	27.06
67	27.45	68	27.59	69	27.55	70	27.15	71	26.81	72	26.38
73	26.38	74	26.82	75	27.17	76	27.58	77	27.63	78	27.50
79	27.12	80	26.81	81	26.91	82	26.93	83	26.95	84	26.96
85	26.97	86	26.97	87	26.97	88	26.97	89	26.97	90	26.98
91	26.98	92	26.98	93	26.99	94	26.99	95	26.98	96	26.95
97	26.86	98	26.82	99	26.66	100	26.28	101	26.66	102	26.93
103	26.97	104	27.00	105	27.01	106	27.03	107	27.05	108	27.06
109	27.07	110	27.08	111	27.09	112	27.09	113	27.09	114	27.10
115	27.10	116	27.09	117	27.08	118	27.05	119	26.94	120	26.84
121	26.63	122	26.23	123	26.28	124	26.45	125	26.78	126	26.97
127	27.10	128	27.19	129	27.24	130	27.27	131	27.28	132	27.28
133	27.26	134	27.22	135	27.15	136	27.04	137	26.90	138	26.73
139	26.54	140	26.35	141	25.98	142	25.83	143	25.76	144	25.74
145	25.00	146	25.00	147	25.00	148	25.00	149	25.00	150	25.01
151	25.01	152	25.02	153	25.02	154	25.03	155	25.03	156	25.04
157	25.04	158	25.05	159	25.05	160	25.06	161	25.07	162	25.07
163	25.07	164	25.08	165	25.08	166	25.09	167	25.09	168	25.09
169	25.10	170	25.10	171	25.11	172	25.12	173	25.12	174	25.13
175	25.13	176	25.14	177	25.14	178	25.15	179	25.15	180	25.16
181	25.16	182	25.17	183	25.17	184	25.18	185	25.18	186	25.19
187	25.19	188	25.20	189	25.20	190	25.21	191	25.21	192	25.22
193	25.22	194	25.23	195	25.24	196	25.24	197	25.25	198	25.25
199	25.26	200	25.26	201	25.27	202	25.27	203	25.28	204	25.28
205	25.29	206	25.29	207	25.30	208	25.30	209	25.31	210	25.32
211	25.32	212	25.33	213	25.34	214	25.34	215	25.35	216	25.36
217	25.36	218	25.37	219	25.37	220	25.38	221	25.39	222	25.39
223	25.40	224	25.41	225	25.41	226	25.42	227	25.42	228	25.43
229	25.43	230	25.44	231	25.44	232	25.45	233	25.45	234	25.46
235	25.46	236	25.47	237	25.47	238	25.48	239	25.48	240	25.49
241	25.49	242	25.50	243	25.50	244	25.51	245	25.51	246	25.52
247	25.52	248	25.53	249	25.53	250	25.54	251	25.54	252	25.55
253	25.55	254	25.56	255	25.56	256	25.57	257	25.57	258	25.58
259	25.59	260	25.59	261	25.60	262	25.60	263	25.61	264	25.61
265	25.62	266	25.62	267	25.62	268	25.62	269	25.63	270	25.63
271	25.64	272	25.64	273	25.65	274	25.65	275	25.66	276	25.66
277	25.67	278	25.68	279	25.68	280	25.68	281	25.69	282	25.69
283	25.70	284	25.70	285	25.70	286	25.70	287	25.70	288	25.70
301	40.00	302	25.00								

LIST OF REFERENCES

- Burmeister, L. C., (1993). *Convective Heat Transfer*, 2nd Ed., John Wiley & Sons Book Company, New York.
- Garrett, S. L., (1992). *ThermoAcoustic Life Sciences Refrigerator: Heat Exchanger Design and Performance Prediction*, NASA Technical Report.
- Hamming, R., (1973). *Numerical Methods for Scientists and Engineers*, Dover Publishing Co., New York.
- Incropera, F. P., and DeWitt, D. P. (1985). *Fundamentals of Heat and Mass Transfer*, 2nd Ed., John Wiley & Sons Book Company, New York.
- Kays, W. M., and London, A. L. (1984) *Compact Heat Exchangers*, 3rd Ed., McGraw-Hill Book Company, New York.
- Kern, D. Q., and Kraus, A. D. (1972). *Extended Surface Heat Transfer*, McGraw-Hill Book Company, New York.
- Kraus, A. D. (1961). Efficiency of the Cold Plate Heat Exchanger, Proc. Natl. Aeronaut. Electronics Conf., Dayton, Ohio, 381.
- Kraus, A. D. (1962). Optimization of the Cold Plate Heat Exchanger, Proc. Natl. Aeronaut. Electronics Conf., Dayton, Ohio, 78.
- Kraus, A. D., Snider, A. D., and Doty, L. F. (1978). An Efficient Algorithm for Evaluating Arrays of Extended Surfaces, *J. Heat Transfer*, 100, 288.
- Kraus, A. D. (1982). *Analysis and Evaluation of Extended Surface Thermal Systems*, Hemisphere Publishing Co., New York.
- Kraus, A. D. (1989). *Steady State Thermal Analyzer User's Guide*, InterCept Software, San Diego.
- Pieper, R. J., and Kraus, A. D. (1995). Cold Plates with Asymmetric Heat Loading Part I - The Single Stack, *Proceedings of the ASME Inetpack'95 Conference, Advances in Electronic Packaging*, Vol. 10-2, ASME, pp 871-876, March 1995
- Sieder, E. N., and Tate, G. E., (1936). *Ind. Eng. Chem.*, 28, 1429.
- Snider, A. D., and Kraus, A. D. (1981). A General Extended

Surface Analysis Method, *J. Heat Transfer*, 103, 699.

Vainshtein, P., Fichman, M., and Gutfinger, C. (1995). Acoustic enhancement of heat transfer between two parallel plates, *Int. J. Heat Mass Transfer*, Vol. 38, No. 10, pp 1893.

INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Technical Information Center Cameron Station Alexandria, Virginia 22304-6145	2
2. Library, Code 52 Naval Postgraduate School Monterey, California 93943-5101	2
3. Department Chairman, Code ME Department of Mechanical Engineering Naval Postgraduate School Monterey, California 93943-5000	1
4. Department Chairman, Code AA Department of Aeronautics and Astronautics Naval Postgraduate School Monterey, California 93953-5106	1
5. Chairman, Code SP Space Systems Academic Group Naval Postgraduate School Monterey, California 93943-5110	1
6. Captain Thompson Office of the Chief of Naval Operations Code N63, Room 4E679 The Pentagon Washington, DC 20350-2000	1
7. Professor Ron J. Pieper, Code EC/Pr Department of Electrical and Computer Engineering Naval Postgraduate School Monterey, California 93943-5121	1
8. Professor Allan D. Kraus, Code EC/KS Department of Electrical and Computer Engineering Naval Postgraduate School Monterey, California 93943-5121	1
9. Professor Ashok Gopinath, Code ME/ Department of Mechanical Engineering Naval Postgraduate School Monterey, California 93943-5000	1
10. Professor Oscar Biblarz, Code AA/Bi Department of Aeronautics and Astronautics Naval Postgraduate School Monterey, California 93943-5106	1

11. LT Kevin S. Muhs
PO Box 570021
Orlando, Florida 32857-0021

2

DUDLEY KNOX LIBRARY
NAVAL POSTGRADUATE SCHOOL
MONTEREY CA 93943-5101



DUDLEY KNOX LIBRARY



3 2768 00317374 1